

WICHITA STATE UNIVERSITY NATIONAL INSTITUTE FOR AVIATION RESEARCH

Report No: NCP-RP-2024-002 Rev N/C Report Date: August 7<sup>th</sup>, 2024



# Renegade RM-2014-LDk-Tk 4581 8HS Quartz fabric 286 gsm 38% RC Material Allowables Statistical Analysis Report

NCAMP Project Number: NPN 032302

# NCAMP Report Number: NCP-RP-2024-002 Rev N/C

Report Date: August 7th, 2024

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# 1. Introduction

This report contains statistical analysis of the Renegade RM-2014-LDk-Tk 4581 8HS Quartz satin fabric prepreg material property data published in NCAMP Test Report CAM-RP-2024-007 Rev N/C. The lamina and laminate material property data have been generated with NCAMP oversight through NCAMP Project Number NPN 032302 and also meet the requirements outlined in NCAMP Standard Operating Procedure NSP 100. The test panels and test specimens have been inspected by NCAMP Authorized Inspection Representatives (AIR) and the testing has been witnessed by NCAMP Authorized Engineering Representatives (AER).

B-Basis values, A-estimates, and B-estimates were calculated using a variety of techniques that are detailed in section 2. The qualification material was procured to NCAMP Material Specification NMS 201/1 Rev -, dated August 31<sup>st</sup>, 2023. The qualification test panels were cured in accordance with NCAMP Process Specification NPS 82014 Rev -, dated July 5<sup>th</sup>, 2023 using "A" Cure Cycle. The panels were fabricated at Resonant Sciences, 4085 Executive Dr., Dayton, OH 45430. The NCAMP Test Plan NTP 2014Q1 was used for this qualification program. The testing was performed at Renegade Materials Corporation in Miamisburg, Ohio and the National Institute for Aviation Research (NIAR) in Wichita, Kansas.

Basis numbers are labeled as 'values' when the data meets all the requirements of CMH-17-1H. When those requirements are not met, they will be labeled as 'estimates.' When the data does not meet all requirements, the failure to meet these requirements is reported and the specific requirement(s) the data fails to meet is identified. The method used to compute the basis value is noted for each basis value provided. When appropriate, in addition to the traditional computational methods, values computed using the modified coefficient of variation method is also provided.

The material property data acquisition process is designed to generate basic material property data with sufficient pedigree for submission to Complete Documentation sections of the Composite Materials Handbook (CMH-17-1H).

The NCAMP shared material property database contains material property data of common usefulness to a wide range of aerospace projects. However, the data may not fulfill all the needs of a project. Specific properties, environments, laminate architecture, and loading situations that individual projects need may require additional testing.

The use of NCAMP material and process specifications do not guarantee material or structural performance. Material users should be actively involved in evaluating material performance and quality including, but not limited to, performing regular purchaser quality control tests, performing periodic equivalency/additional testing, participating in material change management activities, conducting statistical process control, and conducting regular supplier audits.

The applicability and accuracy of NCAMP material property data, material allowables, and specifications must be evaluated on case-by-case basis by aircraft companies and certifying agencies. NCAMP assumes no liability whatsoever, expressed or implied, related to the use of the material property data, material allowables, and specifications.

Part fabricators that wish to utilize the material property data, allowables, and specifications may be able to do so by demonstrating the capability to reproduce the original material properties; a process known as equivalency. More information about this equivalency process including the test statistics and its limitations can be found in Section 6 of DOT/FAA/AR-03/19 and Section 8.4.1 of CMH-17-1G. The applicability of equivalency process must be evaluated on program-by-program basis by the applicant and certifying agency. The applicant and certifying agency must agree that the equivalency test plan along with the equivalency process described in Section 6 of DOT/FAA/AR-03/19 and Section 6 of DOT/FAA/AR-03/19 and Section 8.4.1 of CMH-17-1G are adequate for the given program.

Aircraft companies should not use the data published in this report without specifying NCAMP Material Specification NMS 201/1. NMS 201/1 has additional requirements that are listed in its prepreg process control document (PCD), fiber specification, fiber PCD, and other raw material specifications and PCDs which impose essential quality controls on the raw materials and raw material manufacturing equipment and processes. *Aircraft companies and certifying agencies should assume that the material property data published in this report is not applicable when the material is not procured to NCAMP Material Specification NMS 201/1.* NMS 201/1 is a free, publicly available, non-proprietary aerospace industry material specification.

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Test Property	Abbreviation
Warp Compression	WC
Warp Tension	WT
Fill Compression	FC
Fill Tension	FT
In-Plane Shear	IPS
Short Beam Strength	SBS
Unnotched Tension	UNT
Unnotched Compression	UNC
Filled Hole Tension	FHT
Filled Hole Compression	FHC
Open Hole Tension	OHT
Open Hole Compression	OHC
Single Shear Bearing	SSB
Interlaminar Tension	ILT
Compression After Impact	CAI

# **1.1** Symbols and Abbreviations

### Table 1-1: Test Property Abbreviations

Test Property	Symbol
Warp Compression Strength	F1 <sup>cu</sup>
Warp Compression Modulus	$E_1^c$
Warp Compression Poisson's Ratio	$v_{12}^{c}$
Warp Tension Strength	$F_1$ <sup>tu</sup>
Warp Tension Modulus	$E_1^t$
Warp Tension Poisson's Ratio	$v_{12}^t$
Fill Compression Strength	$F_2^{cu}$
Fill Compression Modulus	$E_2^c$
Fill Compression Poisson's Ratio	$v_{21}^{c}$
Fill Tension Strength	$F_2^{tu}$
Fill Tension Modulus	$E_2^t$
In Plane Shear Strength at 5% strain	$F_{12}^{s5\%}$
In Plane Shear Strength at 0.2% offset	$F_{12}^{s0.2\%}$
In Plane Shear Modulus	$G_{12}^s$

Table 1-2: Test Property Symbols

<b>Environmental Condition</b>	Abbreviation	Temperature
Cold Temperature Dry	CTD	$-65 \pm 5^{\circ}F$
Room Temperature Dry	RTD	$70 \pm 10^{\circ} F$
Elevated Temperature Dry	ETD	$212 \pm 5^{\circ}F$
Elevated Temperature Wet	ETW	$212 \pm 5^{\circ}F$

### Table 1-3: Environmental Conditions Abbreviations

Tests with a number immediately after the abbreviation indicate the lay-up:

1 refers to a 25/50/25 layup. This is also referred to as "Quasi-Isotropic" 2 refers to a 10/80/10 layup. This is also referred to as "Soft" 3 refers to a 40/20/40 layup. This is also referred to as "Hard"

EX: OHT1 is an open hole tension test with a 25/50/25 layup

Detailed information about the test methods and conditions used is given in NCAMP Test Report CAM-RP-2024-007 Rev N/C.

# **1.2 Pooling Across Environments**

When pooling across environments was allowable, the pooled co-efficient of variation was used. CMH17 STATS (CMH17 Approved Statistical Analysis Program) was used to determine if pooling was allowable and to compute the pooled coefficient of variation for those tests. In these cases, the modified coefficient of variation based on the pooled data was used to compute the basis values.

When pooling across environments was not advisable because the data was not eligible for pooling and engineering judgment indicated there was no justification for overriding the result, then B-Basis values were computed for each environmental condition separately, which are also provided by CMH17 STATS.

# **1.3 Basis Value Computational Process**

The general form to compute engineering basis values is: basis value  $= \overline{X} - kS$  where k is a factor based on the sample size and the distribution of the sample data. There are many different methods to determine the value of k in this equation, depending on the sample size and the distribution of the data. In addition, the computational formula used for the standard deviation, S, may vary depending on the distribution of the data. The details of those different computations and when each should be used are in section 2.

# **1.4 Modified Coefficient of Variation (CV) Method**

A common problem with new material qualifications is that the initial specimens produced and tested do not contain all of the variability that will be encountered when the material is being produced in larger amounts over a lengthy period of time. This can result in setting basis values that are unrealistically high. The variability as measured in the qualification program is often lower than the actual material variability because of several reasons. The materials used in the qualification programs are usually manufactured within a short period of time, typically 2-3 weeks only, which is not representative of the production material. Some raw ingredients that are used to manufacture the multi-batch qualification materials may actually be from the same production batches or manufactured within a short period of time so the qualification materials, although regarded as multiple batches, may not truly be multiple batches so they are not representative of the actual production material variability.

The modified Coefficient of Variation (CV) used in this report is in accordance with section 8.4.4 of CMH-17-1G. It is a method of adjusting the original basis values downward in anticipation of the expected additional variation. Composite materials are expected to have a CV of at least 6%. The modified coefficient of variation (CV) method increases the measured coefficient of variation when it is below 8% prior to computing basis values. A higher CV will result in lower or more conservative basis values and lower specification limits. The use of the modified CV method is intended for a temporary period of time when there is minimal data available. When a sufficient number of production batches (approximately 8 to 15) have been produced and tested, the as-measured CV may be used so that the basis values and specification limits may be adjusted higher.

The material allowables in this report are calculated using both the as-measured CV and modified CV, so users have the choice of using either one. When the measured CV is greater than 8%, the modified CV method does not change the basis value. NCAMP recommended values make use of the modified CV method when it is appropriate for the data.

When the data fails the Anderson-Darling K-sample test for batch to batch variability or when the data fails the normality test, the modified CV method is not appropriate and no modified CV basis value will be provided. When the ANOVA method is used, it may produce excessively conservative basis values. When appropriate, a single batch or two batch estimate may be provided in addition to the ANOVA estimate.

In some cases a transformation of the data to fit the assumption of the modified CV resulted in the transformed data passing the ADK test and thus the data can be pooled only for the modified CV method.

NCAMP recommends that if a user decides to use the basis values that are calculated from asmeasured CV, the specification limits and control limits be calculated with as-measured CV also. Similarly, if a user decides to use the basis values that are calculated from modified CV, the specification limits and control limits be calculated with modified CV also. This will ensure that the link between material allowables, specification limits, and control limits is maintained.

# 2. Background

Statistical computations are performed with CMH17 STATS. Pooling across environments will be used whenever it is permissible according to CMH-17-1G guidelines. If pooling is not permissible, the results of a single point analysis provided by CMH17 STATS is included instead. If the data does not meet CMH-17-1G requirements for a single point analysis, estimates are created by a variety of methods depending on which is most appropriate for the dataset available. Specific procedures used are presented in the individual sections where the data is presented.

# 2.1 CMH17 STATS Statistical Formulas and Computations

This section contains the details of the specific formulas CMH17 STATS uses in its computations.

# 2.1.1 Basic Descriptive Statistics

The basic descriptive statistics shown are computed according to the usual formulas, which are shown below:

Mean:	$\overline{X} = \sum_{i=1}^{n} \frac{X_i}{n}$	Equation 1
Std. Dev.:	$S = \sqrt{\frac{1}{n-1}\sum_{i=1}^{n} \left(X_i - \overline{X}\right)^2}$	Equation 2
% Co. Variation:	$\frac{S}{\overline{X}} \times 100$	Equation 3

Where *n* refers to the number of specimens in the sample and  $X_i$  refers to the individual specimen measurements.

# 2.1.2 Statistics for Pooled Data

Prior to computing statistics for the pooled dataset, the data is normalized to a mean of one by dividing each value by the mean of all the data for that condition. This transformation does not affect the coefficients of variation for the individual conditions.

# 2.1.2.1 Pooled Standard Deviation

The formula to compute a pooled standard deviation is given below:

Pooled Std. Dev.: 
$$S_{p} = \sqrt{\frac{\sum_{i=1}^{k} (n_{i} - 1)S_{i}^{2}}{\sum_{i=1}^{k} (n_{i} - 1)}}$$
 Equation 4

Where k refers to the number of batches,  $S_i$  indicates the standard deviation of  $i^{th}$  sample, and  $n_i$  refers to the number of specimens in the  $i^{th}$  sample.

#### 2.1.2.2 Pooled Coefficient of Variation

Since the mean for the normalized data is 1.0 for each condition, the pooled normalized data also has a mean of one. The coefficient of variation for the pooled normalized data is the pooled standard deviation divided by the pooled mean, as in equation 3. Since the mean for the pooled normalized data is one, the pooled coefficient of variation is equal to the pooled standard deviation of the normalized data.

Pooled Coefficient of Variation = 
$$\frac{S_p}{1} = S_p$$
 Equation 5

#### 2.1.3 Basis Value Computations

Basis values are computed using the mean and standard deviation for that environment, as follows: The mean is always the mean for the environment, but if the data meets all requirements for pooling,  $S_p$  can be used in place of the standard deviation for the environment, S.

Basis Values:  

$$\begin{aligned} A-basis = \overline{X} - K_a S \\ B-basis = \overline{X} - K_b S \end{aligned}$$
Equation 6

#### 2.1.3.1 K-factor computations

 $K_a$  and  $K_b$  are computed according to the methodology documented in section 8.3.5 of CMH-17-1G. The approximation formulas are given below:

$$K_{a} = \frac{2.3263}{\sqrt{q(f)}} + \sqrt{\frac{1}{c_{A}(f) \cdot n_{j}}} + \left(\frac{b_{A}(f)}{2c_{A}(f)}\right)^{2}} - \frac{b_{A}(f)}{2c_{A}(f)}$$
Equation 7
$$K_{b} = \frac{1.2816}{\sqrt{q(f)}} + \sqrt{\frac{1}{c_{B}(f) \cdot n_{j}}} + \left(\frac{b_{B}(f)}{2c_{B}(f)}\right)^{2}} - \frac{b_{B}(f)}{2c_{B}(f)}$$
Equation 8

Where

r = the number of environments being pooled together  $n_i =$  number of data values for environment j

$$N = \sum_{j=1}^{r} n_j$$

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$$f = N - r$$

$$\begin{split} q(f) &= 1 - \frac{2.323}{\sqrt{f}} + \frac{1.064}{f} + \frac{0.9157}{f\sqrt{f}} - \frac{0.6530}{f^2} & \text{Equation 9} \\ b_B(f) &= \frac{1.1372}{\sqrt{f}} - \frac{0.49162}{f} + \frac{0.18612}{f\sqrt{f}} & \text{Equation 10} \\ c_B(f) &= 0.36961 + \frac{0.0040342}{\sqrt{f}} - \frac{0.71750}{f} + \frac{0.19693}{f\sqrt{f}} & \text{Equation 11} \\ b_A(f) &= \frac{2.0643}{\sqrt{f}} - \frac{0.95145}{f} + \frac{0.51251}{f\sqrt{f}} & \text{Equation 12} \\ c_A(f) &= 0.36961 + \frac{0.0026958}{\sqrt{f}} - \frac{0.65201}{f} + \frac{0.011320}{f\sqrt{f}} & \text{Equation 13} \end{split}$$

### 2.1.4 Modified Coefficient of Variation

The coefficient of variation is modified according to the following rules:

Modified CV = 
$$CV^* = \begin{cases} .06 & \text{if } CV < .04 \\ \frac{CV}{2} + .04 & \text{if } .04 \le CV < .08 \\ CV & \text{if } CV \ge .08 \end{cases}$$
 Equation 14

This is converted to percent by multiplying by 100%.

 $CV^*$  is used to compute a modified standard deviation  $S^*$ .

$$S^* = CV^* \cdot \overline{X}$$
 Equation 15

To compute the pooled standard deviation based on the modified CV:

$$S_{p}^{*} = \sqrt{\frac{\sum_{i=1}^{k} \left( (n_{i} - 1) \left( CV_{i}^{*} \cdot \overline{X}_{i} \right)^{2} \right)}{\sum_{i=1}^{k} (n_{i} - 1)}}$$
Equation 16

The A-basis and B-basis values under the assumption of the modified CV method are computed by replacing S with  $S^*$ 

### 2.1.4.1 Transformation of data based on Modified CV

In order to determine if the data would pass the diagnostic tests under the assumption of the modified CV, the data must be transformed such that the batch means remain the same while the standard deviation of transformed data (all batches) matches the modified standard deviation.

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To accomplish this requires a transformation in two steps:

Step 1: Apply the modified CV rules to each batch and compute the modified standard deviation  $S_i^* = CV^* \cdot \overline{X}_i$  for each batch. Transform the individual data values ( $X_{ij}$ ) in each batch as follows:

$$X'_{ij} = C_i \left( X_{ij} - \overline{X}_i \right) + \overline{X}_i$$
 Equation 17  
$$C_i = \frac{S_i^*}{S_i}$$
 Equation 18

Run the Anderson-Darling k-sample test for batch equivalence (see section 2.1.6) on the transformed data. If it passes, proceed to step 2. If not, stop. The data cannot be pooled.

Step 2: Another transformation is needed as applying the modified CV to each batch leads to a larger CV for the combined data than when applying the modified CV rules to the combined data (due to the addition of between batch variation when combining data from multiple batches). In order to alter the data to match  $S^*$ , the transformed data is transformed again, this time setting using the same value of C' for all batches.

$$X_{ij}'' = C' \left( X_{ij}' - \overline{X}_i \right) + \overline{X}_i$$
Equation 19  

$$C' = \sqrt{\frac{SSE^*}{SSE'}}$$
Equation 20  

$$SSE^* = (n-1) \left( CV^* \cdot \overline{X} \right)^2 - \sum_{i=1}^k n_i \left( \overline{X}_i - \overline{X} \right)^2$$
Equation 21  

$$SSE' = \sum_{i=1}^k \sum_{j=1}^{n_i} \left( X_{ij}' - \overline{X}_i \right)^2$$
Equation 22

Once this second transformation has been completed, the k-sample Anderson Darling test for batch equivalence can be run on the transformed data to determine if the modified co-efficient of variation will permit pooling of the data.

### 2.1.5 Determination of Outliers

All outliers are identified in text and graphics. If an outlier is removed from the dataset, it will be specified and the reason why will be documented in the text. Outliers are identified using the Maximum Normed Residual Test for Outliers as specified in section 8.3.3 of CMH-17-1G.

$$MNR = \frac{\max_{all i} |X_i - \overline{X}|}{S}, i = 1...n$$
 Equation 23  
$$C = \frac{n-1}{\sqrt{n}} \sqrt{\frac{t^2}{n-2+t^2}}$$
 Equation 24

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where t is the  $1-\frac{.05}{2n}$  quartile of a t distribution with n-2 degrees of freedom, n being the total number of data values.

If MNR > C, then the  $X_i$  associated with the MNR is considered to be an outlier. If an outlier exists, then the  $X_i$  associated with the MNR is dropped from the dataset and the MNR procedure is applied again. This process is repeated until no outliers are detected. Additional information on this procedure can be found in references 1 and 2.

### 2.1.6 The k-Sample Anderson Darling Test for Batch Equivalency

The k-sample Anderson-Darling test is a nonparametric statistical procedure that tests the hypothesis that the populations from which two or more groups of data were drawn are identical. The distinct values in the combined data set are ordered from smallest to largest, denoted  $z_{(1)}$ ,  $z_{(2)}$ , ...,  $z_{(L)}$ , where *L* will be less than n if there are tied observations. These rankings are used to compute the test statistic.

The k-sample Anderson-Darling test statistic is:

$$ADK = \frac{n-1}{n^{2}(k-1)} \sum_{i=1}^{k} \left[ \frac{1}{n_{i}} \sum_{j=1}^{L} h_{j} \frac{\left(nF_{ij} - n_{i}H_{j}\right)^{2}}{H_{j}\left(n - H_{j}\right) - \frac{nh_{j}}{4}} \right]$$
 Equation 25

Where

 $n_i$  = the number of test specimens in each batch

 $n = n_1 + n_2 + \ldots + n_k$ 

 $h_j$  = the number of values in the combined samples equal to  $z_{(j)}$ 

 $H_j$  = the number of values in the combined samples less than  $z_{(j)}$  plus  $\frac{1}{2}$  the number of values in the combined samples equal to  $z_{(j)}$ 

 $F_{ij}$  = the number of values in the *i*<sup>th</sup> group which are less than  $z_{(j)}$  plus  $\frac{1}{2}$  the number of values in this group which are equal to  $z_{(j)}$ .

The critical value for the test statistic at  $1-\alpha$  level is computed:

$$ADC = 1 + \sigma_n \left[ z_\alpha + \frac{0.678}{\sqrt{k-1}} - \frac{0.362}{k-1} \right]$$
 Equation 26

This formula is based on the formula in reference 3 at the end of section 5, using a Taylor's expansion to estimate the critical value via the normal distribution rather than using the t distribution with k-1 degrees of freedom.

$$\sigma_n^2 = VAR(ADK) = \frac{an^3 + bn^2 + cn + d}{(n-1)(n-2)(n-3)(k-1)^2}$$
 Equation 27

With

$$a = (4g - 6)(k - 1) + (10 - 6g)S$$
  

$$b = (2g - 4)k^{2} + 8Tk + (2g - 14T - 4)S - 8T + 4g - 6$$
  

$$c = (6T + 2g - 2)k^{2} + (4T - 4g + 6)k + (2T - 6)S + 4T$$
  

$$d = (2T + 6)k^{2} - 4Tk$$
  

$$S = \sum_{i=1}^{k} \frac{1}{n_{i}}$$
  

$$T = \sum_{i=1}^{n-1} \frac{1}{i}$$
  

$$g = \sum_{i=1}^{n-2} \sum_{j=i+1}^{n-1} \frac{1}{(n-i)j}$$

The data is considered to have failed this test (i.e. the batches are not from the same population) when the test statistic is greater than the critical value. For more information on this procedure, see reference 3.

#### 2.1.7 The Anderson Darling Test for Normality

**Normal Distribution:** A two parameter  $(\mu, \sigma)$  family of probability distributions for which the probability that an observation will fall between *a* and *b* is given by the area under the curve between a and b:

 $F(x) = \int_{a}^{b} \frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{(x-\mu)^{2}}{2\sigma^{2}}} dx$  Equation 28

A normal distribution with parameters ( $\mu$ ,  $\sigma$ ) has population mean  $\mu$  and variance  $\sigma^2$ .

The normal distribution is considered by comparing the cumulative normal distribution function that best fits the data with the cumulative distribution function of the data. Let

$$z_{(i)} = \frac{x_{(i)} - \overline{x}}{s}$$
, for i = 1,...,n Equation 29

where  $x_{(i)}$  is the smallest sample observation,  $\overline{x}$  is the sample average, and s is the sample standard deviation.

The Anderson Darling test statistic (AD) is:

$$AD = \sum_{i=1}^{n} \frac{1-2i}{n} \left\{ \ln \left[ F_0(z_{(i)}) \right] + \ln \left[ 1 - F_0(z_{(n+1-i)}) \right] \right\} - n$$
 Equation 30

Where  $F_0$  is the standard normal distribution function. The observed significance level (OSL) is

$$OSL = \frac{1}{1 + e^{-0.48 + 0.78 \ln(AD^*) + 4.58 AD^*}}, \quad AD^* = \left(1 + \frac{4}{n} - \frac{25}{n^2}\right) AD \quad \text{Equation 31}$$

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This OSL measures the probability of observing an Anderson-Darling statistic at least as extreme as the value calculated if, in fact, the data are a sample from a normal population. If OSL > 0.05, the data is considered sufficiently close to a normal distribution.

# 2.1.8 Levene's Test for Equality of Coefficient of Variation

Levene's test performs an Analysis of Variance on the absolute deviations from their sample medians. The absolute value of the deviation from the median is computed for each data value.  $w_{ij} = |y_{ij} - \tilde{y}_i|$  An F-test is then performed on the transformed data values as follows:

$$F = \frac{\sum_{i=1}^{k} n_i \left( \overline{w}_i - \overline{w} \right)^2 / (k-1)}{\sum_{i=1}^{k} \sum_{j=1}^{n_i} i \left( w_{ij} - \overline{w}_i \right)^2 / (n-k)}$$

Equation 32

If this computed F statistic is less than the critical value for the F-distribution having k-1 numerator and n-k denominator degrees of freedom at the 1- $\alpha$  level of confidence, then the data is not rejected as being too different in terms of the co-efficient of variation. CMH-17 STATS provides the appropriate critical values for F at  $\alpha$  levels of 0.10, 0.05, 0.025, and 0.01. For more information on this procedure, see references 4, and 5.

# 2.1.9 Distribution Tests

In addition to testing for normality using the Anderson-Darling test (see 2.1.7), CMH17 STATS also tests to see if the Weibull or Lognormal distribution is a good fit for the data.

Each distribution is considered using the Anderson-Darling test statistic which is sensitive to discrepancies in the tail regions. The Anderson-Darling test compares the cumulative distribution function for the distribution of interest with the cumulative distribution function of the data.

An observed significance level (OSL) based on the Anderson-Darling test statistic is computed for each test. The OSL measures the probability of observing an Anderson-Darling test statistic at least as extreme as the value calculated if the distribution under consideration is in fact the underlying distribution of the data. In other words, the OSL is the probability of obtaining a value of the test statistic at least as large as that obtained if the hypothesis that the data are actually from the distribution being tested is true. If the OSL is less than or equal to 0.05, then the assumption that the data are from the distribution being tested is rejected with at most a five percent risk of being in error.

If the normal distribution has an OSL greater than 0.05, then the data is assumed to be from a population with a normal distribution. If not, then if either the Weibull or lognormal distributions has an OSL greater than 0.05, then one of those can be used. If neither of these distributions has an OSL greater than 0.05, a non-parametric approach is used.

In what follows, unless otherwise noted, the sample size is denoted by n, the sample observations by  $x_1, ..., x_n$ , and the sample observations ordered from least to greatest by  $x_{(1)}, ..., x_{(n)}$ .

# 2.1.9.1 One-sided B-basis tolerance factors, k<sub>B</sub>, for the normal distribution when sample size is greater than 15.

The exact computation of k<sub>B</sub> values is  $1/\sqrt{n}$  times the 0.95th quantile of the noncentral t-distribution with noncentrality parameter  $1.282\sqrt{n}$  and n – 1 degrees of freedom. Since this in not a calculation that Excel can handle, the following approximation to the k<sub>B</sub> values is used:

$$k_B \approx 1.282 + \exp\{0.958 - 0.520\ln(n) + 3.19/n\}$$
 Equation 33

This approximation is accurate to within 0.2% of the tabulated values for sample sizes greater than or equal to 16.

### 2.1.9.2 One-sided A-basis tolerance factors, kA, for the normal distribution

The exact computation of  $k_A$  values is  $1/\sqrt{n}$  times the 0.95th quantile of the noncentral t-distribution with noncentrality parameter  $2.326\sqrt{n}$  and n - 1 degrees of freedom (Reference 11). Since this is not a calculation that Excel can handle easily, the following approximation to the  $k_A$  values is used:

$$k_A \approx 2.326 + \exp\{1.34 - 0.522\ln(n) + 3.87/n\}$$
 Equation 34

This approximation is accurate to within 0.2% of the tabulated values for sample sizes greater than or equal to 16.

### 2.1.9.3 Two-parameter Weibull Distribution

A probability distribution for which the probability that a randomly selected observation from this population lies between *a* and *b*  $(0 < a < b < \infty)$  is given by

$$e^{-\left(\frac{a}{\alpha}\right)^{\beta}} - e^{-\left(\frac{b}{\alpha}\right)^{\beta}}$$
 Equation 35

where  $\alpha$  is called the scale parameter and  $\beta$  is called the shape parameter.

In order to compute a check of the fit of a data set to the Weibull distribution and compute basis values assuming Weibull, it is first necessary to obtain estimates of the population shape and scale parameters (Section 2.1.9.3.1). Calculations specific to the goodness-of-fit test for the Weibull distribution are provided in section 2.1.9.3.2.

### 2.1.9.3.1 Estimating Weibull Parameters

This section describes the *maximum likelihood* method for estimating the parameters of the twoparameter Weibull distribution. The maximum-likelihood estimates of the shape and scale parameters are denoted  $\hat{\beta}$  and  $\hat{\alpha}$ . The estimates are the solution to the pair of equations:

$$\hat{\alpha}\hat{\beta}n - \frac{\hat{\beta}}{\hat{\alpha}\hat{\beta}-1}\sum_{i=1}^{n} x_{i}^{\hat{\beta}} = 0$$
Equation 36
$$\frac{n}{\hat{\beta}} - n\ln\hat{\alpha} + \sum_{i=1}^{n} \ln x_{i} - \sum_{i=1}^{n} \left[\frac{x_{i}}{\hat{\alpha}}\right]^{\hat{\beta}} \left(\ln x_{i} - \ln\hat{\alpha}\right) = 0$$
Equation 37

CMH17 STATS solves these equations numerically for  $\hat{\beta}$  and  $\hat{\alpha}$  in order to compute basis values.

### 2.1.9.3.2 Goodness-of-fit test for the Weibull distribution

The two-parameter Weibull distribution is considered by comparing the cumulative Weibull distribution function that best fits the data with the cumulative distribution function of the data. Using the shape and scale parameter estimates from section 2.1.9.3.1, let

$$z_{(i)} = \left[ x_{(i)} / \hat{\alpha} \right]^{\beta}$$
, for  $i = 1, ..., n$  Equation 38

The Anderson-Darling test statistic is

$$AD = \sum_{i=1}^{n} \frac{1-2i}{n} \left[ \ln \left[ 1 - \exp(-z_{(i)}) \right] - z_{(n+1-i)} \right] - n$$
 Equation 39

and the observed significance level is

$$OSL = 1/\{1 + exp[-0.10 + 1.24 \ln(AD^*) + 4.48 AD^*]\}$$
 Equation 40

where

$$AD^* = \left(1 + \frac{0.2}{\sqrt{n}}\right)AD$$
 Equation 41

This OSL measures the probability of observing an Anderson-Darling statistic at least as extreme as the value calculated if in fact the data is a sample from a two-parameter Weibull distribution. If OSL  $\leq 0.05$ , one may conclude (at a five percent risk of being in error) that the population does not have a two-parameter Weibull distribution. Otherwise, the hypothesis that the population has a two-parameter Weibull distribution is not rejected. For further information on these procedures, see reference 6.

### 2.1.9.3.3 Basis value calculations for the Weibull distribution

For the two-parameter Weibull distribution, the B-basis value is

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$$B = \hat{q}e^{\left(\frac{-V/\hat{\beta}\sqrt{n}}{\hat{\beta}\sqrt{n}}\right)}$$
 Equation 42

where

$$\hat{q} = \hat{\alpha} \left( 0.10536 \right)^{\frac{1}{\hat{\beta}}}$$
 Equation 43

To calculate the A-basis value, substitute the equation below for the equation above.

 $\hat{q} = \hat{\alpha} (0.01005)^{1/\beta}$  Equation 44

V is the value in Table 2-1 when the sample size is less than 16. For sample sizes of 16 or larger, a numerical approximation to the V values is given in the two equations immediately below.

$$V_{B} \approx 3.803 + \exp\left[1.79 - 0.516\ln(n) + \frac{5.1}{n-1}\right]$$
 Equation 45  
$$V_{A} \approx 6.649 + \exp\left[2.55 - 0.526\ln(n) + \frac{4.76}{n}\right]$$
 Equation 46

This approximation is accurate within 0.5% of the tabulated values for n greater than or equal to 16.

Weibull Dist. K Factors for N<16		
N	B-basis	A-basis
2	690.804	1284.895
3	47.318	88.011
4	19.836	36.895
5	13.145	24.45
6	10.392	19.329
7	8.937	16.623
8	8.047	14.967
9	7.449	13.855
10	6.711	12.573
11	6.477	12.093
12	6.286	11.701
13	6.127	11.375
14	5.992	11.098
15	5.875	10.861

Table 2-1: Weibull Distribution Basis Value Factors

### 2.1.9.4 Lognormal Distribution

A probability distribution for which the probability that an observation selected at random from this population falls between a and b  $(0 < a < b < \infty)$  is given by the area under the normal distribution between ln(a) and ln(b).

The lognormal distribution is a positively skewed distribution that is simply related to the normal distribution. If something is lognormally distributed, then its logarithm is normally distributed. The natural (base e) logarithm is used.

## 2.1.9.4.1 Goodness-of-fit test for the Lognormal distribution

In order to test the goodness-of-fit of the lognormal distribution, take the logarithm of the data and perform the Anderson-Darling test for normality from Section 2.1.7. Using the natural logarithm, replace Equation 29 above with Equation 47 below:

$$z_{(i)} = \frac{\ln(x_{(i)}) - \overline{x}_L}{s_L}, \quad \text{for } i = 1, \dots, n$$
 Equation 47

where  $x_{(i)}$  is the i<sup>th</sup> smallest sample observation,  $\overline{x}_L$  and  $s_L$  are the mean and standard deviation of the ln( $x_i$ ) values.

The Anderson-Darling statistic is then computed using Equation 30 above and the observed significance level (OSL) is computed using Equation 31 above. This OSL measures the probability of observing an Anderson-Darling statistic at least as extreme as the value calculated if in fact the data are a sample from a lognormal distribution. If OSL  $\leq 0.05$ , one may conclude (at a five percent risk of being in error) that the population is not lognormally distributed. Otherwise, the hypothesis that the population is lognormally distributed is not rejected. For further information on these procedures, see reference 6.

# 2.1.9.4.2 Basis value calculations for the Lognormal distribution

If the data set is assumed to be from a population with a lognormal distribution, basis values are calculated using the equation above in section 2.1.3. However, the calculations are performed using the logarithms of the data rather than the original observations. The computed basis values are then transformed back to the original units by applying the inverse of the log transformation.

# 2.1.10 Non-parametric Basis Values

Non-parametric techniques do not assume any particularly underlying distribution for the population the sample comes from. It does require that the batches be similar enough to be grouped together, so the ADK test must have a positive result. While it can be used instead of assuming the normal, lognormal or Weibull distribution, it typically results in lower basis values. One of following two methods should be used, depending on the sample size.

# 2.1.10.1 Non-parametric Basis Values for large samples

The required sample sizes for this ranking method differ for A and B basis values. A sample size of at least 29 is needed for the B-basis value while a sample size of 299 is required for the A-basis.

To calculate a B-basis value for n > 28, the value of r is determined with the following formulas:

For B-basis values:

$$r_{B} = \frac{n}{10} - 1.645\sqrt{\frac{9n}{100}} + 0.23$$

Equation 48

For A-Basis values:

Equation 50

Equation 51

$$r_A = \frac{n}{100} - 1.645 \sqrt{\frac{99n}{10,000}} + 0.29 + \frac{19.1}{n}$$
 Equation 49

The formula for the A-basis values should be rounded to the nearest integer. This approximation is exact for most values and for a small percentage of values (less than 0.2%), the approximation errs by one rank on the conservative side.

The B-basis value is the  $r_B$ <sup>th</sup> lowest observation in the data set, while the A-basis value is the  $r_A$ <sup>th</sup> lowest observation in the data set. For example, in a sample of size n = 30, the lowest (r = 1) observation is the B-basis value. Further information on this procedure may be found in reference 7.

### 2.1.10.2 Non-parametric Basis Values for small samples

The Hanson-Koopmans method (references 8 and 9) is used for obtaining a B-basis value for sample sizes not exceeding 28 and A-basis values for sample sizes less than 299. This procedure requires the assumption that the observations are a random sample from a population for which the logarithm of the cumulative distribution function is concave, an assumption satisfied by a large class of probability distributions. There is substantial empirical evidence that suggests that composite strength data satisfies this assumption.

The Hanson-Koopmans B-basis value is:

$$B = x_{(r)} \left[ \frac{x_{(1)}}{x_{(r)}} \right]^k$$

The A-basis value is:

$$A = x_{(n)} \left[ \frac{x_{(1)}}{x_{(n)}} \right]^k$$

where  $x_{(n)}$  is the largest data value,  $x_{(1)}$  is the smallest, and  $x_{(r)}$  is the r<sup>th</sup> largest data value. The values of r and k depend on n and are listed in Table 2-2. This method is not used for the B-basis value when  $x_{(r)} = x_{(1)}$ .

The Hanson-Koopmans method can be used to calculate A-basis values for n less than 299. Find the value  $k_A$  corresponding to the sample size n in Table 2-3. For an A-basis value that meets all the requirements of CMH-17-1G, there must be at least five batches represented in the data and at least 55 data points. For a B-basis value, there must be at least three batches represented in the data and at least 18 data points.

B-Basis Hanson-Koopmans Table			
n	r	k	
2	2	35.177	
3	3	7.859	
4	4	4.505	
5	4 5 5 6	4.101	
6	5	3.064	
7	5	2.858	
8		2.382	
9	6 6	2.253	
10		2.137	
11	7 7 7	1.897	
12	7	1.814	
13		1.738	
14	8	1.599	
15	8	1.540	
16	8	1.485	
17	8	1.434 1.354	
18	9	1.354	
19	9	1.311 1.253	
20	10	1.253	
21	10	1.218	
22	10	1.184	
23	11	1.143	
24	11	1.114	
25	11	1.087	
26	11	1.060	
27	11	1.035	
28	12	1.010	

Table 2-2: B-Basis Hanson-Koopmans Table

<b></b>	A-Basis	Hanson-	Koopmans	Table	
n	k	n	k	n	k
2	80.00380	38	1.79301	96	1.32324
3	16.91220	39	1.77546	98	1.31553
4	9.49579	40	1.75868	100	1.30806
5	6.89049	41	1.74260	105	1.29036
6	5.57681	42	1.72718	110	1.27392
7	4.78352	43	1.71239	115	1.25859
8	4.25011	44	1.69817	120	1.24425
9	3.86502	45	1.68449	125	1.23080
10	3.57267	46	1.67132	130	1.21814
11	3.34227	47	1.65862	135	1.20620
12	3.15540	48	1.64638	140	1.19491
13	3.00033	49	1.63456	145	1.18421
14	2.86924	50	1.62313	150	1.17406
15	2.75672	52	1.60139	155	1.16440
16	2.65889	54	1.58101	160	1.15519
17	2.57290	56	1.56184	165	1.14640
18	2.49660	58	1.54377	170	1.13801
19	2.42833	60	1.52670	175	1.12997
20	2.36683	62	1.51053	180	1.12226
21	2.31106	64	1.49520	185	1.11486
22	2.26020	66	1.48063	190	1.10776
23	2.21359	68	1.46675	195	1.10092
24	2.17067	70	1.45352	200	1.09434
25	2.13100	72	1.44089	205	1.08799
26	2.09419	74	1.42881	210	1.08187
27	2.05991	76	1.41724	215	1.07595
28	2.02790	78	1.40614	220	1.07024
29	1.99791	80	1.39549	225	1.06471
30	1.96975	82	1.38525	230	1.05935
31	1.94324	84	1.37541	235	1.05417
32	1.91822	86	1.36592	240	1.04914
33	1.89457	88	1.35678	245	1.04426
34	1.87215	90	1.34796	250	1.03952
35	1.85088	92	1.33944	275	1.01773
36	1.83065	94	1.33120	299	1.00000
37	1.81139				

### 2.1.11 Analysis of Variance (ANOVA) Basis Values

ANOVA is used to compute basis values when the batch to batch variability of the data does not pass the ADK test. Since ANOVA makes the assumption that the different batches have equal variances, the data is checked to make sure the assumption is valid. Levene's test for equality of variance is used (see section 2.1.8). If the dataset fails Levene's test, the basis values computed are likely to be conservative. Thus this method can still be used but the values produced will be listed as estimates.

Equation 58

### 2.1.11.1 Calculation of basis values using ANOVA

The following calculations address batch-to-batch variability. In other words, the only grouping is due to batches and the k-sample Anderson-Darling test (Section 2.1.6) indicates that the batch to batch variability is too large to pool the data. The method is based on the one-way analysis of variance random-effects model, and the procedure is documented in reference 10.

ANOVA separates the total variation (called the sum of squares) of the data into two sources: between batch variation and within batch variation.

First, statistics are computed for each batch, which are indicated with a subscript  $(n_i, \bar{x}_i, s_i^2)$  while statistics that were computed with the entire dataset do not have a subscript. Individual data values are represented with a double subscript, the first number indicated the batch and the second distinguishing between the individual data values within the batch. *k* stands for the number of batches in the analysis. With these statistics, the Sum of Squares Between batches (SSB) and the Total Sum of Squares (SST) are computed:

$$SSB = \sum_{i=1}^{k} n_i \overline{x}_i^2 - n \overline{x}^2$$
Equation 52
$$SST = \sum_{i=1}^{k} \sum_{j=1}^{n_i} x_{ij}^2 - n \overline{x}^2$$
Equation 53

The within-batch, or error, sum of squares (SSE) is computed by subtraction

Next, the mean sums of squares are computed:

$$MSB = \frac{SSB}{k-1}$$
Equation 55  
$$MSE = \frac{SSE}{n-k}$$
Equation 56

Since the batches need not have equal numbers of specimens, an 'effective batch size,' is defined as

$$n' = \frac{n - \frac{1}{n} \sum_{i=1}^{k} n_i^2}{k - 1}$$
 Equation 57

Using the two mean squares and the effective batch size, an estimate of the population standard deviation is computed:

$$S = \sqrt{\frac{MSB}{n'} + \left(\frac{n'-1}{n'}\right)MSE}$$

Two k-factors are computed using the methodology of section 8.3.5 of CMH-17-1G using a sample size of n (denoted  $k_0$ ) and a sample size of k (denoted  $k_1$ ). Whether this value is an A- or B-basis value depends only on whether  $k_0$  and  $k_1$  are computed for A or B-basis values.

Denote the ratio of mean squares by

$$u = \frac{MSB}{MSE}$$
 Equation 59

If u is less than one, it is set equal to one. The tolerance limit factor is

 $T = \frac{k_0 - \frac{k_1}{\sqrt{n'}} + (k_1 - k_0)\sqrt{\frac{u}{u + n' - 1}}}{1 - \frac{1}{\sqrt{n'}}}$ Equation 60

The basis value is  $\overline{x} - TS$ .

The ANOVA method can produce extremely conservative basis values when a small number of batches are available. Therefore, when less than five (5) batches are available and the ANOVA method is used, the basis values produced will be listed as estimates.

#### 2.2 Single Batch and Two Batch Estimates using Modified CV

This method has not been approved for use by the CMH-17 organization. Values computed in this manner are estimates only. It is used only when fewer than three batches are available and no valid B-basis value could be computed using any other method. The estimate is made using the mean of the data and setting the coefficient of variation to 8 percent if it was less than that. A modified standard deviation (S<sub>adi</sub>) was computed by multiplying the mean by 0.08 and computing the A and B-basis values using this inflated value for the standard deviation.

### Estimated B-Basis = $\overline{X} - k_b S_{adj} = \overline{X} - k_b \cdot 0.08 \cdot \overline{X}$ Equation 61

# 2.3 Lamina Variability Method (LVM)

This method has not been approved for use by the CMH-17 organization. Values computed in this manner are estimates only. It is used only when the sample size is less than 16 and no valid B-basis value could be computed using any other method. The prime assumption for applying the LVM is that the intrinsic strength variability of the laminate (small) dataset is no greater than the strength variability of the lamina (large) dataset. This assumption was tested and found to be reasonable for composite materials as documented by Tomblin and Seneviratne [12].

To compute the estimate, the coefficients of variation (CVs) of laminate data are paired with lamina CV's for the same loading condition and environmental condition. For example, the 0° compression lamina CV CTD condition is used with open hole compression CTD condition. Bearing and in-plane shear laminate CV's are paired with 0° compression lamina CV's.

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However, if the laminate CV is larger than the corresponding lamina CV, the larger laminate CV value is used.

The LVM B-basis value is then computed as:

LVM Estimated B-Basis = 
$$\overline{X}_1 - K_{(N_1,N_2)} \cdot \overline{X}_1 \cdot \max(CV_1, CV_2)$$
 Equation 62

When used in conjunction with the modified CV approach, a minimum value of 8% is used for the CV.

Mod CV LVM Estimated B-Basis = 
$$\overline{X}_1 - K_{(N_1,N_2)} \cdot \overline{X}_1 \cdot Max(8\%, CV_1, CV_2)$$
 Equation 63

With:

 $\overline{X}_1$  the mean of the laminate (small dataset) N<sub>1</sub> the sample size of the laminate (small dataset) N<sub>2</sub> the sample size of the lamina (large dataset) CV<sub>1</sub> is the coefficient of variation of the laminate (small dataset) CV<sub>2</sub> is the coefficient of variation of the lamina (large dataset)  $K_{(N_1,N_2)}$  is given in Table 2-4

		N1													
		2	3	4	5	6	7	8	9	10	11	12	13	14	15
	2	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	3	4.508	0	0	0	0	0	0	0	0	0	0	0	0	0
	4	3.827	3.607	0	0	0	0	0	0	0	0	0	0	0	0
	5	3.481	3.263	3.141	0	0	0	0	0	0	0	0	0	0	0
	6	3.273	3.056	2.934	2.854	0	0	0	0	0	0	0	0	0	0
	7	3.134	2.918	2.796	2.715	2.658	0	0	0	0	0	0	0	0	0
	8	3.035	2.820	2.697	2.616	2.558	2.515	0	0	0	0	0	0	0	0
	9	2.960	2.746	2.623	2.541	2.483	2.440	2.405	0	0	0	0	0	0	0
	10	2.903	2.688	2.565	2.484	2.425	2.381	2.346	2.318	0	0	0	0	0	0
	11	2.856	2.643	2.519	2.437	2.378	2.334	2.299	2.270	2.247	0	0	0	0	0
	12	2.819	2.605	2.481	2.399	2.340	2.295	2.260	2.231	2.207	2.187	0	0	0	0
	13	2.787	2.574	2.450	2.367	2.308	2.263	2.227	2.198	2.174	2.154	2.137	0	0	0
	14	2.761	2.547	2.423	2.341	2.281	2.236	2.200	2.171	2.147	2.126	2.109	2.093	0	0
	15	2.738	2.525	2.401	2.318	2.258	2.212	2.176	2.147	2.123	2.102	2.084	2.069	2.056	0
	16	2.719	2.505	2.381	2.298	2.238	2.192	2.156	2.126	2.102	2.081	2.063	2.048	2.034	2.022
	17	2.701	2.488	2.364	2.280	2.220	2.174	2.138	2.108	2.083	2.062	2.045	2.029	2.015	2.003
	18	2.686	2.473	2.348	2.265	2.204	2.158	2.122	2.092	2.067	2.046	2.028	2.012	1.999	1.986
	19	2.673	2.459	2.335	2.251	2.191	2.144	2.108	2.078	2.053	2.032	2.013	1.998	1.984	1.971
	20	2.661	2.447	2.323	2.239	2.178	2.132	2.095	2.065	2.040	2.019	2.000	1.984	1.970	1.958
N1+N2-2	21	2.650	2.437	2.312	2.228	2.167	2.121	2.084	2.053	2.028	2.007	1.988	1.972	1.958	1.946
	22	2.640	2.427	2.302	2.218	2.157	2.110	2.073	2.043	2.018	1.996	1.978	1.962	1.947	1.935
	23	2.631	2.418	2.293	2.209	2.148	2.101	2.064	2.033	2.008	1.987	1.968	1.952	1.938	1.925
	24	2.623	2.410	2.285	2.201	2.139	2.092	2.055	2.025	1.999	1.978	1.959	1.943	1.928	1.916
	25	2.616	2.402	2.277	2.193	2.132	2.085	2.047	2.017	1.991	1.969	1.951	1.934	1.920	1.907
	26	2.609	2.396	2.270	2.186	2.125	2.078	2.040	2.009	1.984	1.962	1.943	1.927	1.912	1.900
	27	2.602	2.389	2.264	2.180	2.118	2.071	2.033	2.003	1.977	1.955	1.936	1.920	1.905	1.892
	28	2.597	2.383	2.258	2.174	2.112	2.065	2.027	1.996	1.971	1.949	1.930	1.913	1.899	1.886
	29	2.591	2.378	2.252	2.168	2.106	2.059	2.021	1.990	1.965	1.943	1.924	1.907	1.893	1.880
	30	2.586	2.373	2.247	2.163	2.101	2.054	2.016	1.985	1.959	1.937	1.918	1.901	1.887	1.874
	40	2.550	2.337	2.211	2.126	2.063	2.015	1.977	1.946	1.919	1.897	1.877	1.860	1.845	1.832
	50	2.528	2.315	2.189	2.104	2.041	1.993	1.954	1.922	1.896	1.873	1.853	1.836	1.820	1.807
	60	2.514	2.301	2.175	2.089	2.026	1.978	1.939	1.907	1.880	1.857	1.837	1.819	1.804	1.790
	70	2.504	2.291	2.164	2.079	2.016	1.967	1.928	1.896	1.869	1.846	1.825	1.808	1.792	1.778
	80	2.496	2.283	2.157	2.071	2.008	1.959	1.920	1.887	1.860	1.837	1.817	1.799	1.783	1.769
	90	2.491	2.277	2.151	2.065	2.002	1.953	1.913	1.881	1.854	1.830	1.810	1.792	1.776	1.762
	100	2.486	2.273	2.146	2.060	1.997	1.948	1.908	1.876	1.849	1.825	1.805	1.787	1.771	1.757
	125	2.478	2.264	2.138	2.051	1.988	1.939	1.899	1.867	1.839	1.816	1.795	1.777	1.761	1.747
	150	2.472	2.259	2.132	2.046	1.982	1.933	1.893	1.861	1.833	1.809	1.789	1.770	1.754	1.740
	175	2.468	2.255	2.128	2.042	1.978	1.929	1.889	1.856	1.828	1.805	1.784	1.766	1.750	1.735
	200	2.465	2.252	2.125	2.039	1.975	1.925	1.886	1.853	1.825	1.801	1.781	1.762	1.746	1.732

Table 2-4: B-Basis Factors for Small Datasets Using Variability of Corresponding Large Dataset

# 3. Summary of Results

The basis values for all tests are summarized in the following tables. The NCAMP recommended B-basis values meet all requirements of CMH-17-1G. However, not all test data meets those requirements. The summary tables provide a complete listing of all computed basis values and estimates of basis values. Data that does not meet the requirements of CMH-17-1G are shown in shaded boxes and labeled as estimates. Basis values computed with the modified coefficient of variation (CV) are presented whenever possible. Basis values and estimates computed without that modification are presented for all tests.

# 3.1 NCAMP Recommended B-basis Values

The following rules are used in determining what B-basis value, if any, is included in tables Table 3-1 and Table 3-2 of recommended values.

- 1. Recommended values are NEVER estimates. Only B-basis values that meet all requirements of CMH-17-1G are recommended.
- 2. Modified CV basis values are preferred. Recommended values will be the modified CV basis value when available. The CV provided with the recommended basis value will be the one used in the computation of the basis value.
- 3. Only normalized basis values are given for properties that are normalized.
- 4. ANOVA B-basis values are not recommended since only three batches of material are available and CMH-17-1G recommends that no less than five batches be used when computing basis values with the ANOVA method.
- 5. Basis values of 90% or more of the mean value imply that the CV is unusually low and may not be conservative. Caution is recommended with B-Basis values calculated from CMH-17 STATS when the B-basis value is 90% or more of the average value. Such values will be indicated.
- 6. If the data appear questionable (e.g. when the CTD-RTD-ETW trend of the basis values is not consistent with the CTD-RTD-ETW trend of the average values), then the B-basis values will not be recommended.

			Recommen									
	Renegade RM-2014-LDk-Tk 45818 8HS Quartz Fabric 286 gs 38% RC All B-basis values in this table meet the standards for publication in CMH-17-1G Handbook											
An B-basis values in this table meet the standards for publication in CMH-17-1G Handbook Values are for normalized data unless noted												
		values a			unicos nou	.u						
			Lamina S	trength Tes	ts							
Environment Statistic WT WC FT FC IPS* SBS*												
Environment	Statistic	** 1	we	r I	re	0.2% Offset	5% Strain	303				
	<b>B</b> -basis	111.1	72.21	NA: A	59.98	4.951	8.936	8.602				
CTD (-65°F)	Mean	122.2	79.16	102.4	66.02	5.616	9.901	9.467				
	CV	6.000	6.728	7.550	6.000	6.000	6.000	6.000				
RTD (70°F)	<b>B</b> -basis	97.07	61.72	82.41	52.28	3.822	6.657	7.773				
	Mean	108.1	68.67	93.33	58.33	4.335	7.622	8.638				
	CV	6.000	6.037	6.000	6.000	6.000	6.000	6.000				
	<b>B</b> -basis	99.88	48.23	NA: A	38.32	2.468	NA: A	5.018				
ETD (212°F)	Mean	110.9	55.18	90.63	44.36	2.791	4.923	5.883				
	CV	6.000	6.982	8.318	6.597	6.000	6.939	6.000				
	<b>B</b> -basis	63.70	34.83	NA: A	24.85	1.428	2.139	3.017				
ETW (212°F)	Mean	74.75	41.57	63.12	30.73	1.653	2.527	3.447				
	CV	6.000	6.486	12.73	11.22	7.139	7.781	6.321				
	fied CV B-basis				e.							
1	-			0	recommen	ded requirements						
	indicates ANOV						-					
	as measured rat											

# Table 3-1: NCAMP Recommended B-Basis Values for Lamina Test Data

#### NCAMP Recommended B-basis Values for Renegade RM-2014-LDk-Tk 45818 8HS Quartz Fabric 286 gs 38% RC All B-basis values in this table meet the standards for publication in CMH-17-1G Handbook Values are for normalized data unless noted

Layup	Environment	Statistic	UNT	UNC	SBS*	OHT	FHT	OHC	FHC	SS	В
										2% Offset	Ult. Str.
		B-basis	NA			44.96	46.64				
	CTD (-65°F)	Mean	82.81			49.37	51.30				
		CV	6.000			6.000	6.000				
		B-basis	67.55	51.79	6.927	39.53	41.07	29.04	51.02	77.91	93.35
S	RTD (70°F)	Mean	76.62	58.75	7.857	43.95	45.72	32.05	57.77	87.73	103.6
25/50/25		CV	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000	6.000
5/5		B-basis				37.98		21.90			
6	ETD (212°F)	Mean				42.39		24.91			
		CV				6.00		6.00			
		B-basis	43.96	NA: A	2.977	25.84	27.47	18.69	NA: A	59.50	61.50
	ETW (212°F)	Mean	49.31	31.93	3.423	30.26	32.13	21.69	29.83	69.32	71.77
		CV	6.035	8.878	7.031	6.120	6.016	7.586	6.911	7.960	6.962
	CTD (-65°F)	B-basis	42.07			30.71	33.47				
		Mean	46.05			34.20	37.97				
		CV	6.000			6.000	6.000				
		B-basis	35.44	32.15		25.94	27.46	21.68	33.42	66.61	86.54
0	RTD (70°F)	Mean	39.42	36.47	-	29.43	31.15	24.60	37.79		95.42
80/1	01/08/01 ETD (212°F)	CV	6.000	6.000		6.000	6.000	6.000	6.000	6.000	6.000
3/0]		B-basis									
-		Mean									
		CV									
		B-basis	17.45	NA: A	-	15.57	16.44	12.39	16.01	48.61	56.56
	ETW (212°F)	Mean	21.43	19.17	-	17.67	18.71	14.14	18.16		65.39
	ETW (212°F)	CV	6.460	7.322		6.000	6.148	6.271	6.000	7.750	6.000
		B-basis	90.89		-	62.91	56.77				
	CTD (-65°F)	Mean	101.4			71.37	63.23				
		CV	6.000			6.000	6.000				
		B-basis	80.07	52.44	-	NA: A	48.15	28.91	52.79		79.56
40	RTD (70°F)	Mean CV	90.57 6.000	57.77 6.000		58.00 7.840	54.60 6.000	32.80 6.000	57.89 6.000		88.06 6.000
40/20/40		B-basis	0.000	0.000		7.840	0.000	0.000	0.000	0.201	0.000
40	ETD (212°E)	Mean									
	<b>ETD</b> (212°F)	CV									
		B-basis	55.18	27.01		33,96	NA: A	NA: A	26.29	50.00	50.55
	ETW (212°F)	Mean	61.81	32.24		38.52	38.41	21.08	31.48		59.04
		CV	6.000	7.622		6.000	6.703	7.470	6.000		6.685
Notes:	The modified CV B-basis The CV provided corresp NA implies that tests wer "NA: A" indicates ANOV Shaded empty boxes indic	onds with the B- e run but data di A with 3 batche	basis value g d not meet N s.	given. ICAMP's rec		requirements					

#### Table 3-2: NCAMP Recommended B-Basis Values for Laminate Test Data

# 3.2 Lamina and Laminate Summary Tables

Prepreg Material: Material Specificat Process Specificat	tion:	NMS 201/1 NPS 82014 Re	·V -		Quartz Fabric 2	U.		TK	Renegade RM-2014-LDk-Tk 4581 8HS Quartz Fabric 286 gsm with RC 38% Lamina Properties Summary					
Fabric:		4581 8HS Qua	rtz satin wea	ve	Resin:	Renegade RI	M-2014-LDk-	-1K						
	0.	lry) 3-pt Bend: gle Cantilever:			Tg (wet	) 3-pt Bend:	245.5°F		Tg METHO	DD: ASTM D	7028			
Date of fiber man	ufacture	· · · · · · · · · · · · · · · · · · ·	Lot 1 12/16/2021			Lot 2 1/4/2023			Lot 3 6/12/2023	· ·	- 			
Date of resin man			3/7/2023			8/8/2023			9/6/2023					
Date of prepreg m			3/7/2023		5 10 1	8/10/2023			9/8/2023					
Date of composite	manufactur	e			7/8/.	2023 - 9/25/2	2023							
Date of testing					9/12/	/2023 - 3/15/	2024							
Date of data subm	ittal					4/8/2024								
Date of analysis					4/22/2	2024 - 5/22/2	024							
						DODEDT	<b>D D I G F G G G G G G G G G G</b>		-			-		
		Data wana			CHANICAL P				CDT. 0.0112	0 in				
								s, normalizing ( ts and are estin		0 IN				
							~	ved by the certi						
Test Condition		CTD			RTD			ETD						
Property	B-Basis	Modified CV B-basis	Mean	<b>B-Basis</b>	Modified CV B-basis	Mean	<b>B-Basis</b>	Modified CV B-basis	Mean	<b>B-Basis</b>	Modified CV B-basis	Mean		
$\mathbf{F_1}^{\mathrm{tu}}$	110.8	108.9	123.5	70.03	NA	108.3	98.93	98.01	111.2	54.66	65.13	75.09		
(ksi)	(117.8)	(111.1)	(122.2)	(88.29)	(97.07)	(108.1)	(105.69)	(99.88)	(110.9)	(69.19)	(63.70)	(74.75)		
$\mathbf{E_1}^t$			3.534			3.281			3.131			3.033		
(Msi)			(3.495)			(3.275)			(3.124)			(3.024)		
v <sub>12</sub> <sup>t</sup>			0.1284			0.1247			0.1001			0.07861		
$\mathbf{F_2}^{\mathrm{tu}}$	77.20	91.95	103.35	89.16	81.87	93.33	59.73	79.00	90.46	27.42	NA	62.89		
(ksi)	(64.64)	NA	(102.37)	(75.32)	(82.41)	(93.33)	(45.99)	NA	(90.63)	(16.13)	NA	(63.12)		
$\mathbf{E_2}^{t}$			3.428			3.279			2.976			2.979		
(Msi)	53.53	72.10	(3.403)	(2.45	(1.01	(3.270)	40.10	17.77	(2.971)	26.00	24.50	(2.948)		
$\mathbf{F_1}^{cu}$	73.53	72.10	79.11	62.45	61.01	68.03	49.10	47.66	54.68	36.09	34.70	41.50		
(ksi) E1 <sup>c</sup>	(60.89)	(72.21)	(79.16) 3.576	(63.15)	(61.72)	(68.67)	(41.09)	(48.23)	(55.18) 3.300	(32.57)	(34.83)	(41.57) 3.198		
$E_1$ (Msi)			3.576 (3.579)			3.466 (3.499)			(3.328)			(3.208)		
(MSI) F2 <sup>cu</sup>	61.84	60.70	<u>(3.579)</u> 66.84	46.83	52.43	(3.499)	40.21	38.41	(3.328)	24.35	25.07	(3.208)		
F <sub>2</sub> (ksi)	(61.97)	60.70 (59.98)	00.84 (66.02)	40.83	(52.28)	58.50 (58.33)	(34.46)	(38.32)	(44.36)	(24.35)	(24.85)	(30.73)		
$E_2^c$	(01.57)	(33.30)	(00.02) 3.451	(34.20)	(32.20)	(38.33)	(34.40)	(30.32)	(44.30) 3.194	(24.20)	(24.03)	2.937		
E <sub>2</sub> (Msi)			(3.408)			(3.346)			(3.194			(2.906)		
F <sub>12</sub> <sup>s0.2%</sup> (ksi)	5.460	4.951	5.616	3.721	3.822	4.335	2.193	2.468	2.791	1.456	1.428	1.653		
$F_{12}^{s5\%}$ (ksi)	9.325	8.936	9.901	7.046	6.657	7.622	3.301	NA	4.923	2.149	2.139	2.527		
		0.200	0.7640	/.040	0.027	0.599	01001		0.4137	2.177	2.107	0.2470		
G <sub>12</sub> <sup>s</sup> (Msi)	0.201	8 (02		7 207	7 772		5.250	5 019		2 1 2 1	2.017			
SBS (ksi)	9.201	8.602	9.467	7.587	7.773	8.638	5.350	5.018	5.883	3.131	3.017	3.447		

Table 3-3: Summary of Test Results for Lamina Data

Tg (dry) Single Cantil         Tg (dry) Single Cantil         Tg (dry) Single Cantil         Date of fiber manufacture         Date of resin manufacture         Date of resin manufacture         Date of composite manufactur         Date of cesting         Date of data submittal         Date of data submittal         Date of data submittal         Date of data submittal         Date of analysis         Test       Prope         OHT (normalized)       Streng Modt         OHC (normalized)       Streng Modt         UNT (normalized)       Streng Modt         UNC (normalized)       Streng Modt         SBS1 (as measured)       Streng Modt         FHT (normalized)       Streng Modt         FHT (normalized)       Streng Modt         SBS1 (as measured)       Streng Modt         FHT (normalized)       Streng Modt         FHT (normalized)       Streng Modt         SBS1 (as measured)       Streng Modt         Single Shear Bearing (normalized)       2% Of         Single Shear Bearing (normalized)       2% Of	ilever: 3			Tg (wet	) 3-pt Bend:	245.5°F						nary
Date of resin manufacture         Date of prepreg manufacture         Date of composite manufacture         Date of composite manufacture         Date of testing         Date of data submittal         Date of data submittal         Date of analysis         Test       Prope         OHT (normalized)       Streng         OHC (normalized)       Streng         UNT (normalized)       Streng         UNT (normalized)       Streng         UNC (normalized)       Modt         SBS1 (as measured)       Streng         FHT (normalized)       Streng         FHT (normalized)       Streng         FHT       Streng         Modt       Streng         Gingle Shear       2% Of         Single Shear       2% Of         Single Shear       2% Of								Tg METHO	DD: ASTM	D7028		
Date of resin manufacture         Date of prepreg manufacture         Date of composite manufacture         Date of composite manufacture         Date of testing         Date of data submittal         Date of data submittal         Date of analysis         Test       Prope         OHT (normalized)       Streng         OHC (normalized)       Streng         UNT (normalized)       Streng         UNT (normalized)       Streng         UNC (normalized)       Modt         SBS1 (as measured)       Streng         FHT (normalized)       Streng         FHT (normalized)       Streng         FHT (normalized)       Streng         FHT (normalized)       Streng         FHC (normalized)       Streng         Single Shear Bearing       2% Of         Single Shear (normalized)       2% Of				Lot 1			Lot 2			Lot 3		
Date of prepreg manufactur Date of composite manufact Date of composite manufact Date of data submittal Date of data submittal Date of analysis Test Prope OHT (normalized) Streng Modu OHC (normalized) Streng Modu Stren Modu Stren Modu Stren Modu Stren Modu Stren Modu Stren Modu Stren Modu Stren Modu Stren Modu Stren Modu Stren Modu Stren Modu Stren Stren Modu Stren Stren Modu Stren Stren Modu Stren Modu Stren Stren Modu Stren Modu Stren Stren Modu Stren Bearing V V Stren Bearing V V Stren Bearing V V Stren S				12/16/2021			1/4/2023			6/12/2023		
Date of composite manufact       Date of testing Date of data submittal Date of analysis       Test     Prope       OHT (normalized)     Streng Modt       OHC (normalized)     Streng Modt       UNT (normalized)     Streng Modt       UNT (normalized)     Streng Modt       UNT (normalized)     Streng Modt       UNC (normalized)     Streng Modt       SBS1 (as measured)     Streng Modt       FHT (normalized)     Streng Modt       FHC (normalized)     Streng Modt       Single Shear Bearing (normalized)     2% Of Streng Ultimation				3/7/2023			8/8/2023			9/6/2023		
Date of testing Date of data submittal Date of analysis Test Prope OHT (normalized) Streng OHC (normalized) Streng Modu Streng Bearing Ultima Streng Bearing Ultima Streng But Streng Streng Streng Bearing Ultima Streng St	ure			3/7/2023			8/10/2023	2022		9/8/2023		
Date of data submittal Date of analysis Test Prope Contractionalized) OHC (normalized) OHC (normalized) OHC (normalized) OHC (normalized) OHC (normalized) Streng Modu Streng Streng Bearing Ultimation Streng Ultimation Streng Ultimation Streng Ultimation Streng Ultimation Streng Ultimation Streng Ultimation Streng Stren						1/8/2	2023 - 9/25/	2025				
Date of data submittal Date of analysis Test Prope Contractionalized) OHC (normalized) OHC (normalized) OHC (normalized) OHC (normalized) OHC (normalized) Streng Modu Streng Streng Bearing Ultimation Streng Ultimation Streng Ultimation Streng Ultimation Streng Ultimation Streng Ultimation Streng Ultimation Streng Stren						9/12/	2023 - 3/15	/2024				
Test Prope OHT (normalized) Streng OHC (normalized) Streng Modu UNT (normalized) Streng Modu Streng Bearing Ultimation Ultimation Streng Streng St							4/8/2024					
OHT (normalized) OHC (normalized) UNT (normalized) UNT (normalized) SBS1 (as measured) FHT (normalized) SIGS SIGN SIGN SIGN SIGN SIGN SIGN SIGN						4/22/	2024 - 5/22	/2024				
OHT (normalized) OHC (normalized) UNT (normalized) UNT (normalized) SBS1 (as measured) FHT (normalized) SBS1 Streng Modu Streng No Streng Streng Streng Bearing Ultima Streng Ultima Streng Ultima Streng Ultima Streng Ultima Streng No Streng Streng Streng Streng Streng Streng Streng Ultima Streng Ultima Streng Str												
OHT (normalized) OHC (normalized) UNT (normalized) UNT (normalized) SBS1 (as measured) FHT (normalized) SBS1 Streng Modu Streng No Streng Streng Streng Bearing Ultima Streng Ultima Streng Ultima Streng Ultima Streng Ultima Streng No Streng Streng Streng Streng Streng Streng Streng Ultima Streng Ultima Streng Str						PERTY B-B						
OHT (normalized) OHC (normalized) UNT (normalized) UNT (normalized) SBS1 (as measured) FHT (normalized) SIGS SIGN SIGN SIGN SIGN SIGN SIGN SIGN		Values sho		-		ormalizing C IH-17G requi			ates only			
OHT (normalized) OHC (normalized) UNT (normalized) UNT (normalized) SBS1 (as measured) FHT (normalized) SIGS SIGN SIGN SIGN SIGN SIGN SIGN SIGN	Т					ess specifical				7		
OHT (normalized) OHC (normalized) UNT (normalized) UNT (normalized) SBS1 (as measured) FHT (normalized) SBS1 Streng Modu Streng No Streng Streng Streng Bearing Ultima Streng Ultima Streng Ultima Streng Ultima Streng Ultima Streng No Streng Streng Streng Streng Streng Streng Streng Ultima Streng Ultima Streng Str			Layup:		i Isotropic 2			Soft'' 10/80/			Hard'' 40/20	0/40
OHT (normalized)     Streng       OHC (normalized)     Streng       OHC (normalized)     Streng       UNT (normalized)     Streng       UNT (normalized)     Modu       Streng     Modu       SBS1 (as measured)     Streng       FHT (normalized)     Streng       FHC (normalized)     Streng       Single Shear Bearing     2% Of       Streng     Ultimation	Property 1				Mod. CV		_	Mod. CV		_	Mod. CV	
(normalized) OHC (normalized) OHC (normalized) UNT (normalized) UNT (normalized) Streng Modu Streng Streng Streng Bearing Ultimaticed) Ultimaticed Streng Streng Ultimaticed Streng Stre		Condition	Unit	<b>B-value</b>	B-value	Mean	B-value	B-value	Mean	B-value	<b>B-value</b>	Mean
(normalized) OHC (normalized) UNT (normalized) UNT (normalized) Streng Modu Streng Streng Streng Bearing Ultimaticed) Ultimaticed Streng Streng Stren		CTD	ksi	47.59	44.96	49.37	32.92	30.71	34.20	64.13	62.91	71.37
(normalized) OHC (normalized) UNT (normalized) Streng Modu Streng Streng Bearing Ultimatized) Streng Ultimatized	th	RTD	ksi	42.16	39.53	43.95	28.15	25.94	29.43	26.06	NA	58.00
(normalized) Streng Modu UNT Streng (normalized) Modu Streng Streng Streng Streng Streng Streng Streng Bu Streng Bu Streng Bu Streng Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Ultima Streng Ultima Streng Ultima Streng Ultima	igtn	ETD	ksi	40.61	37.98	42.39	15.05	15.57	17.67			
(normalized) Streng Modu UNT Streng (normalized) Modu Streng Streng Streng Streng Streng Streng Streng Bu Streng Bu Streng Bu Streng Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Ultima Streng Ultima Streng Ultima Streng Ultima		ETW	ksi	21.97	25.84	30.26				28.66	33.96	38.52
(normalized) Streng Modu UNT Streng (normalized) Modu Streng Streng Streng Streng Streng Streng Streng Bu Streng Bu Streng Bu Streng Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Bu Streng Ultima Streng Ultima Streng Ultima Streng Ultima		RTD	ksi	30.77	29.04	32.05	21.53	21.68	24.60	30.85	28.91	32.80
Modu UNT (normalized) UNT (normalized) UNC (normalized) UNC (normalized) SBS1 (as measured) FHT (normalized) SITeng FHC (normalized) Single Shear Bearing Ultimatice Ultimatice Streng Ultimatice Ultimatice Streng Ultimatice Ultimatice Streng Streng Ultimatice Streng Streng Streng Ultimatice Streng Streng Ultimatice Streng Streng Streng Streng Ultimatice Streng S	ngth	ETD	ksi	20.59	21.90	24.91	10.07			11 54		
Modu UNT (normalized) UNT (normalized) UNC (normalized) UNC (normalized) SBS1 (as measured) FHT (normalized) SITeng FHC (normalized) Single Shear Bearing Ultimatice Ultimatice Streng Ultimatice Ultimatice Streng Ultimatice Ultimatice Streng Streng Ultimatice Streng Streng Streng Ultimatice Streng Streng Ultimatice Streng Streng Streng Streng Ultimatice Streng S	n orth	ETW	ksi	18.86 78.14	18.69 NA	21.69	10.27	12.39 42.07	14.14 46.05	11.76 89.19	NA 90.89	21.08
UNT (normalized) Modu Stren; Modu UNC Modu (normalized) Stren; (normalized) Stren; (as measured) Stren; (normalized) Stren; FHT (normalized) Stren; Single Shear Bearing Ultimit (normalized) Ultimit	0	CTD	ksi msi	/8.14	NA 	82.81	44.53	42.07	2.450	09.19	90.89	101.4 3.245
(normalized) (normalized) (normalized) SBS1 (as measured) FHT (normalized) FHC (normalized) FHC Single Shear Bearing (normalized) UNC Streng Streng Modu Streng Ultimatized) Streng Ultimatized Ultimatized Ultimatized			ksi	71.96	67.55	76.62	32.81	35.44	39.42	74.26	80.07	90.57
Modu       UNC     Modu       (normalized)     Streng       SBS1     Streng       (as measured)     Streng       FHT     Streng       (normalized)     Streng       FHC     Streng       (normalized)     Streng       Single Shear     2% Of       Streng     Ultimation       Understand     Utimation		RTD	msi			2.616			2.087			3.008
UNC Modu (normalized) Streng Modu SBS1 Streng (as measured) Streng FHT (normalized) Streng FHC (normalized) Streng Single Shear Bearing Ultimation Streng Ultimation Streng		DOW	ksi	40.36	43.96	49.31	15.06	17.45	21.43	47.66	55.18	61.81
UNC Modu (normalized) Streng Modu SBS1 (as measured) Streng FHT (normalized) Streng FHC (normalized) Streng Single Shear Bearing Ultimation	lulus	ETW	msi			2.083			1.549			2.628
(normalized) Streng Modu SBS1 (as measured) Streng FHT (normalized) Streng FHC (normalized) Streng Compalized) 2% Of Streng Bearing Ultimation Streng Ultimation Streng	· ·	RTD	ksi	56.21	51.79	58.75	34.17	32.15	36.47	54.67	52.44	57.77
Model       SBS1     Streng       (as measured)     Streng       FHT     Streng       (normalized)     Streng       FHC     Streng       (normalized)     Streng       Single Shear     2% Of       Bearing     Ultimation       Ultimation     Ultimation			msi			2.799			2.213			3.131
SBS1 (as measured)     Streng       FHT (normalized)     Streng       FHC (normalized)     Streng       Single Shear Bearing (normalized)     2% Of Streng       Ultimation     Ultimation	0	ETW	ksi	14.57	NA	31.93	11.84	NA	19.17	27.84	27.01	32.24
(as measured)     Streng       FHT (normalized)     Streng       FHC (normalized)     Streng       Single Shear Bearing (normalized)     2% Of Streng       Ultimation     Ultimation	iuius	RTD	msi ksi	6.930	 6.927	2.232			1.484			2.709
FHT (normalized)     Streng       FHC (normalized)     Streng       Single Shear Bearing (normalized)     2% Of Streng       Ultimation     Ultimation	ngth	ETW	ksi	3.038	2.977	3.423						
(normalized) Streng FHC Streng (normalized) 2% Of Single Shear Bearing Ultima (normalized) Ultima		CTD	ksi	42.19	46.64	51.30	36.59	33.47	37.97	51.36	56.77	63.23
FHC (normalized) Streng Single Shear Bearing Ultimatic U	ngth	RTD	ksi	40.15	41.07	45.72	28.69	27.46	31.15	48.89	48.15	54.60
(normalized) Streng Single Shear Bearing (normalized) Ultima		ETW	ksi	23.73	27.47	32.13	17.12	16.44	18.71	24.16	NA	38.41
(normalized) 2% Of Single Shear Bearing (normalized) Ultima	ngth	RTD	ksi	56.19	51.02	57.77	33.45	33.42	37.79	50.69	52.79	57.89
Bearing Ultimation	-	ETW	ksi	19.39	NA	29.83	17.14	16.01	18.16	29.44	26.29	31.48
(normalized)		RTD	ksi kai	79.38	77.91	87.73	70.30	66.61	74.67	58.47 51.30	70.71	78.97
(normalized)		ETW RTD	ksi ksi	60.97 89.50	59.50 93.35	<u>69.32</u> 103.6	48.35 78.56	48.61 86.54	<u>56.63</u> 95.42	51.30 82.95	50.00 79.56	58.26 88.06
- Strens		ETW	ksi	63.38	61.50	71.77	60.36	56.56	65.39	53.93	50.55	59.04
CAL												
(normalized) Streng	ngth	RTD	ksi			26.04						
ILT		CTD	ksi			10.39						
(as measured) Streng	ngth	RTD	ksi			7.979						
(	-	ETW	ksi			2.949						
CBS	-	CTD	lb 15			527.3						
(as measured) Streng		RTD ETW	lb lb			401.4						

Table 3-4: Summary of Test Results for Laminate Data

### 4. Individual Test Summaries, Statistics, Basis Values and Graphs

Test data for fiber dominated properties was normalized according to nominal cured ply thickness. Both normalized and as-measured statistics were included in the tables, but only the normalized data values were graphed. Test failures, outliers and explanations regarding computational choices were noted in the accompanying text for each test.

All individual specimen results are graphed for each test by batch and environmental condition with a line indicating the recommended basis values for each environmental condition. The data is jittered (moved slightly to the left or right) in order for all specimen values to be clearly visible. The strength values are always graphed on the vertical axis with the scale adjusted to include all data values and their corresponding basis values. The vertical axis may not include zero. The horizontal axis values will vary depending on the data and how much overlapping there was of the data within and between batches. When there was little variation, the batches were graphed from left to right. The environmental conditions were identified by the shape and color of the symbol used to plot the data. Otherwise, the environmental conditions were graphed from left to right and the batches were identified by the shape and color of the symbol.

When a dataset fails the Anderson-Darling k-sample (ADK) test for batch-to-batch variation, an ANOVA analysis is required. In order for B-basis values to be computed using the ANOVA method, data from five batches are required. Since this qualification dataset has only three batches, the basis values computed using ANOVA are considered estimates only. However, the basis values resulting from the ANOVA method using only three batches may be overly conservative. The ADK test is performed again after a transformation of the data according to the assumptions of the modified CV method (see section 2.1.4 for details). If the dataset still passes the ADK test at this point, modified CV basis values are provided. If the dataset does not pass the ADK test after the transformation, estimates may be computed using the modified CV method per the guidelines of CMH-17-1G section 8.3.10.

# 4.1 Warp Tension (WT)

Warp Tension data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, ETD, and ETW.

For the normalized dataset, the RTD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Applying the modified CV, there were no diagnostic test failures so pooling was acceptable for the four conditions.

For the as-measured dataset, all the environments failed the ADK for batch equivalency. ANOVA was used to compute basis values, and with three batches of data available these are estimates. Applying the modified CV, the RTD environment failed the ADK test for batch equivalency, therefore basis values could not be computed for that environment, and pooling across environments was not acceptable.

There were two statistical outliers. The highest normalized value in batch two of the CTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized CTD dataset but not in the as-measured CTD dataset. The highest normalized value in batch three of the RTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized RTD dataset but not in the as-measured RTD dataset. They were retained for this analysis.

Statistics, estimates, and basis values are given for the WT strength data in Table 4-1 and for the modulus data in Table 4-2. The normalized data, B-estimates, and B-basis values are shown graphically in Figure 4-1.

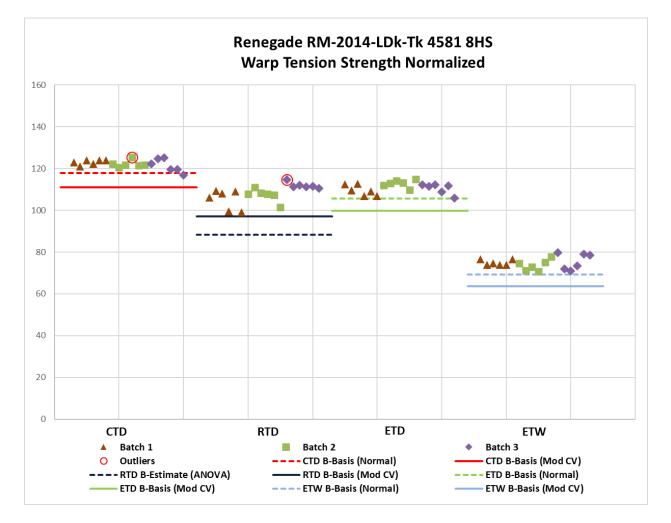


Figure 4-1: Batch Plot for WT Normalized Strength

			Warp Tensio	n (WT) Basis Valu	es and Statistics			
		Norma	alized		As-Measured			
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW
Mean	122.2	108.1	110.9	74.75	123.5	108.3	111.2	75.09
Stdev	2.200	4.236	2.651	2.817	2.916	6.067	2.812	4.091
CV	1.801	3.918	2.390	3.769	2.362	5.600	2.529	5.448
Mod CV	6.000	6.000	6.000	6.000	6.000	6.800	6.000	6.724
Min	116.9	99.11	105.8	70.62	117.7	98.90	105.9	67.60
Max	125.3	114.5	114.9	79.80	130.6	117.7	115.8	82.80
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18	18	18
				Basis Value Estim	ates			
B-Basis Value	117.8		105.7	69.19				
B-Estimate		88.29			110.8	70.03	98.93	54.66
A-Estimate	114.7	74.16	102.0	65.24	101.7	42.68	90.19	40.09
Method	Normal	ANOVA	Normal	Normal	ANOVA	ANOVA	ANOVA	ANOVA
			Modifie	d CV Basis Value	Estimates			
B-Value	111.1	97.07	99.88	63.70	108.9		98.01	65.13
A-Estimate	103.8	89.79	92.60	56.42	98.52	NA	88.70	58.07
Method	Pooled	Pooled	Pooled	Pooled	Normal		Normal	Normal

Table 4-1: Statistics and Basis values for WT Strength Data

			Warp Ten	sion (WT) Modulus	s Statistics			
		Norm	alized			As-Me	asured	
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW
Mean	3.495	3.275	3.124	3.024	3.534	3.281	3.131	3.033
Stdev	0.03362	0.06087	0.09843	0.1739	0.08252	0.1009	0.09731	0.1286
CV	0.9619	1.859	3.151	5.752	2.335	3.077	3.108	4.240
Mod CV	6.000	6.000	6.000	6.876	6.000	6.000	6.000	6.120
Min	3.415	3.062	2.988	2.837	3.394	3.090	2.970	2.860
Max	3.537	3.359	3.310	3.420	3.678	3.450	3.340	3.390
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18	18	18

Table 4-2: Statistics from WT Modulus Data

# 4.2 Fill Tension (FT)

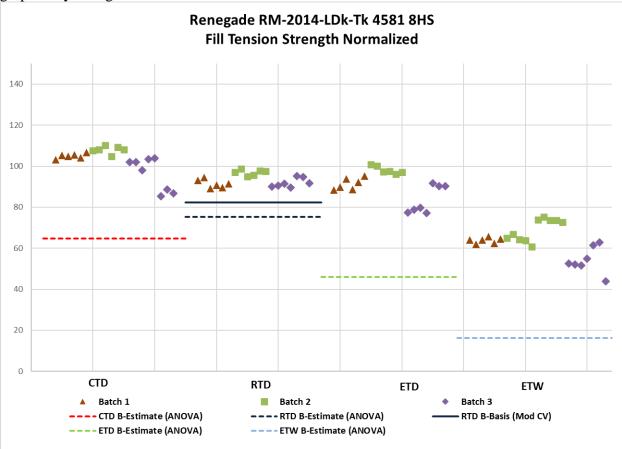
Fill Tension data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, ETD, and ETW.

For the normalized dataset, all the environments failed the ADK test for batch equivalency. ANOVA was used to compute basis values, and with three batches of data available these are estimates. Applying the modified CV, only the RTD environment passed the ADK test for batch equivalency, therefore pooling is not acceptable.

For the as-measured dataset, the CTD, ETD and ETW environments failed the ADK test for batch equivalency. ANOVA was used to compute basis values, and with three batches of data available these are estimates. Applying the modified CV, CTD and ETD passed the ADK test for batch equivalency, but ETW failed and basis values were not computed. CTD, RTD, and ETD were acceptable for pooling.

There were no statistical outliers.

Statistics, estimates and basis values are given for the FT strength data in Table 4-3 and for the modulus data in Table 4-4. The normalized data, B-estimates and the B-basis values are shown graphically in Figure 4-2.



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		-	Fill Tension (FT)	Strength Basis V	alues and Statistic	S		
		Norm	alized		As-Measured			
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW
Mean	102.4	93.33	90.63	63.12	103.4	93.33	90.46	62.89
Stdev	7.267	3.109	7.539	8.036	6.153	2.139	6.043	6.324
CV	7.099	3.331	8.318	12.73	5.953	2.292	6.680	10.06
Mod CV	7.550	6.000	8.318	12.73	6.977	6.000	7.340	10.06
Min	85.32	89.00	77.10	43.82	86.82	89.00	78.50	46.30
Max	110.2	98.63	100.8	75.23	109.5	96.90	99.00	71.40
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	20	19	19	23	20	19	19	23
				Basis Value Estim	ates			
B-Basis Value						89.16		
B-Estimate	64.64	75.32	45.99	16.13	77.20		59.73	27.42
A-Estimate	37.72	62.47	14.13	NA	58.55	86.20	37.81	2.098
Method	ANOVA	ANOVA	ANOVA	ANOVA	ANOVA	Normal	ANOVA	ANOVA
			Modifie	d CV Basis Value	Estimates			
B-Basis Value		82.41			91.95	81.87	79.00	
A-Estimate	NA	74.67	NA	NA	84.27	74.20	71.34	NA
Method		Normal			Pooled	Pooled	Pooled	

#### Figure 4-2: Batch Plot for FT Normalized Strength

#### Table 4-3: Statistics and Basis Values for FT Strength Data

			Fill Tens	sion (FT) Modulus	Statistics			
		Norm	alized			As-Me	asured	
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW
Mean	3.403	3.270	2.971	2.948	3.428	3.279	2.976	2.979
Stdev	0.03599	0.06790	0.09929	0.2638	0.08113	0.1122	0.09955	0.2664
CV	1.058	2.077	3.342	8.950	2.367	3.420	3.345	8.943
Mod CV	6.000	6.000	6.000	8.950	6.000	6.000	6.000	8.943
Min	3.313	3.082	2.775	2.688	3.213	3.110	2.800	2.700
Max	3.447	3.361	3.143	3.548	3.559	3.453	3.230	3.580
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	18	20	20	17	18	20	20	17

Table 4-4: Statistics from FT Modulus Data

# 4.3 Warp Compression (WC)

Warp Compression data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, ETD, and ETW.

For the normalized dataset, the CTD, ETD and ETW environments failed the ADK test for batch equivalency. ANOVA was used to compute basis values, and with three batches of data available these are estimates. Applying the modified CV, there were no diagnostic test failures so pooling the four environments was acceptable.

For the as-measured dataset, there were no diagnostic test failures so pooling the four environments was acceptable.

There were two statistical outliers. The highest as-measured value in batch two of the ETD environment was an outlier for the batch but not for the environment. It was an outlier in the asmeasured dataset but not in normalized dataset. The lowest as-measured value in batch three of the ETD environment was an outlier for the environment but not for the batch. It was an outlier in the as-measured dataset but not in the normalized dataset. They were retained for this analysis.

Statistics, basis values and estimates are given for the WC strength data in Table 4-5 and for the modulus data in Table 4-6. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-3.

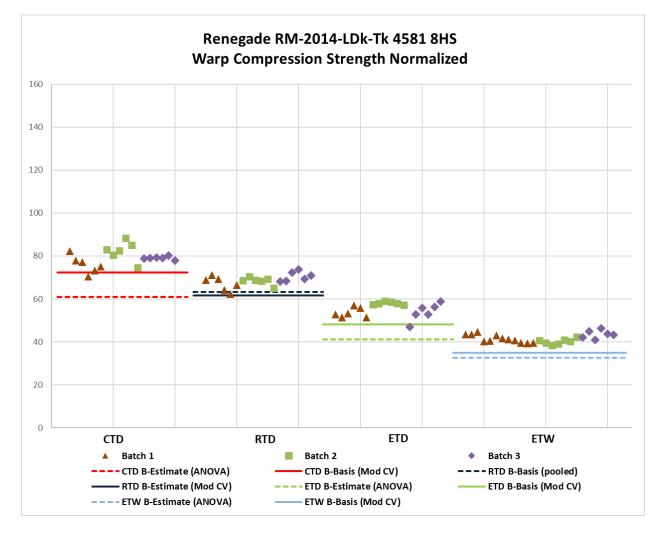


Figure 4-3: Batch Plot for WC Normalized Streng
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		Wa	rp Compressio	n (WC) Basis Va	lues and Statist	ics	•	-
		Norm	alized		As-Measured			
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW
Mean	79.16	68.67	55.18	41.57	79.11	68.03	54.68	41.50
Stdev	4.319	2.797	3.291	2.067	4.440	3.322	2.823	2.194
CV	5.456	4.073	5.964	4.972	5.612	4.883	5.163	5.286
Mod CV	6.728	6.037	6.982	6.486	6.806	6.442	6.581	6.643
Min	70.37	62.33	47.10	38.30	69.66	60.70	47.10	38.30
Max	88.38	73.80	59.04	46.21	87.51	73.80	58.90	45.80
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	18	18	18	25	18	18	18	25
			Ba	sis Value Estima	ates			
B-Basis Value		63.15			73.53	62.45	49.10	36.09
B-Estimate	60.89		41.09	32.57				
A-Estimate	47.87	59.24	31.05	26.13	69.87	58.78	45.43	32.40
Method	ANOVA	Normal	ANOVA	ANOVA	Pooled	Pooled	Pooled	Pooled
			Modified	CV Basis Value	Estimates			
B-Value	72.21	61.72	48.23	34.83	72.10	61.01	47.66	34.70
A-Estimate	67.64	57.15	43.66	30.22	67.49	56.40	43.05	30.06
Method	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled

Table 4-5: Statistics and Basis Values for WC Strength Data

			Warp Compr	ession (WC) Modu	Ilus Statistics			
		Norm	alized			As-Me	asured	
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW
Mean	3.579	3.499	3.328	3.208	3.576	3.466	3.300	3.198
Stdev	0.03018	0.06806	0.1280	0.2087	0.03841	0.07717	0.1486	0.2250
CV	0.8432	1.945	3.846	6.503	1.074	2.227	4.504	7.033
Mod CV	6.000	6.000	6.000	7.252	6.000	6.000	6.252	7.517
Min	3.520	3.388	3.030	2.976	3.514	3.340	3.030	2.950
Max	3.617	3.610	3.550	3.938	3.651	3.610	3.550	4.010
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18	18	18

Table 4-6: Statistics from WC Modulus Data

# 4.4 Fill Compression (FC)

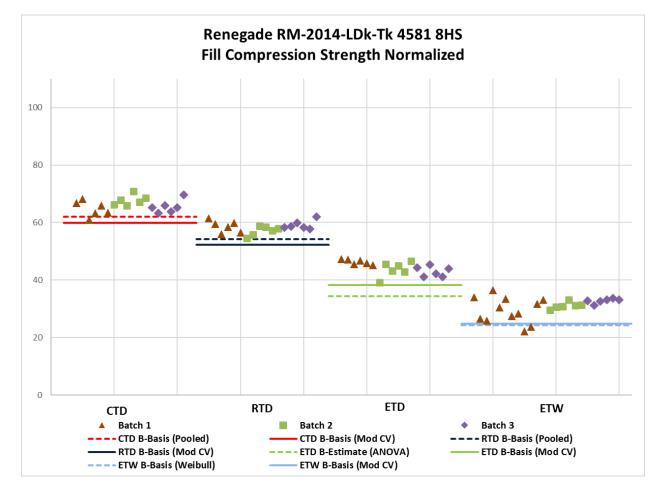
Fill Compression data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, ETD, and ETW.

For the normalized dataset, the ETD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. The ETW environment failed the normality test. Applying the modified CV, there were no diagnostic tests failures so pooling the four environments was acceptable.

For the as-measured data, the RTD environment failed the ADK test for batch equivalency, ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. The ETW environment failed the normality test. Applying the modified CV, there were no diagnostic test failures so pooling the four environments was acceptable.

There was one statistical outlier. The highest as-measured value in batch three of the CTD environment was an outlier for the batch but not for the environment. It was an outlier in the asmeasured dataset but not in the normalized dataset. It was retained for this analysis.

Statistics, basis values and estimates are given for the FC strength data in Table 4-7 and for the modulus data in Table 4-8. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-4.



		Fill C	ompression (FC	C) Strength Basis	s Values and Sta	atistics		
		Norm	alized		As-Measured			
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW
Mean	66.02	58.33	44.36	30.73	66.84	58.56	44.54	31.03
Stdev	2.513	1.890	2.304	3.449	2.530	2.408	2.194	3.568
CV	3.806	3.240	5.194	11.22	3.785	4.111	4.925	11.50
Mod CV	6.000	6.000	6.597	11.22	6.000	6.056	6.463	11.50
Min	60.95	54.58	39.25	22.20	61.75	54.10	38.90	22.20
Max	70.90	62.07	47.30	36.57	71.55	63.20	47.50	36.90
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	18	18	18	24	18	18	18	24
			В	asis Value Estim	nates			
B-Basis Value	61.97	54.28		24.26	61.84		40.21	24.35
B-Estimate			34.46			46.83		
A-Estimate	59.22	51.52	27.39	18.45	58.30	38.47	37.14	18.39
Method	Pooled	Pooled	ANOVA	Weibull	Normal	ANOVA	Normal	Weibull
			Modified	l CV Basis Value	Estimates			
B-Basis Value	59.98	52.28	38.32	24.85	60.70	52.43	38.41	25.07
A-Estimate	56.00	48.31	34.35	20.85	56.67	48.40	34.38	21.01
Method	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled

Table 4-7: Statistics and Basis Values for FC Strength Data

	Fill Compression (FC) Modulus Statistics										
		Norm	alized	d			As-Measured				
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW			
Mean	3.408	3.346	3.180	2.906	3.451	3.360	3.194	2.937			
Stdev	0.05918	0.1230	0.1193	0.1500	0.09116	0.1723	0.1498	0.1664			
CV	1.736	3.675	3.753	5.163	2.641	5.128	4.690	5.667			
Mod CV	6.000	6.000	6.000	6.582	6.000	6.564	6.345	6.833			
Min	3.283	3.148	2.966	2.650	3.283	3.120	2.940	2.650			
Max	3.482	3.591	3.410	3.163	3.603	3.690	3.410	3.250			
No. Batches	3	3	3	3	3	3	3	3			
No. Spec.	18	18	18	18	18	18	18	18			

Table 4-8: Statistics from FC Modulus Data

# 4.5 In-Plane Shear (IPS)

In Plane Shear data is not normalized. Test results were available for 0.2% offset strength and strength at 5% strain in the following environmental conditions: CTD, RTD, ETD, and ETW.

For the 0.2% Offset Strength dataset, the RTD and ETD environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available these are estimates. Applying the modified CV, the environments were not acceptable for pooling because the dataset failed the Levene's Test for equality of variances.

For the Strength at 5% strain dataset, the ETD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value and with three batches of data available this is an estimate. The CTD and RTD environments were acceptable for pooling. Applying the modified CV, the ETD environment failed the ADK test for batch equivalency, therefore a basis value could not be computed.

There were two outliers. The highest value in batch three of the 0.2% offset strength ETW dataset was an outlier for the batch but not for the environment. The highest value in batch three of the strength at 5% strain ETD dataset was an outlier for the batch but not for the environment. They were retained for this analysis. Statistics, basis values and estimates are given for the IPS strength data in Table 4-9 and for the modulus data in Table 4-10. The as-measured data, B-basis values and B-estimates are shown graphically for Strength at 5% Strain in

Figure 4-5 and for 0.2% Offset Strength in Figure 4-6.

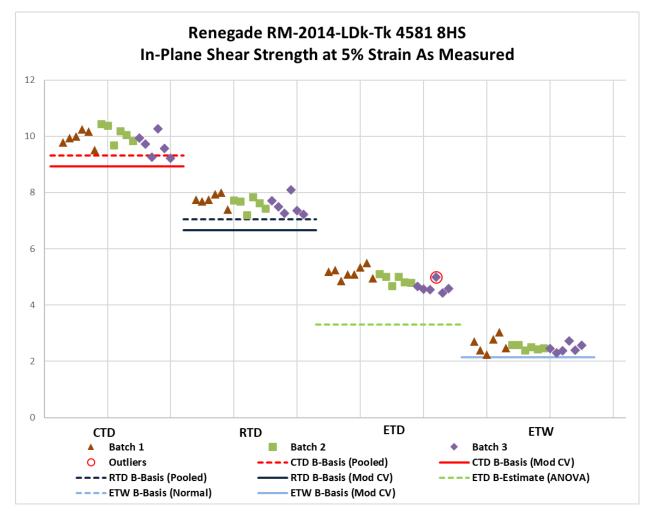


Figure 4-5: Batch Plot for IPS Maximum Strength and Strength at 5% Strain As-Measured

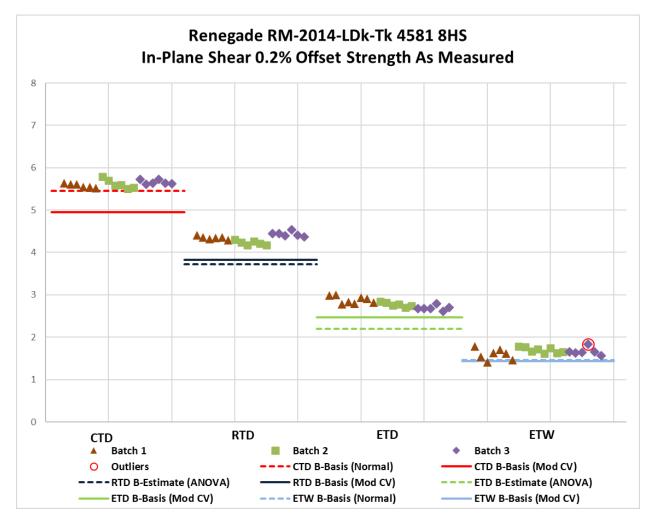


Figure 4-6: Batch Plot for IPS 0.2% Offset Strength As-Measured

			In Plane Shear	Strength Basis Va	lues and Statistics	3		
		0.2% Offse	et Strength		Strength at 5% Strain			
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW
Mean	5.616	4.335	2.791	1.653	9.901	7.622	4.923	2.527
Stdev	0.07899	0.09660	0.1065	0.1038	0.3607	0.2649	0.2893	0.1911
CV	1.406	2.228	3.816	6.278	3.643	3.476	5.877	7.562
Mod CV	6.000	6.000	6.000	7.139	6.000	6.000	6.939	7.781
Min	5.503	4.180	2.610	1.410	9.217	7.210	4.440	2.250
Max	5.789	4.530	3.000	1.830	10.45	8.090	5.500	3.030
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	18	18	20	21	18	18	20	18
				Basis Value Estim	ates			
B-basis Value	5.460			1.456	9.325	7.046		2.149
B-Estimate		3.721	2.193				3.301	
A-Estimate	5.350	3.283	1.766	1.315	8.933	6.654	2.143	1.882
Method	Normal	ANOVA	ANOVA	Normal	Pooled	Pooled	ANOVA	Normal
			Modifie	d CV Basis Value	Estimates			
B-basis Value	4.951	3.822	2.468	1.428	8.936	6.657		2.139
A-Estimate	4.480	3.458	2.239	1.268	8.279	6.000	NA	1.864
Method	Normal	Normal	Normal	Normal	Pooled	Pooled		Normal

Table 4-9: Statistics and Basis Values for IPS Strength Data

	In Plane Shear A	As Measured Mo	dulus Statistics	
Env	CTD	RTD	ETD	ETW
Mean	0.7640	0.5988	0.4137	0.2470
Stdev	0.01668	0.01971	0.01454	0.02201
CV	2.183	3.291	3.516	8.913
Mod CV	6.000	6.000	6.000	8.913
Min	0.7336	0.5700	0.3900	0.2170
Max	0.7878	0.6440	0.4370	0.3060
No. Batches	3	3	3	3
No. Spec.	18	18	20	21

## 4.6 "25/50/25" Unnotched Tension 1 (UNT1)

The UNT1 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, an ETW.

For the normalized dataset, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its value, and with three batches of data available this is an estimate. The CTD and RTD environments were acceptable for pooling. Applying the modified CV, all pooling variations fail the Anderson Darling test for normality.

For the as-measured dataset, the CTD and ETW environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available, these are estimates. Applying the modified CV, there were no diagnostic test failures so pooling the three environments was acceptable.

There were no statistical outliers.

Statistics, basis values and estimates are given for the UNT1 strength data in Table 4-11 and for the modulus data in Table 4-12. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-7.

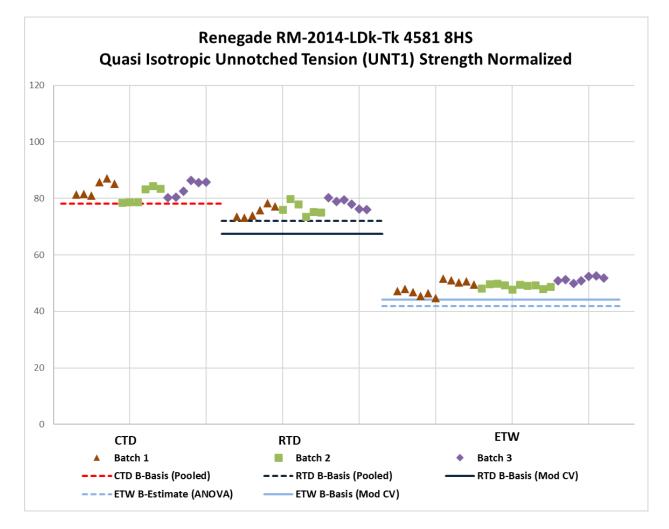


Figure 4-7: Batch Plot for UNT1 Normalized Strength

		Unnotched Tensi	on 1 (UNT1) Basis	Values and Statist	ics	
	Normalized			As-Measured		
Env	CTD	RTD	ETW	CTD	RTD	ETW
Mean	82.81	76.62	49.31	81.77	75.52	48.94
Stdev	2.830	2.262	2.007	2.772	2.267	1.604
CV	3.417	2.952	4.071	3.390	3.003	3.277
Mod CV	6.000	6.000	6.035	6.000	6.000	6.000
Min	78.50	73.27	44.69	77.03	71.20	45.50
Max	87.09	80.24	52.50	85.73	79.30	51.50
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	28	18	18	28
			Basis Value Estin	nates		
B-Basis Value	78.14	71.96			71.04	
B-Estimate			40.36	68.21		40.60
A-Estimate	74.97	68.78	33.95	58.54	67.87	34.63
Method	Pooled	Pooled	ANOVA	ANOVA	Normal	ANOVA
		Modifi	ed CV Basis Value	e Estimates		
B-Estimate		67.55	43.96	NA	NA NA	43.66
A-Estimate	NA	61.13	40.10			39.85
Method		Normal	Normal			Normal

Table 4-11: Statistics and Basis Values for UNT1 Strength Data

		Unnotched Ter	sion 1 (UNT1) Mo	dulus Statistics		
		Normalized		As-Measured		
Env	CTD	RTD	ETW	CTD	RTD	ETW
Mean	2.881	2.616	2.083	2.846	2.577	2.327
Stdev	0.03367	0.1081	0.06325	0.05972	0.08171	0.3807
CV	1.169	4.132	3.04	2.099	3.170	16.36
Mod CV	6.000	6.066	6.000	6.000	6.000	16.36
Min	2.796	2.452	1.945	2.724	2.439	1.950
Max	2.937	2.730	2.151	2.971	2.718	3.110
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	16	18	18	16

# 4.7 **"10/80/10"** Unnotched Tension 2 (UNT2)

The UNT2 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, and ETW.

For the normalized dataset, the RTD and ETW environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available, these are estimates. Applying the modified CV, there were no diagnostic test failures so pooling the thee environments was acceptable.

For the as-measured dataset, the three environments failed the ADK test for batch equivalency,. ANOVA was used to compute their basis values and with three batches of data available, these are estimates. Applying the modified CV, the RTD and ETW environments failed the ADK test for batch equivalency so basis values were not computed for those.

There was one outlier. The lowest normalized value in batch three of the RTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized and asmeasured dataset,. It was retained for this analysis.

Statistics, basis values and estimates are given for the UNT2 strength data in Table 4-13 and for the modulus data in Table 4-14. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-8.

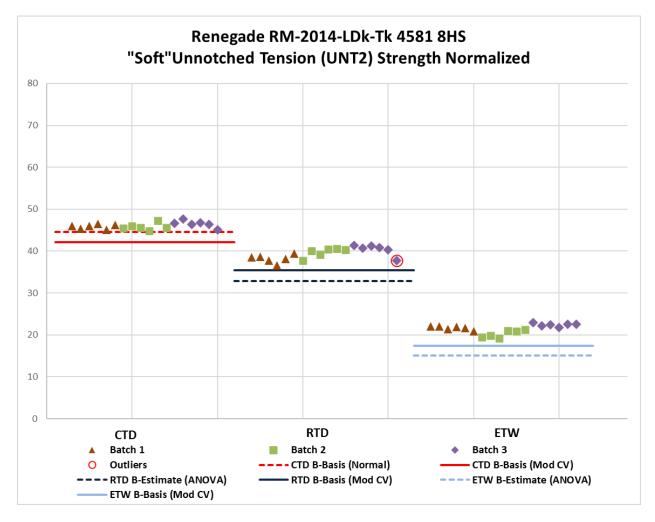


Figure 4-8: Batch Plot for UNT2 Normalized Strength

		Unnotched Tensic	on 2 (UNT2) Basis	Values and Statis	tics		
		Normalized		As-Measured			
Env	CTD	RTD	ETW	CTD	RTD	ETW	
Mean	46.05	39.42	21.43	46.11	39.40	21.54	
Stdev	0.7691	1.424	1.054	1.075	1.702	1.124	
CV	1.670	3.613	4.919	2.331	4.320	5.218	
Mod CV	6.000	6.000	6.460	6.000	6.160	6.609	
Min	44.82	36.62	19.25	44.01	36.30	19.40	
Max	47.72	41.35	22.90	48.46	42.40	22.90	
No. Batches	3	3	3	3	3	3	
No. Spec.	18	18	18	18	18	18	
			Basis Value Estim	ates			
B-Basis Value	44.53						
B-Estimate		32.81	15.06	40.62	29.77	14.43	
A-Estimate	43.46	28.10	10.51	36.70	22.90	9.356	
Method	Normal	ANOVA	ANOVA	ANOVA	ANOVA	ANOVA	
		Modifie	d CV Basis Value	Estimates			
B-Value	42.07	35.44	17.45	40.65			
A-Estimate	39.42	32.79	14.80	36.79	NA	NA	
Method	Pooled	Pooled	Pooled	Normal			

Table 4-13: Statistics and Basis Values for UNT2 Strength Data

		Unnotched Ten	sion 2 (UNT2) Mo	dulus Statistics		
		Normalized		As-Measured		
Env	CTD	RTD	ETW	CTD	RTD	ETW
Mean	2.450	2.087	1.549	2.453	2.085	1.556
Stdev	0.02747	0.08428	0.1614	0.04164	0.1015	0.1558
CV	1.121	4.037	10.42	1.698	4.867	10.01
Mod CV	6.000	6.019	10.42	6.000	6.433	10.01
Min	2.369	1.939	1.326	2.349	1.922	1.350
Max	2.484	2.175	1.917	2.507	2.228	1.900
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18

Table 4-14: Statistics from UNT2 Modulus Data

# 4.8 **"40/20/40"** Unnotched Tension 3 (UNT3)

The UNT3 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in three environmental conditions.

For the normalized dataset, the three environments fail the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available these are estimates. Applying the modified CV, pooling the three environments failed the Levene's test for equality of variances but the CTD and RTD environments were acceptable for pooling.

For the as-measured dataset, the RTD and ETW environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available, these are estimates. Applying the modified CV, the RTD and ETW environments failed the ADK test for batch equivalency so basis values were not computed for those.

There was one outlier. The lowest normalized value in batch three of the RTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset but not in the as-measured dataset. It was retained for this analysis.

Statistics, basis values and estimates are given for the UNT3 strength data in Table 4-15 and for the modulus data in Table 4-16. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-9.

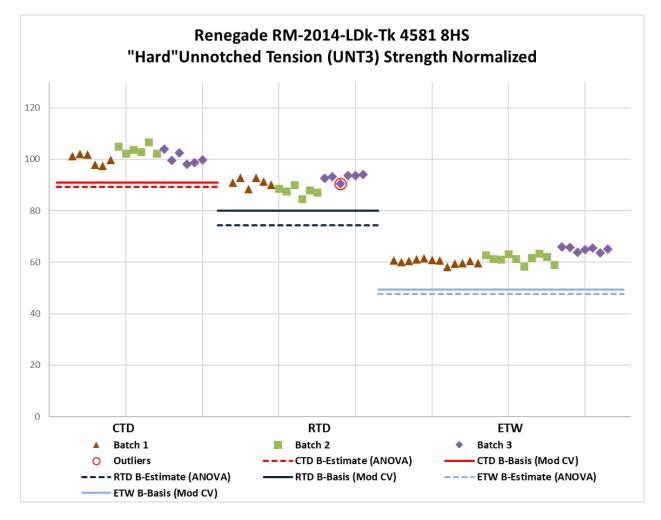


Figure 4-9: Batch Plot for UNT3 Normalized Strength

		Unnotched Tensio	on 3 (UNT3) Basis	Values and Statist	ics	
	Normalized			As-Measured		
Env	CTD	RTD	ETW	CTD	RTD	ETW
Mean	101.4	90.57	61.81	102.1	91.42	62.63
Stdev	2.615	2.725	2.221	2.511	4.294	2.903
CV	2.579	3.008	3.593	2.459	4.697	4.635
Mod CV	6.000	6.000	6.000	6.000	6.349	6.318
Min	97.38	84.65	58.20	97.13	83.90	58.20
Max	106.7	94.01	65.90	106.7	98.40	67.90
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	29	18	18	29
			Basis Value Estim	ates		
B-Basis Value				97.15		
B-Estimate	89.19	74.26	47.66		62.82	42.90
A-Estimate	80.50	62.61	37.56	93.64	42.40	28.82
Method	ANOVA	ANOVA	ANOVA	Normal	ANOVA	ANOVA
		Modifie	d CV Basis Value	Estimates		
B-Value	90.89	80.07	55.18	90.01		
A-Estimate	83.74	72.92	50.39	81.46	NA	NA
Method	Pooled	Pooled	Normal	Normal		

Table 4-15: Statistics and Basis Values for UNT3 Strength Data

		Unnotched Ten	sion 3 (UNT3) Mo	dulus Statistics		
		Normalized		As-Measured		
Env	CTD	RTD	ETW	CTD	RTD	ETW
Mean	3.245	3.008	2.628	3.268	3.035	2.669
Stdev	0.02366	0.1237	0.05955	0.04205	0.1475	0.07075
CV	0.7291	4.111	2.266	1.287	4.861	2.650
Mod CV	6.000	6.055	6.00	6.000	6.430	6.000
Min	3.203	2.780	2.557	3.198	2.780	2.580
Max	3.284	3.125	2.754	3.329	3.234	2.800
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18

#### 4.9 "25/50/25" Unnotched Compression 1 (UNC1)

The UNC1 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For the normalized dataset, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available, this is an estimate. Applying the modified CV, the ETW environment failed the ADK test for batch equivalency, therefore, a basis value was not computed.

For the as-measured dataset, both environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available, these are estimates. Applying the modified CV, the ETW environment failed the ADK test for batch equivalency, therefore a basis value was not computed.

There was one outlier. The lowest normalized value in batch two of the ETW environment was an outlier for the environment but not for the batch. It was an outlier in the normalized dataset but not in the as-measured dataset. It was retained for this analysis.

Statistics, basis values and estimates are given for the UNC1 strength data in Table 4-17 and for the modulus data in Table 4-18. The normalized data and B-basis values are shown graphically in Figure 4-10.

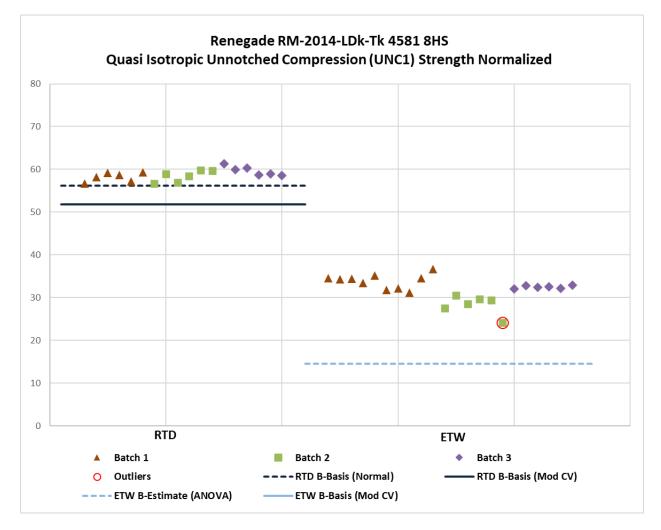


Figure 4-10: Batch Plot for UNC1 Normalized Strength

Unnotched Compression 1 (UNC1) Basis Values and Statistics							
	Norm	alized	As-Measured				
Env	RTD	ETW	RTD	ETW			
Mean	58.75	31.93	58.55	32.05			
Stdev	1.285	2.835	1.717	3.091			
CV	2.188	8.878	2.933	9.643			
Mod CV	6.000	8.878	6.000	9.643			
Min	56.63	24.11	55.20	24.00			
Max	61.26	36.63	61.90	37.30			
No. Batches	3	3	3	3			
No. Spec.	18	22	18	22			
	Bas	sis Value Estima	ites				
<b>B-Basis Value</b>	56.21						
B-Estimate		14.57	50.65	12.08			
A-Estimate	54.41	2.183	45.03	NA			
Method	Normal	ANOVA	ANOVA	ANOVA			
	Modified (	CV Basis Value I	Estimates				
B-Value	51.79		51.61				
A-Estimate	46.86	NA	46.71	NA			
Method	Normal		Normal				

Table 4-17: Statistics and Basis Values for UNC1 Strength Data

Unnotched Compression 1 (UNC1) Modulus Statistics							
	Norm	alized	As-Measured				
Env	RTD	ETW	RTD	ETW			
Mean	2.799	2.232	2.789	2.232			
Stdev	0.05678	0.06787	0.03848	0.05264			
CV	2.029	3.041	1.380	2.358			
Mod CV	6.000	6.000	6.000	6.000			
Min	2.671	2.108	2.720	2.130			
Max	2.854	2.344	2.850	2.300			
No. Batches	3	3	3	3			
No. Spec.	18	18	18	18			

Table 4-18: Statistics from UNC1 Modulus Data

#### 4.10 "10/80/10" Unnotched Compression 2 (UNC2)

The UNC2 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For the normalized dataset, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available, this is an estimate. Applying the modified CV, the ETW environment failed the ADK test for batch equivalency, therefore, a basis value was not computed.

For the as-measured dataset, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Applying the modified CV, the ETW environment failed the ADK test for batch equivalency, therefore, a basis value was not computed.

There were no statistical outlies.

Statistics, basis values and estimates are given for the UNC2 strength data in Table 4-19 and for the modulus data in Table 4-20. The normalized data and B-basis values are shown graphically in Figure 4-11.

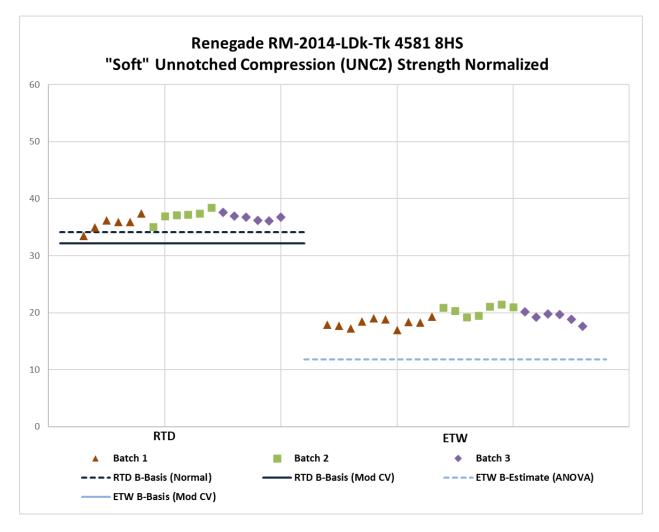


Figure 4-11: Batch Plot for UNC2 Normalized Strength

Unnotched Compression 2 (UNC2) Basis Values and Statistics								
	Norm	alized	As-Measured					
Env	RTD	ETW	RTD	ETW				
Mean	36.47	19.17	37.13	19.53				
Stdev	1.165	1.274	0.9653	1.144				
CV	3.194	6.645	2.599	5.859				
Mod CV	6.000	7.322	6.000	6.930				
Min	33.46	16.99	34.70	17.30				
Max	38.48	21.50	38.60	21.50				
No. Batches	3	3	3	3				
No. Spec.	18	23	18	23				
	Ba	asis Value Estima	tes					
B-Basis Value	34.17		35.23					
<b>B-Estimate</b>		11.84		13.40				
A-Estimate	32.54	6.597	33.88	9.029				
Method	Normal	ANOVA	Normal	ANOVA				
	Modified CV Basis Value Estimates							
B-Value	32.15		32.73					
A-Estimate	29.10	NA	29.62	NA				
Method	Normal		Normal					

Table 4-19: Statistics and Basis Values for UNC2 Strength Data

Unnotched Compression 2 (UNC2) Modulus Statistics				
	Normalized		As-Measured	
Env	RTD	ETW	RTD	ETW
Mean	2.213	1.484	2.254	1.506
Stdev	0.05096	0.08025	0.05054	0.06955
CV	2.302	5.407	2.242	4.618
Mod CV	6.000	6.704	6.000	6.309
Min	2.112	1.347	2.150	1.400
Max	2.309	1.610	2.330	1.610
No. Batches	3	3	3	3
No. Spec.	18	18	18	18

Table 4-20: Statistics from UNC2 Modulus Data

#### 4.11 "40/20/40" Unnotched Compression 3 (UNC3)

The UNC3 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in two environmental conditions.

For the normalized dataset, there were no diagnostic test failures for the normalized datasets. Pooling the two conditions was acceptable.

For the as-measured dataset, the pooled dataset failed the Anderson Darling test for normality. Applying the modified CV, there were no diagnostic test failures.

There were no statistical outliers.

Statistics, basis values and estimates are given for the UNC3 strength data in Table 4-21 and for the modulus data in Table 4-22. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-12.

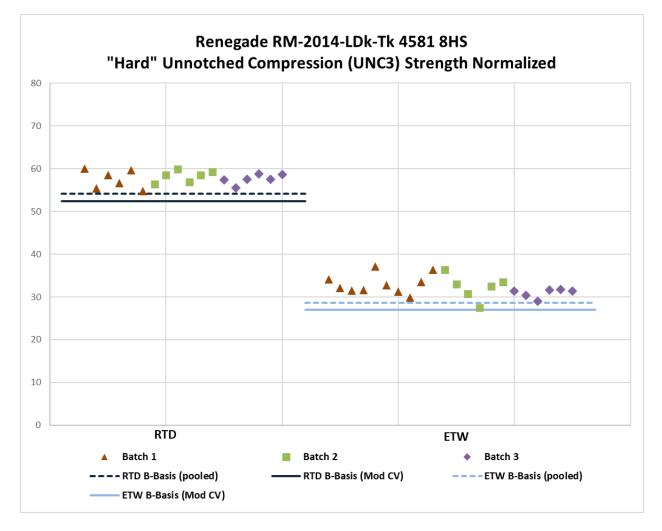


Figure 4-12: Batch Plot for UNC3 Normalized Strength

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Unno	tched Compress	ion 3 (UNC3) Basis	s Values and Stati	stics	
	Normalized		As-Me	As-Measured	
Env	RTD	ETW	RTD	ETW	
Mean	57.77	32.24	58.13	32.58	
Stdev	1.573	2.335	1.731	2.413	
CV	2.723	7.244	2.978	7.408	
Mod CV	6.000	7.622	6.000	7.704	
Min	54.80	27.50	54.80	27.50	
Max	59.96	37.13	60.90	37.80	
No. Batches	3	3	3	3	
No. Spec.	18	22	18	22	
Basis Value Estimates					
B-Basis Value	54.67	27.84	54.72	28.03	
A-Estimate	52.47	24.69	52.29	24.77	
Method	Normal	Normal	Normal	Normal	
Modified CV Basis Value Estimates					
B-Value	52.44	27.01	52.74	27.28	
A-Estimate	48.84	23.38	49.09	23.61	
Method	Pooled	Pooled	Pooled	Pooled	

Table 4-21: Statistics and Basis Values for UNC3 Strength Data

Unnotched Compression 3 (UNC3) Modulus Statistics				
	Normalized		As-Measured	
Env	RTD	ETW	RTD	ETW
Mean	3.131	2.709	3.152	2.733
Stdev	0.1105	0.08700	0.1596	0.08568
CV	3.529	3.212	5.064	3.135
Mod CV	6.000	6.000	6.532	6.000
Min	2.931	2.495	2.880	2.540
Max	3.300	2.830	3.370	2.850
No. Batches	3	3	3	3
No. Spec.	18	18	18	18

Table 4-22: Statistics from UNC3 Modulus Data

# 4.12 Lamina Short-Beam Strength (SBS)

The Short Beam Strength data is not normalized. Tests were conducted in the following environmental conditions: CTD, RTD, ETD, and ETW.

The datasets for the RTD and ETD environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available these are estimates. Applying the modified CV, pooling the four environments was not acceptable because the pooled dataset failed the Levene's test for equality of variances. The CTD, RTD, and ETD environments were acceptable for pooling.

There were no statistical outliers.

Statistics, basis values and estimates are given for the SBS data in Table 4-23. The as-measured data, B-estimates and B-basis values are shown graphically in Figure 4-13.

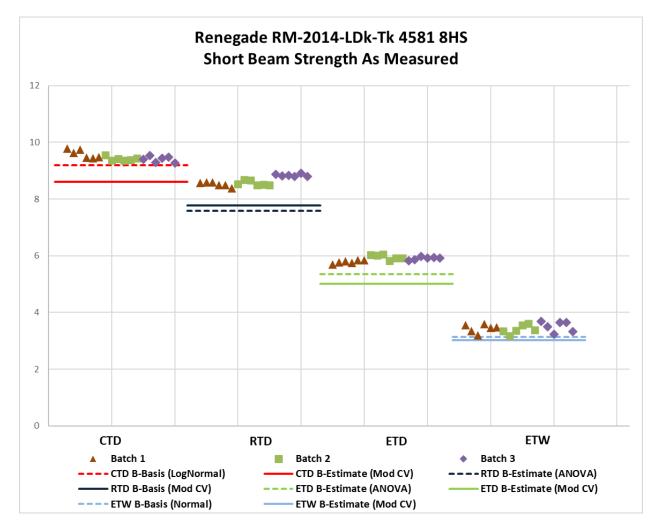


Figure 4-13: Batch Plot for SBS As-Measured

Short Beam Strength (SBS) As Measured Basis Values and Statistics					
Env	CTD	RTD	ETD	ETW	
Mean	9.467	8.638	5.883	3.447	
Stdev	0.1370	0.1602	0.09888	0.1600	
CV	1.447	1.855	1.681	4.642	
Mod CV	6.000	6.000	6.000	6.321	
Min	9.275	8.380	5.690	3.180	
Max	9.780	8.900	6.050	3.680	
No. Batches	3	3	3	3	
No. Spec.	18	18	18	18	
Basis Value Estimates					
<b>B-Basis Value</b>	9.201			3.131	
B-Estimate		7.587	5.350		
A-Estimate	9.017	6.837	4.970	2.907	
Method	LogNormal	ANOVA	ANOVA	Normal	
Modified CV Basis Value Estimates					
B-Value	8.602	7.773	5.018	3.017	
A-Estimate	8.025	7.196	4.441	2.712	
Method	Pooled	Pooled	Pooled	Normal	

Table 4-23: Statistics and Basis Values for SBS Data

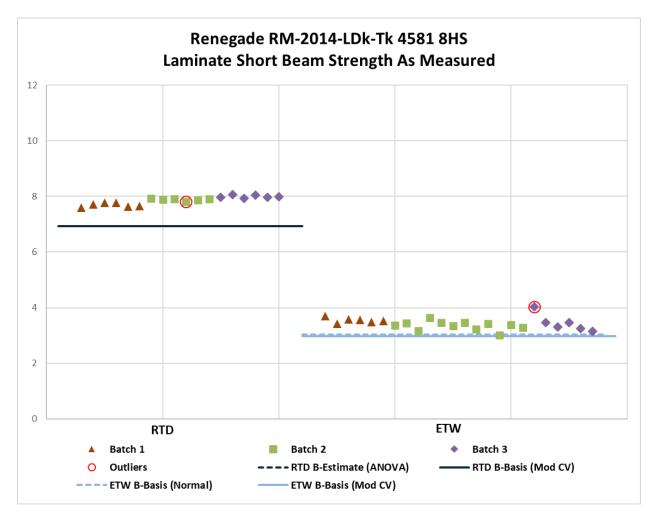
#### 4.13 Laminate Short-Beam Strength (SBS1)

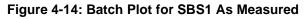
The Laminate Short Beam Strength data is not normalized. Tests were conducted in the following environmental conditions: RTD and ETW.

The RTD dataset failed the ADK test for batch equivalency. ANOVA was used to compute its basis value and with three batches of data available, this is an estimate. Applying the modified CV, pooling the two environments was not acceptable because the pooled dataset failed the Levene's test for equality of variances.

There were two statistical outliers. The lowest value in batch two for the RTD environment was an outlier for the batch but not for the environment. The highest value in batch three for the ETW environment was an outlier for the environment but not for the batch. They were retained for this analysis.

Statistics, basis values and estimates are given for the SBS1 data in Table 4-24. The as-measured data, B-estimates and B-basis values are shown graphically in Figure 4-14.





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Short Beam Strength 1 (SBS1) As Measured						
Env	RTD	ETW				
Mean	7.857	3.423				
Stdev	0.1389	0.2075				
CV	1.768	6.063				
Mod CV	6.000	7.031				
Min	7.590	3.010				
Max	8.070	4.040				
No. Batches	3	3				
No. Spec.	18	24				
Ba	sis Value Estima	ites				
<b>B-Basis Value</b>		3.038				
B-Estimate	6.930					
A-Estimate	6.268	2.763				
Method	ANOVA	Normal				
Modified CV Basis Value Estimates						
B-Estimate	6.927	2.977				
A-Estimate	6.268	2.657				
Method	Normal	Normal				

Table 4-24: Statistics and Basis Values for SBS1 Data

# 4.14 "25/50/25" Open-Hole Tension 1 (OHT1)

The OHT1 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, ETD, and ETW.

For the normalized dataset, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available, this is an estimate. Pooling was acceptable for the CTD, RTD, and ETD environments. Applying the modified CV, there were no diagnostic test failures, so pooling the four environments was acceptable.

For the as-measured dataset, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available, this is an estimate. Pooling was acceptable for the RTD and ETD environments. Applying the modified CV, there were no diagnostic test failures, so pooling the four environments was acceptable.

There were no statistical outliers.

Statistics, basis values and estimates are given for the OHT1 strength data in Table 4-25. The normalized data, B-basis values and B-estimates are shown graphically in Figure 4-15.

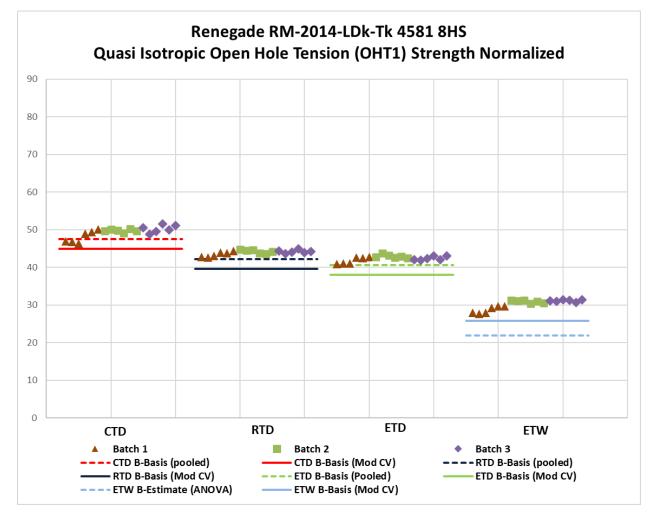


Figure 4-15: Batch Plot for OHT1 Normalized Strength

		Oper	n Hole Tension 1 (	OHT1) Strength B	asis Values and St	atistics			
	Normalized					As-Measured			
Env	CTD	RTD	ETD	ETW	CTD	RTD	ETD	ETW	
Mean	49.37	43.95	42.39	30.26	49.20	43.74	42.28	30.01	
Stdev	1.406	0.6514	0.8090	1.283	1.291	0.4090	0.3507	1.041	
CV	2.849	1.482	1.908	4.240	2.623	0.9351	0.8296	3.470	
Mod CV	6.000	6.000	6.000	6.120	6.000	6.000	6.000	6.000	
Min	46.35	42.56	40.89	27.61	46.49	43.10	41.50	27.90	
Max	51.61	44.97	43.84	31.47	51.54	44.60	42.70	31.30	
No. Batches	3	3	3	3	3	3	3	3	
No. Spec.	18	18	18	18	18	18	18	18	
				Basis Value Estim	ates				
B-basis Value	47.59	42.16	40.61		46.65	43.05	41.58		
B-Estimate				21.97				23.26	
A-Estimate	46.39	40.97	39.41	16.04	44.85	42.58	41.11	18.45	
Method	Pooled	Pooled	Pooled	ANOVA	Normal	Pooled	Pooled	ANOVA	
			Modifie	ed CV Basis Value	Estimates				
B-basis Value	44.96	39.53	37.98	25.84	44.81	39.36	37.89	25.62	
A-Estimate	42.04	36.62	35.06	22.93	41.92	36.46	35.00	22.73	
Method	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	

Table 4-25: Statistics and Basis Values for OHT1 Strength Data

# 4.15 "10/80/10" Open-Hole Tension 2 (OHT2)

The OHT2 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, and ETW.

For the normalized dataset, the ETD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. The CTD and RTD environments were pooled. Applying the modified CV, there were no diagnostic test failures, so pooling for the three environments was acceptable.

For the as-measured dataset, the RTD and ETD environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available these are estimates. Applying the modified CV, pooling the three environments failed the Levene's test for equality of variances but the CTD and RTD environments were acceptable for pooling.

There was one statistical outlier. The lowest as-measured value in batch two of the CTD environment was an outlier for the batch and for the environment. It was an outlier in the asmeasured dataset but not in the normalized dataset. It was retained for this analysis.

Statistics, basis values and estimates are given for the OHT2 strength data in Table 4-26. The normalized data and B-basis values are shown graphically in Figure 4-16.

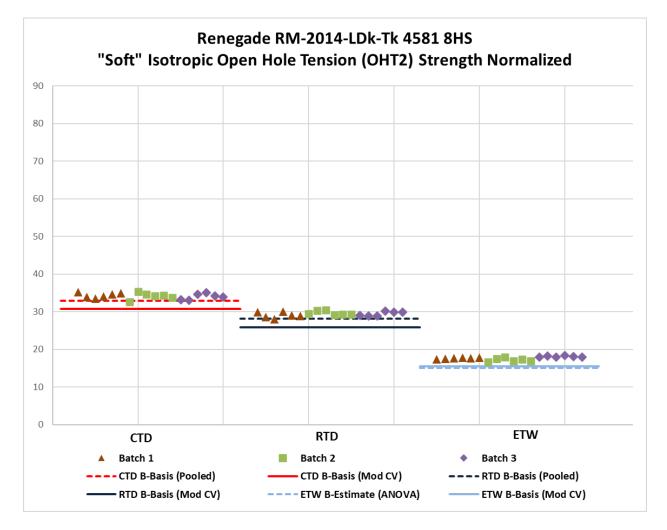


Figure 4-16: Batch Plot for OHT2 Normalized Strength

	Oper	Hole Tension 2 (	OHT2) Strength Ba	asis Values and S	tatistics		
		Normalized			As-Measured		
Env	CTD	RTD	ETD	CTD	RTD	ETD	
Mean	34.20	29.43	17.67	34.39	29.56	17.72	
Stdev	0.7424	0.6621	0.4564	0.6354	0.4767	0.7571	
CV	2.171	2.250	2.583	1.847	1.613	4.274	
Mod CV	6.000	6.000	6.000	6.000	6.000	6.137	
Min	32.69	28.09	16.74	32.68	28.60	16.30	
Max	35.32	30.54	18.33	35.51	30.20	18.80	
No. Batches	3	3	3	3	3	3	
No. Spec.	18	18	18	18	18	18	
			Basis Value Estim	ates			
B-basis Value	32.92	28.15		33.14			
B-Estimate			15.05		27.49	12.47	
A-Estimate	32.05	27.28	13.18	32.25	26.01	8.725	
Method	Pooled	Pooled	ANOVA	Normal	ANOVA	ANOVA	
		Modifie	d CV Basis Value	Estimates			
B-basis Value	30.71	25.94	15.57	30.89	26.06	15.57	
A-Estimate	28.34	23.57	14.09	28.50	23.67	14.05	
Method	Pooled	Pooled	Normal	Pooled	Pooled	Normal	

Table 4-26: Statistics and Basis Values for OHT2 Strength Data

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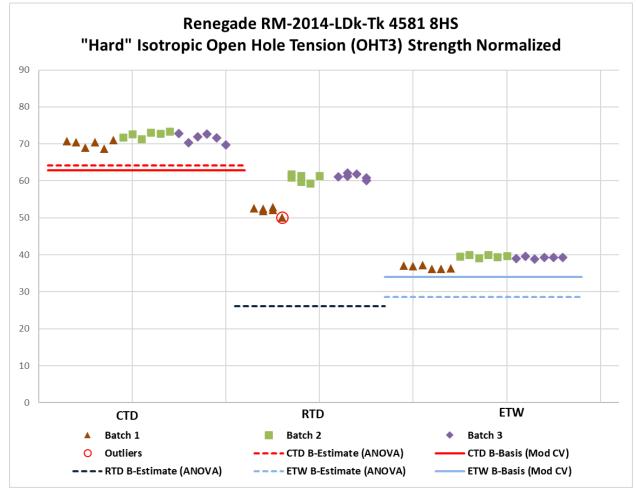
# 4.16 "40/20/40" Open-Hole Tension 3 (OHT3)

The OHT3 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, and ETD.

For both, the normalized and as-measured datasets, the three environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available these are estimates. Applying the modified CV, the RTD environment failed the ADK test for batch equivalency, therefore, basis values were not computed for this environment and pooling was not acceptable.

There were two statistical outliers. The lowest normalized value in batch one of the RTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset as well as in the as-measured dataset. The lowest as-measured value in batch three of the ETW environment was an outlier for the batch but not for the environment. It was an outlier in the as-measured dataset but not in the normalized dataset. They were retained for this analysis.

Statistics, basis values and estimates are given for the OHT3 strength data in Table 4-27. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-17.



	Oper	n Hole Tension 3 (	OHT3) Strength Ba	asis Values and S	tatistics		
	Normalized			As-Measured			
Env	CTD	RTD	ETW	CTD	RTD	ETD	
Mean	71.37	58.00	38.52	71.52	58.06	38.72	
Stdev	1.403	4.454	1.392	1.466	5.043	1.404	
CV	1.966	7.679	3.613	2.050	8.686	3.626	
Mod CV	6.000	7.840	6.000	6.000	8.686	6.000	
Min	68.73	50.04	36.17	68.89	49.60	36.50	
Max	73.35	62.17	40.05	73.95	63.30	40.00	
No. Batches	3	3	3	3	3	3	
No. Spec.	18	18	18	18	18	18	
-		E	Basis Value Estim	ates			
B-Estimate	64.13	26.06	28.66	63.80	21.77	28.65	
A-Estimate	58.97	3.261	21.61	58.29	NA	21.46	
Method	ANOVA	ANOVA	ANOVA	ANOVA	ANOVA	ANOVA	
		Modifie	d CV Basis Value	Estimates			
B-basis Value	62.91		33.96	63.05			
A-Estimate	56.93	NA	30.73	57.05	NA	NA	
Method	Normal		Normal	Normal			

#### Table 4-27: Statistics and Basis Values for OHT3 Strength Data

## 4.17 "25/50/25" Filled-Hole Tension 1 (FHT1)

The FHT1 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, and ETW.

For both the normalized and as-measured datasets, the three environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available these are estimates. Applying the modified CV, there were no diagnostic test failures so pooling the three environments was acceptable.

There was one statistical outlier. The lowest normalized value in batch three for the CTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset but not in the as-measured dataset. It was retained for this analysis.

Statistics, basis values and estimates are given for the FHT1 strength data in Table 4-28. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-18.

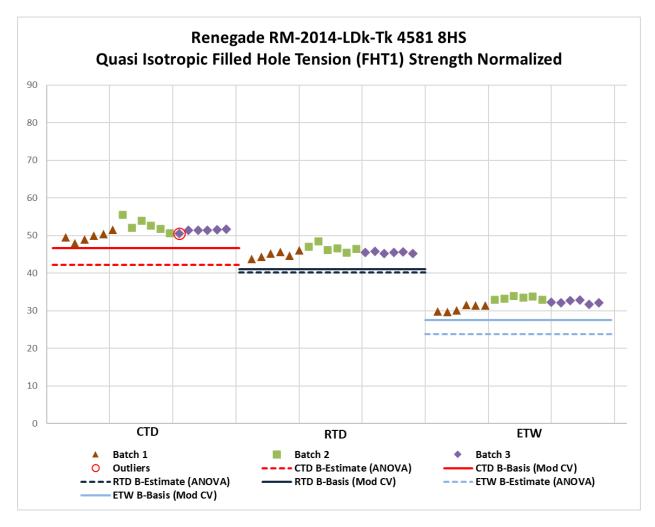


Figure 4-18: Batch Plot for FHT1 Normalized Strength

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	Filled-Ho	le Tension 1 (FH	T1) Strength Bas	sis Values and S	Statistics	-
	Normalized			As-Measured		
Env	CTD	RTD	ETW	CTD	RTD	ETW
Mean	51.30	45.72	32.13	50.70	45.37	31.73
Stdev	1.736	1.064	1.295	1.739	1.055	1.068
CV	3.384	2.326	4.031	3.431	2.326	3.366
Mod CV	6.000	6.000	6.016	6.000	6.000	6.000
Min	47.92	43.71	29.73	47.32	43.20	29.60
Max	55.55	48.47	33.99	54.73	47.90	33.10
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18
		Bas	sis Value Estima	ates		
B-Estimate	42.19	40.15	23.73	41.33	39.77	25.24
A-Estimate	35.69	36.17	17.74	34.65	35.77	20.61
Method	ANOVA	ANOVA	ANOVA	ANOVA	ANOVA	ANOVA
		Modified (	CV Basis Value I	Estimates		
B-Basis Value	46.64	41.07	27.47	46.09	40.77	27.13
A-Estimate	43.54	37.96	24.37	43.02	37.70	24.06
Method	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled

Table 4-28: Statistics and Basis Values for FHT1 Strength Data

## 4.18 "10/80/10" Filled-Hole Tension 2 (FHT2)

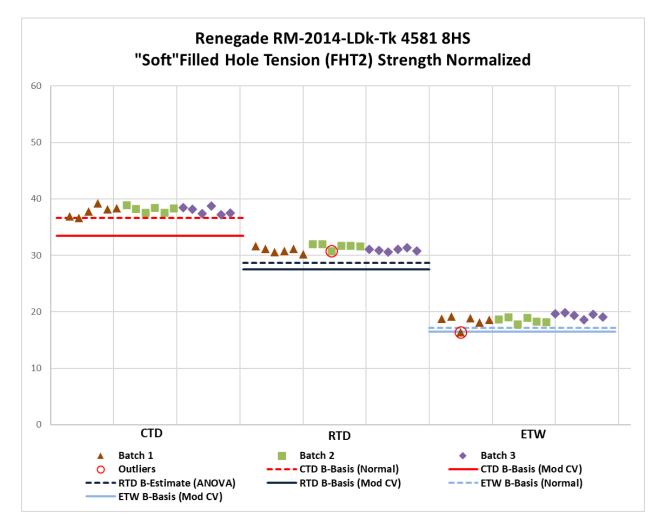
The FHT2 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, and ETW.

For the normalized dataset, the RTD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Applying the modified CV, any combination of environments was acceptable for pooling.

For the as-measured dataset, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimates. The CTD and RTD environments were not acceptable for pooling because the pooled dataset failed the Levene's test for equality of variances. Applying the modified CV, pooling the three environments was not acceptable because the pooled dataset failed the Levene's test for equality of variances. The CTD and RTD environments were acceptable for pooling.

There were two statistical outliers. The lowest normalized value in batch two of the RTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset but not in the as-measured dataset. The lowest normalized value in batch one of the ETW environment was an outlier for the batch as well as for the environment. It was an outlier in the normalized dataset but not in the as-measured dataset. They were retained for this analysis.

Statistics, basis values and estimates are given for the FHT2 strength data in Table 4-29. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-19.



	Fille	d-Hole Tension 2	(FHT2) Strength B	asis Values and S	tatistics	
	Normalized			As-Measured		
Env	CTD	RTD	ETW	CTD	RTD	ETW
Mean	37.97	31.15	18.71	38.34	31.40	18.90
Stdev	0.6973	0.5251	0.8037	0.7784	0.4243	0.8239
CV	1.837	1.686	4.295	2.030	1.351	4.359
Mod CV	6.000	6.000	6.148	6.000	6.000	6.180
Min	36.61	30.23	16.35	37.08	30.50	16.80
Max	39.19	32.00	19.82	39.62	32.20	20.20
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18
			Basis Value Estim	ates		
B-Basis Value	36.59		17.12	36.81	30.56	
B-Estimate		28.69				15.75
A-Estimate	35.62	26.93	16.00	35.72	29.97	13.50
Method	Normal	ANOVA	Normal	Normal	Normal	ANOVA
		Modifie	d CV Basis Value	Estimates		
B-Basis Value	33.47	27.46	16.44	34.51	27.57	16.59
A-Estimate	30.29	24.85	14.83	31.91	24.96	14.96
Method	Normal	Normal	Normal	Pooled	Pooled	Normal

Table 4-29: Statistics and Basis Values for FHT2 Strength Data

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## 4.19 "40/20/40" Filled-Hole Tension 3 (FHT3)

The FHT3 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: CTD, RTD, and ETW.

For both the normalized and as-measured datasets, the three conditions failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available these are estimates. Applying the modified CV, the ETW environment failed the ADK test for batch equivalency so basis values were not computed. The CTD and RTD environments were acceptable for pooling.

There were no statistical outliers.

Statistics, basis values and estimates are given for the FHT3 strength data in Table 4-30. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-20.

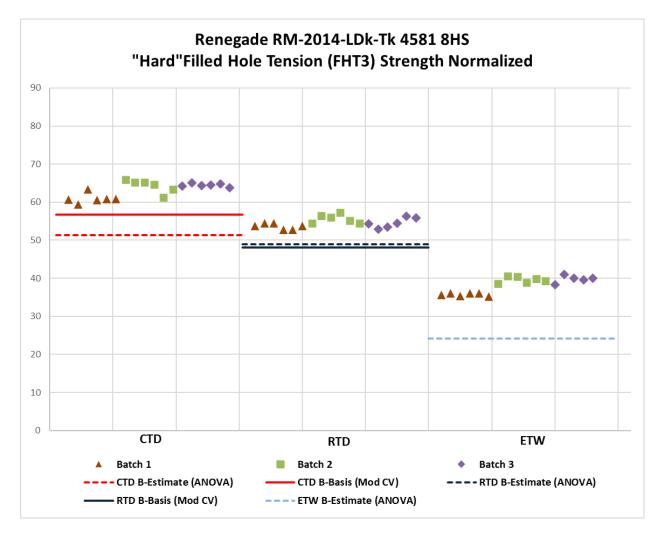


Figure 4-20: Batch plot for FHT3 Normalized Strength

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	Fille	d-Hole Tension 3 (	FHT3) Strength Ba	asis Values and S	tatistics	
	Normalized			As-Measured		
Env	CTD	RTD	ETW	CTD	RTD	ETW
Mean	63.23	54.60	38.41	63.15	54.71	38.51
Stdev	2.036	1.333	2.076	2.066	1.152	2.112
CV	3.220	2.442	5.406	3.271	2.106	5.484
Mod CV	6.000	6.000	6.703	6.000	6.000	6.742
Min	59.46	52.73	35.20	59.16	52.80	35.20
Max	65.85	57.31	41.00	65.61	56.80	41.00
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18
		E	Basis Value Estim	ates		
B-Estimate	51.36	48.89	24.16	51.02	49.56	24.08
A-Estimate	42.89	44.81	13.99	42.36	45.89	13.78
Method	ANOVA	ANOVA	ANOVA	ANOVA	ANOVA	ANOVA
		Modifie	d CV Basis Value	Estimates		
B-Basis Value	56.77	48.15		56.69	48.25	
A-Estimate	52.38	43.76	NA	52.30	43.86	NA
Method	Pooled	Pooled		Pooled	Pooled	

Table 4-30: Statistics and Basis Values for FHT3 Strength Data

#### 4.20 "25/50/25" Open-Hole Compression 1 (OHC1)

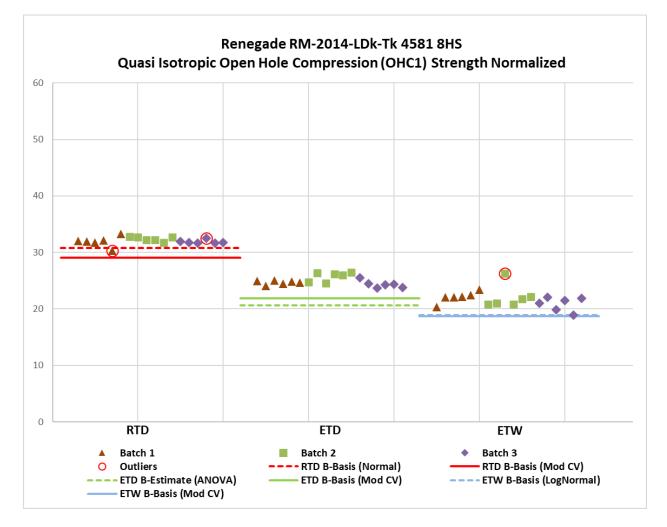
The OHC1 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD, ETD, and ETW.

For the normalized dataset, the ETD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Pooling was not acceptable for the RTD and ETW environments. Applying the modified CV, there were no diagnostic test failures so pooling the three environments was acceptable.

For the as-measured dataset, pooling the three environments was not acceptable because the pooled dataset failed the Anderson Darling test for normality but the RTD and ETD environments were acceptable for pooling. Applying the modified CV, there were no diagnostic test failures so pooling the three environments was acceptable.

There were three statistical outliers. The lowest normalized value in batch one of the RTD environment was an outlier for the environment but not for the batch. It was an outlier in the normalized dataset as well as in the as-measured dataset. The highest value in batch three of the RTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset as well as in the as-measured dataset. The highest normalized value in batch two of the ETW environment was an outlier for the batch and for the environment. It was an outlier in the normalized dataset as well as in the as-measured dataset. The highest normalized value in batch two of the ETW environment was an outlier for the batch and for the environment. It was an outlier in the normalized dataset as well as in the as-measured dataset. They were retained for this analysis.

Statistics, basis values and estimates are given for the OHC1 strength data in Table 4-31. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-21.



	Open H	ole Compression	1 (OHC1) Strength	Basis Values and	d Statistics	
		Normalized		As-Measured		
Env	RTD	ETD	ETW	RTD	ETD	ETW
Mean	32.05	24.91	21.69	31.79	24.74	21.58
Stdev	0.6480	0.8711	1.556	0.6194	0.7548	1.465
CV	2.022	3.497	7.171	1.948	3.050	6.788
Mod CV	6.000	6.000	7.586	6.000	6.000	7.394
Min	30.30	23.73	18.90	29.94	23.80	19.10
Max	33.27	26.50	26.31	32.90	26.00	26.00
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18
		Ba	sis Values and Esti	mates		
B-basis Value	30.77		18.86	30.53	23.49	18.26
B-Estimate		20.59				
A-Estimate	29.86	17.51	17.11	29.68	22.63	12.04
Method	Normal	ANOVA	LogNormal	Pooled	Pooled	Non-Parametric
		Modified	CV Basis Values ar	nd Estimates		
B-basis Value	29.04	21.90	18.69	28.83	21.78	18.62
A-Estimate	27.04	19.90	16.68	26.85	19.81	16.65
Method	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled

Table 4-31: Statistics and Basis Values for OHC1 Strength Data

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## 4.21 "10/80/10" Open-Hole Compression 2 (OHC2)

The OHC2 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For the normalized dataset, both environments failed the ADK test for batch equivalency. ANOVA was used to compute their basis values, and with three batches of data available these are estimates. Applying the modified CV, environments were not acceptable for pooling because the pooled dataset failed the Levene's test for equality of variances.

For the as-measured dataset, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Applying the modified CV, the environments are not acceptable for pooling because the pooled dataset failed the Levene's test for equality of variances.

There were no statistical outliers.

Statistics, basis values and estimates are given for the OHC2 strength data in Table 4-32. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-22.

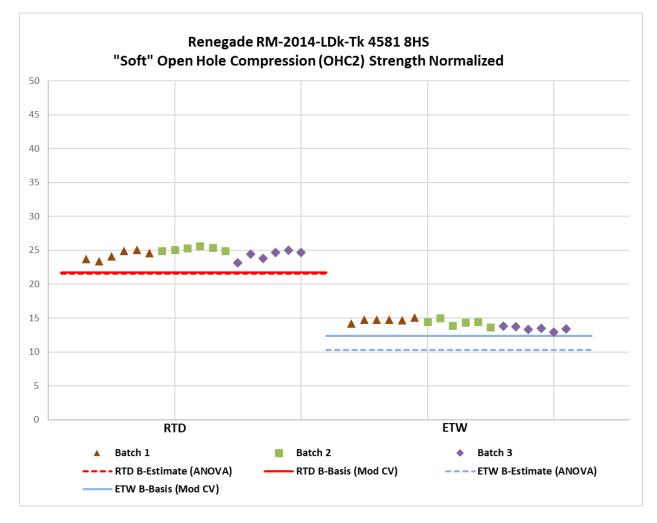


Figure 4-22: Batch Plot for OHC2 Normalized Strength

Open Hole Compression 2 (OHC2) Strength Basis Values and Statistics							
	Norm	alized	As-Mea	asured			
Env	RTD	ETW	RTD	ETW			
Mean	24.60	14.14	24.77	14.26			
Stdev	0.7019	0.6424	0.5881	0.7147			
CV	2.854	4.542	2.375	5.011			
Mod CV	6.000	6.271	6.000	6.506			
Min	23.18	12.90	23.60	12.90			
Max	25.60	15.06	25.60	15.30			
No. Batches	3	3	3	3			
No. Spec.	18	18	18	18			
	Basis	S Values and Estin	mates				
B-basis Value			23.53				
B-Estimate	21.53	10.27		9.862			
A-Estimate	19.35	7.509	22.17	6.723			
Method	ANOVA	ANOVA	Weibull	ANOVA			
Modified CV Basis Values and Estimates							
B-basis Value	21.68	12.39	21.83	12.43			
A-Estimate	19.62	11.15	19.76	11.13			
Method	Normal	Normal	Normal	Normal			

Table 4-32: Statistics and Basis Values for OHC2 Strength Data

## 4.22 "40/20/40" Open-Hole Compression 3 (OHC3)

The OHC3 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For both the normalized and as-measured datasets, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis values, and with three batches of data available these are estimates. Applying the modified CV, the ETW environment failed the ADK test for equivalency, therefore, basis values were not computed.

There were no statistical outliers.

Statistics, basis values and estimates are given for the OHC3 strength data in Table 4-33. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-23.

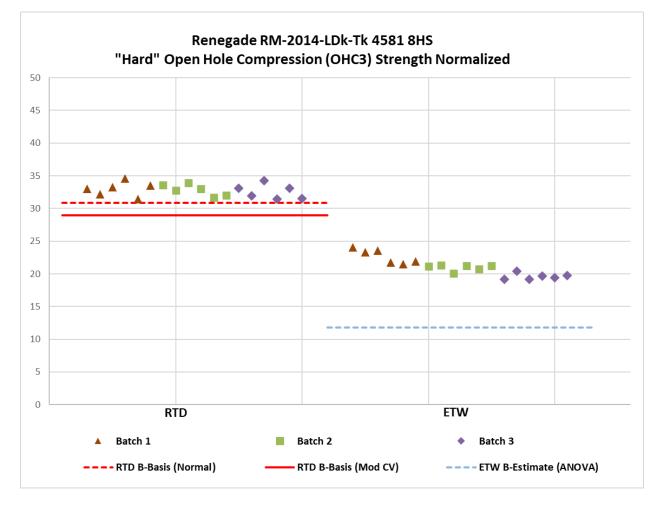


Figure 4-23: Batch Plot for OHC3 Normalized Strength

Open Hole Compression 3 (OHC3) Strength Basis Values and Statistics									
	Norm	alized	As-Me	asured					
Env	RTD	ETW	RTD	ETW					
Mean	32.80	21.08	33.20	21.41					
Stdev	0.9885	1.463	0.9098	1.473					
CV	3.014	6.939	2.741	6.884					
Mod CV	6.000	7.470	6.000	7.442					
Min	31.41	19.15	31.13	19.50					
Max	34.61	24.04	34.61	24.70					
No. Batches	3	3	3	3					
No. Spec.	18	18	18	18					
	Basis	s Values and Estin	nates						
B-basis Value	30.85		31.40						
B-Estimate		11.76		12.41					
A-Estimate	29.47	5.105	30.13	5.992					
Method	Normal	ANOVA	Normal	ANOVA					
	Modified C	/ Basis Values and	d Estimates						
B-basis Value	28.91		29.26						
A-Estimate	26.17	NA	26.48	NA					
Method	Normal		Normal						

Table 4-33: Statistics and Basis Values for OHC3 Strength Data

## 4.23 "25/50/25" Filled-Hole Compression 1 (FHC1)

The FHC1 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For both normalized and as-measured datasets, the ETW environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis values, and with three batches of data available these are estimates. Applying the modified CV, the ETW environment failed the ADK test for equivalency, therefore, basis values were not computed.

There were no statistical outliers.

Statistics, basis values and estimates are given for the FHC1 strength data in Table 4-34. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-24.

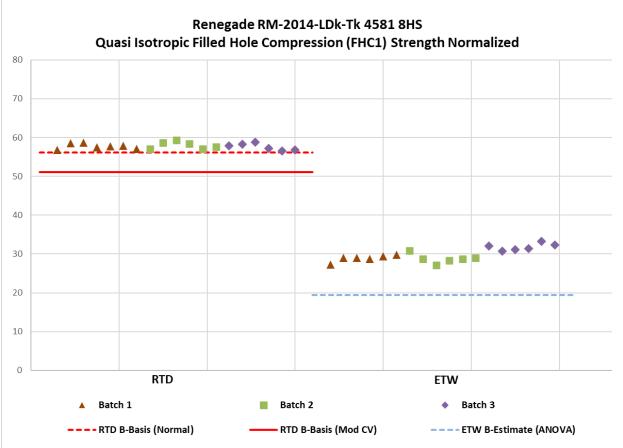


Figure 4-24: Batch plot for FHC1 Normalized Strength

Filled-Hole Compression 1 (FHC1) Strength Basis Values and Statistics									
	Norm	alized	As-Measured						
Env	RTD	ETW	RTD	ETW					
Mean	57.77	29.83	57.65	29.70					
Stdev	0.8143	1.737	0.8703	1.892					
CV	1.409	5.822	1.510	6.370					
Mod CV	6.000	6.911	6.000	7.185					
Min	56.59	27.10	56.04	26.49					
Max	59.35	33.31	59.12	33.69					
No. Batches	3	3	3	3					
No. Spec.	19	18	19	18					
	Bas	sis Value Estima	ates						
<b>B-Basis Value</b>	56.19		55.95						
<b>B-Estimate</b>		19.39		17.99					
A-Estimate	55.06	11.94	54.74	9.638					
Method	Normal	ANOVA	Normal	ANOVA					
	Modified (	CV Basis Value I	Estimates						
<b>B-Basis Value</b>	51.02		50.90						
A-Estimate	-Estimate 46.23		46.12	NA					
Method	Normal		Normal						

Table 4-34: Statistics and Basis Values for FHC1 Strength Data

#### 4.24 "10/80/10" Filled-Hole Compression 2 (FHC2)

The FHC2 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For the normalized dataset, the RTD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Applying the modified CV, both environments were not acceptable for pooling because the pooled dataset failed the Levene's test for equality of variances.

For the as-measured dataset, both environments were not acceptable for pooling because the pooled dataset failed the Anderson Darling test for normality. Applying the modified CV, both environments were not acceptable for pooling because the pooled dataset failed the Levene's test for equality of variances.

There was one statistical outlier. The lowest normalized value in batch one of the RTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset as well as in the as-measured dataset. It was retained for this analysis.

Statistics are given for the FHC2 strength data in Table 4-35. The normalized specimen data are shown graphically in Figure 4-25.

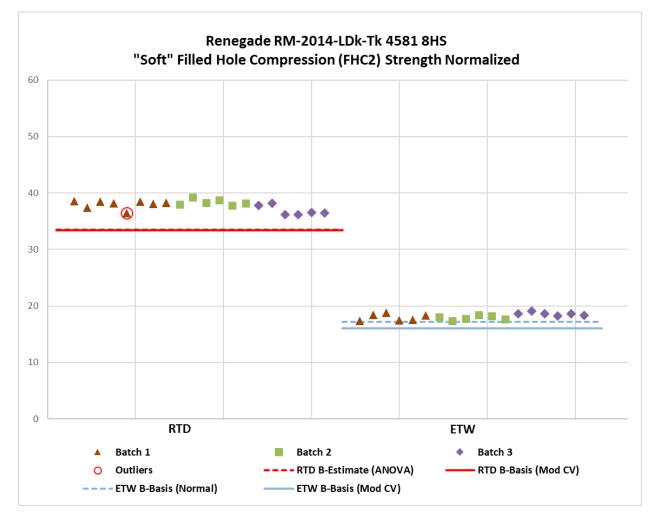


Figure 4-25: Batch plot for FHC2 Normalized Strength

Filled-Hole Compression 2 (FHC2) Strength Basis Values and Statistics									
	Norm	alized	As-Measured						
Env	RTD	ETW	RTD	ETW					
Mean	37.79	18.16	38.15	18.24					
Stdev	0.9216	0.5180	0.8499	0.6107					
CV	2.439	2.852	2.228	3.347					
Mod CV	6.000	6.000	6.000	6.000					
Min	36.16	17.33	36.34	17.15					
Max	39.27	19.12	39.38	19.17					
No. Batches	3	3	3	3					
No. Spec.	20	18	20	18					
	Ba	asis Value Estimat	tes						
B-Basis Value		17.14	36.51	17.04					
B-Estimate	33.45								
A-Estimate	30.35	16.42	35.34	16.18					
Method	ANOVA	Normal	Normal	Normal					
	Modified	CV Basis Value E	stimates						
B-Basis Value	33.42	16.01	33.74	16.08					
A-Estimate	30.32	14.49	30.60	14.55					
Method	Normal	Normal	Normal	Normal					

Table 4-35: Statistics and Basis Values for FHC2 Strength Data

## 4.25 "40/20/40" Filled-Hole Compression 3 (FHC3)

The FHC3 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For the normalized dataset, the RTD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Using the modified CV, there were no diagnostic test failures and both environments were acceptable for pooling.

For the as-measured dataset, the RTD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Using the modified CV, both environments were not acceptable for pooling because the pooled dataset failed the Levene's test for equality of variances.

There were three statistical outliers. The lowest normalized value in batch two of the RTD environment was an outlier for the batch and for the environment. It was an outlier in the normalized dataset as well as in the as-measured dataset. The lowest normalized value in batch one of the RTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset but not in the as-measured dataset. The lowest normalized value in batch one of the ETW environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset but not in the as-measured dataset. The lowest normalized value in batch one of the ETW environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset but not in the as-measured dataset. They were retained for this analysis.

Statistics, basis values and estimates are given for the FHC3 strength data in Table 4-36. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-26.

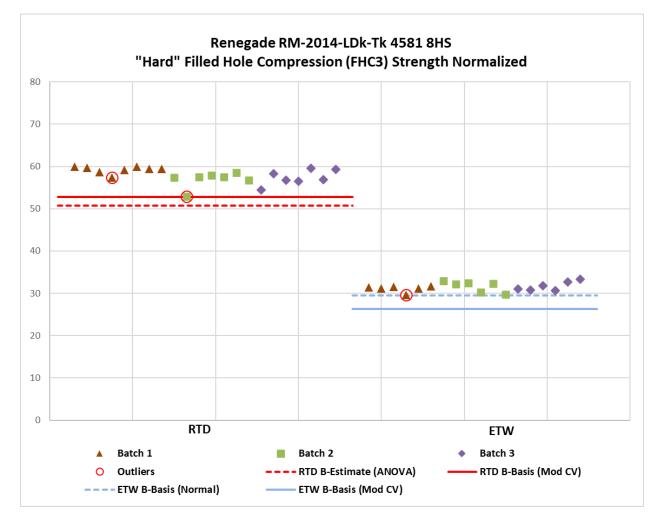


Figure 4-26: Batch Plot for FHC3 Normalized Strength

Filled-Hole Compression 3 (FHC3) Strength Basis Values and Statistics									
	Norm	alized	As-Measured						
Env	RTD	ETW	RTD	ETW					
Mean	57.89	31.48	58.56	31.81					
Stdev	1.783	1.037	1.960	1.021					
CV	3.080	3.294	3.347	3.210					
Mod CV	6.000	6.000	6.000	6.000					
Min	52.87	29.67	52.97	30.02					
Max	59.96	33.28	61.39	33.41					
No. Batches	3	3	3	3					
No. Spec.	22	18	22	18					
	Bas	sis Value Estima	ates						
<b>B-Basis Value</b>		29.44		29.80					
<b>B-Estimate</b>	50.69		50.87						
A-Estimate	45.54	27.99	45.37	28.37					
Method	ANOVA	Normal	ANOVA	Normal					
	Modified (	CV Basis Value	Estimates						
<b>B-Basis Value</b>	52.79	26.29	51.93	28.05					
A-Estimate	49.26	22.78	47.20	25.38					
Method	Pooled	Pooled	Normal	Normal					

Table 4-36: Statistics and Basis Values for FHC3 Strength Data

#### 4.26 "25/50/25" Single-Shear Bearing 1 (SSB1)

The SSB1 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For the normalized datasets, the ultimate strength test in the RTD condition failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Applying the modified CV, there were no diagnostic test failures, so both environmental conditions were acceptable for pooling for 2% offset strength and ultimate strength.

For the as-measured datasets, the environments were not acceptable for pooling for either of the properties because the pooled datasets failed the Levene's test for equality of variances. Applying the modified CV, there were no diagnostic test failures, so both environmental conditions were acceptable for pooling for 2% offset strength and ultimate strength.

There were two statistical outliers. The lowest normalized value in batch one of the 2% offset strength property, RTD environment was an outlier for the environment but not for the batch. It was outlier in the normalized dataset but in for the as-measured dataset. The lowest normalized value in batch three of the ultimate strength property, RTD environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset but not in the as-measured dataset. They were retained for this analysis.

Statistics, basis values and estimates are given for the SSB1 strength data in Table 4-37. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-27.

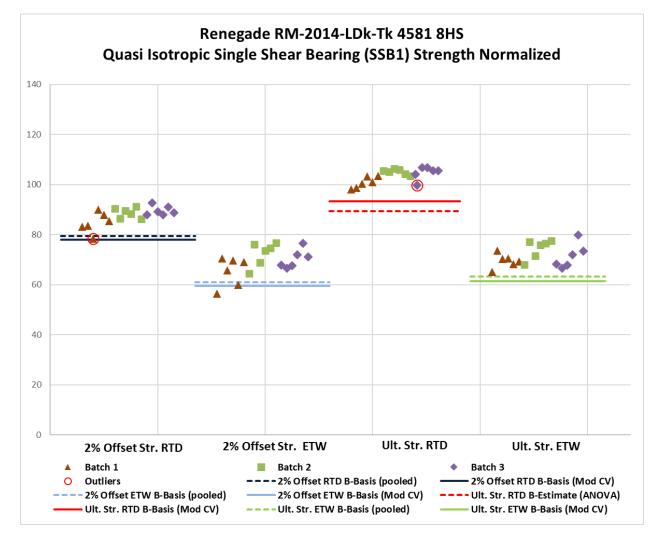


Figure 4-27: Batch Plot for SSB1 Normalized Strength

		Single	Shear Bearing 1	(SSB1) Strength E	Basis Values and S	Statistics		
	Normalized As-Measured							
Property	2% Offse	t Strength	Ultimate Strength		2% Offs	et Strength	Ultimate	Strength
Env	RTD	ETW	RTD	ETW	RTD	ETW	RTD	ETW
Mean	87.73	69.32	103.6	71.77	86.45	68.35	102.1	70.80
Stdev	3.444	5.490	2.811	4.252	2.191	4.915	1.963	3.990
CV	3.926	7.920	2.713	5.924	2.535	7.192	1.922	5.636
Mod CV	6.000	7.960	6.000	6.962	6.000	7.596	6.000	6.818
Min	78.43	56.46	98.11	65.15	80.77	58.72	97.03	64.87
Max	92.74	76.67	106.9	79.86	90.16	75.02	105.1	77.38
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18	18	18
			Bas	is Values and Est	imates			
B-basis Value	79.38	60.97		63.38	82.12	58.64	98.26	62.92
B-Estimate			89.50					
A-Estimate	73.70	55.29	79.42	57.43	79.06	51.77	95.52	57.34
Method	Pooled	Pooled	ANOVA	Normal	Normal	Normal	Normal	Normal
			Modified C	CV Basis Values a	nd Estimates			
B-basis Value	77.91	59.50	93.35	61.50	77.00	58.89	92.09	60.75
A-Estimate	71.23	52.82	86.36	54.51	70.57	52.46	85.26	53.91
Method	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled

Table 4-37: Statistics and Basis Values for SSB1 Strength Data

## 4.27 "10/80/10" Single-Shear Bearing 2 (SSB2)

The SSB2 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For the normalized datasets, the ultimate strength test in the RTD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Applying the modified CV there were no diagnostic test failures so both environments were acceptable for pooling. For the 2% offset strength test, both environments were not acceptable for pooling because the pooled dataset failed the Levene's test for equality of variances. Applying the modified CV there were no diagnostic test failures so both environments were acceptable for pooling because the pooled dataset failed the Levene's test for equality of variances. Applying the modified CV there were no diagnostic test failures so both environments were acceptable for pooling.

For the as-measured datasets, there were no diagnostic test failures for the ultimate strength test so both environments were acceptable for pooling. Applying the modified CV, the pooled dataset failed the Levene's test for equality of variances. The 2% offset strength pooled dataset failed the Levene's test for equality of variances, so environments were not acceptable for pooling. Applying the modified CV there were no diagnostic test failures so both environments were acceptable for pooling.

There were no statistical outliers.

Statistics, basis values and estimates are given for the SSB2 strength data in Table 4-38. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-28.

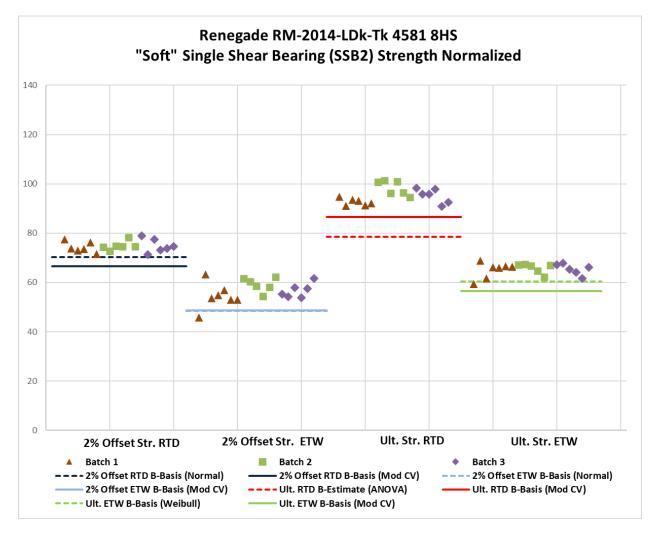


Figure 4-28: Batch Plot for SSB2 Normalized Strength

		Single	e Shear Bearing 2	(SSB2) Strength E	Basis Values and S	Statistics			
	Normalized					As-Measured			
Property	2% Offse	t Strength	Ultimate Strength		2% Offs	et Strength	Ultimate	Strength	
Env	RTD	ETW	RTD	ETW	RTD	ETW	RTD	ETW	
Mean	74.67	56.63	95.42	65.39	74.45	56.50	95.13	65.25	
Stdev	2.214	4.247	3.408	2.512	2.087	4.140	2.942	2.570	
CV	2.965	7.500	3.572	3.841	2.803	7.328	3.092	3.939	
Mod CV	6.000	7.750	6.000	6.000	6.000	7.664	6.000	6.000	
Min	71.22	45.68	90.86	59.42	71.45	46.16	90.52	60.05	
Max	78.90	63.23	101.4	68.92	78.24	64.17	100.2	69.94	
No. Batches	3	3	3	3	3	3	3	3	
No. Spec.	18	19	18	19	18	19	18	19	
			Bas	is Values and Est	imates				
B-basis Value	70.30	48.35		60.36	70.33	48.43	90.12	60.27	
B-Estimate			78.56						
A-Estimate	67.20	42.48	66.53	55.00	67.41	42.70	86.72	56.86	
Method	Normal	Normal	ANOVA	Weibull	Normal	Normal	Pooled	Pooled	
			Modified C	CV Basis Values a	nd Estimates		•	•	
B-basis Value	66.61	48.61	86.54	56.56	66.46	48.55	83.86		
A-Estimate	61.14	43.13	80.52	50.53	61.04	43.11	75.89	NA	
Method	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Normal		

Table 4-38: Statistics and Basis Values for SSB2 Strength Data

## 4.28 "40/20/40" Single-Shear Bearing 3 (SSB3)

The SSB3 data is normalized by cured ply thickness. Both normalized and as-measured statistics are provided. Tests were conducted in the following environmental conditions: RTD and ETW.

For both the normalized datasets, there were no diagnostic test failures in the ultimate strength test so both environment were acceptable for pooling. In the 2% offset strength test, the RTD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Applying the modified CV, there were no diagnostic test failures, so both environments were acceptable for pooling for the two tests.

For the as-measured datasets, for the ultimate strength test, environments were not acceptable for pooling because the pooled dataset failed the Levene's test for equality of variances. For the 2% offset strength test, the RTD environment failed the ADK test for batch equivalency. ANOVA was used to compute its basis value, and with three batches of data available this is an estimate. Applying the modified CV, there were no diagnostic test failures so both environments were acceptable for pooling for the two tests.

There was one statistical outlier. The lowest normalized value in batch one of the 2% offset dataset, ETW environment was an outlier for the batch but not for the environment. It was an outlier in the normalized dataset as well as in the as-measured dataset. It was retained for this analysis.

Statistics, basis values and estimates are given for the SSB3 strength data in Table 4-39. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-29.

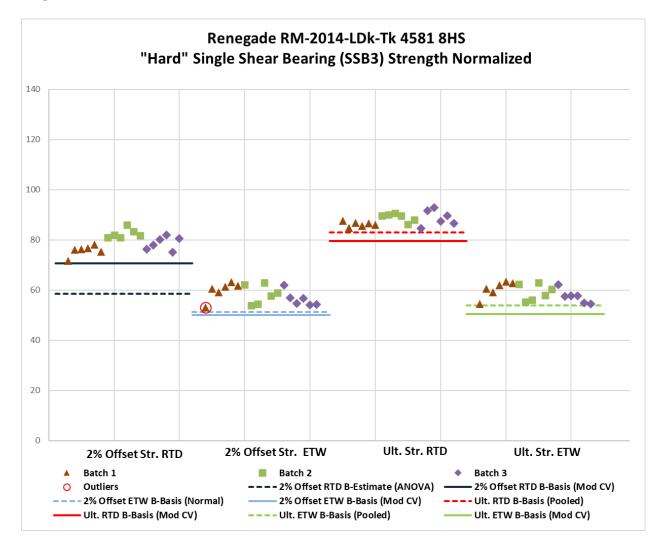


Figure 4-29: Batch	Plot for SSB3	8 Normalized Strength
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		Single Sl	near Bearing 3 (	SSB3) Strength	Basis Values an	d Statistics	•	
	Normalized As-M					As-Mea	asured	
Property	2%Offset	Strength	Ultimate	Strength	2%Offse	et Strength	Ultimate	Strength
Env	RTD	ETW	RTD	ETW	RTD	ETW	RTD	ETW
Mean	78.97	58.26	88.06	59.04	78.56	57.85	87.60	58.63
Stdev	3.571	3.526	2.385	3.170	3.376	3.459	2.177	3.090
CV	4.522	6.051	2.709	5.370	4.297	5.979	2.485	5.270
Mod CV	6.261	7.026	6.000	6.685	6.149	6.989	6.000	6.635
Min	71.59	53.13	84.66	54.42	71.91	52.67	84.51	54.09
Max	85.95	63.22	92.87	63.40	85.07	62.52	92.34	62.70
No. Batches	3	3	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18	18	18
			Basi	s Values and Es	timates			
B-basis Value		51.30	82.95	53.93		51.02	83.31	52.53
B-Estimate	58.47				61.44			
A-Estimate	43.83	46.37	79.47	50.46	49.23	46.19	80.26	48.20
Method	ANOVA	Normal	Pooled	Pooled	ANOVA	Normal	Normal	Normal
			Modified C	V Basis Values a	and Estimates			
B-basis Value	70.71	50.00	79.56	50.55	70.45	49.74	79.18	50.20
A-Estimate	65.08	44.37	73.78	44.77	64.93	44.22	73.45	44.47
Method	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled	Pooled

Table 4-39: Statistics and Basis Values for SSB3 Strength Data

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## 4.29 "25/50/25" Compression After Impact 1 (CAI1)

The CAI1 data is normalized by cured ply thickness. Basis values are not computed for this property. Testing is done only for the RTD condition. Only one batch of material was tested. There was no statistical analysis. Summary statistics are presented in Table 4-40 and the data are displayed graphically in Figure 4-30.

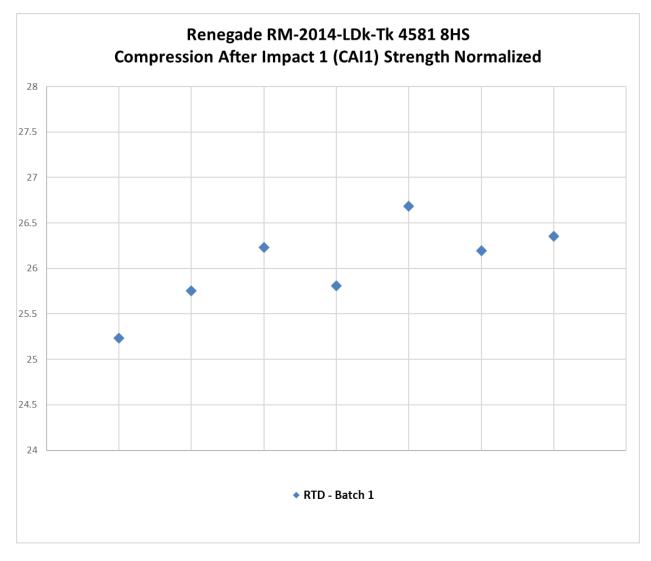


Figure 4-30: Plot for Compression After Impact Normalized Strength

Compression After Impact (CAI1) Strength							
	Normalized	As-Measured					
Env	RTD	RTD					
Mean	26.04	25.77					
Stdev	0.4757	0.4724					
CV	1.827	1.833					
Mod CV	6.000	6.000					
Min	25.23	24.94					
Max	26.69	26.43					
No. Batches	1	1					
No. Spec.	7	7					

Table 4-40: Statistics for	Compression After	r Impact Strength Data
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## 4.30 Interlaminar Tension Strength (ILT) and Curved Beam Strength (CBS)

The ILT data is not normalized. Data is reported on two properties: Interlaminar Tension Strength and Curved Beam Strength. Testing was done in the CTD, RTD and ETW conditions. Only one batch of material was tested. There was no statistical analysis. Basis values are not computed for these properties. Summary statistics are presented in Table 4-41 and the asmeasured data are displayed graphically in Figure 4-31.

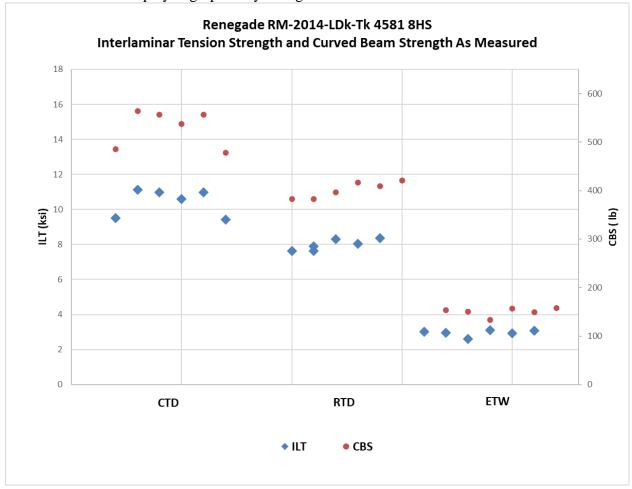


Figure 4-31: Plot for Interlaminar Tension and Curved Beam Strength

	Interlaminar Tension (ILT) Strength Statistics											
	Interlam	inar Tension Strer	ngth (ksi)	Cu	ved Beam Strength (lb)							
Env	CTD	RTD	ETW	CTD	RTD	ETW						
Mean	10.39	7.979	2.949	527.3	401.4	150.1						
Stdev	0.7086	0.3139	0.1836	35.31	16.63	9.060						
CV	6.823	3.935	6.227	6.696	4.143	6.035						
Mod CV	7.411	6.000	7.114	7.348	6.072	7.018						
Min	9.423	7.636	2.601	478.5	382.6	133.1						
Max	11.11	8.364	3.116	564.3	420.9	158.2						
No. Batches	1	1	1	1	1	1						
No. Spec.	7	6	6	7	6	6						

Table 4-41: Statistics for ILT and CBS Data

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#### 5. Outliers

Outliers were identified according to the standards documented in section 2.1.5, which are in accordance with the guidelines developed in section 8.3.3 of CMH-17-1G. An outlier may be an outlier in the normalized data, the as-measured data, or both. A specimen may be an outlier for the batch only (before pooling the three batches within a condition together) or for the condition (after pooling the three batches within a condition together) or both.

Approximately 5 out of 100 specimens will be identified as outliers due to the expected random variation of the data. This test is used only to identify specimens to be investigated for a cause of the extreme observation. Outliers that have an identifiable cause are removed from the dataset as they inject bias into the computation of statistics and basis values. Specimens that are outliers for the condition and in both the normalized and as-measured data are typically more extreme and more likely to have a specific cause and be removed from the dataset than other outliers. Specimens that are outliers only for the batch, but not the condition and specimens that are identified as outliers only for the normalized data or the as-measured data but not both, are typical of normal random variation.

All outliers identified were investigated to determine if a cause could be found. Outliers with causes were removed from the dataset and the remaining specimens were analyzed for this report. Information about specimens that were removed from the dataset along with the cause for removal is documented in the material property data report, NCAMP Test Report CAM-RP-2024-007 Rev N/C. Outliers for which no causes could be identified are listed in Table 5-1. These outliers were included in the analysis for their respective test properties.

Test	Condition	Batch	Saurinea No		Stre	ngth			Outlier	
Test	Condition	Batch	Specimen No.	Normalized	Value	As Measured	Value	High/Low	Batch	Condition
FC	CTD	С	FC-C-C2-1-CTD-11	Not an	Outlier	Yes	71.55	High	Yes	No
FHC2	RTD	А	FHC2-A-C2-1-RTD-1	Yes	36.46	Yes	36.84	Low	Yes	No
FHC3	RTD	В	FHC3-B-C1-1-RTD-2	Yes	52.87	Yes	52.97	Low	Yes	Yes
FHC3	RTD	А	FHC3-A-C1-1-RTD-4	Yes	57.42	Not an O	Dutlier	Low	Yes	No
FHC3	ETW	А	FHC3-A-C2-1-ETW-1	Yes	29.67	Not an O	Dutlier	Low	Yes	No
FHT1	CTD	С	FHT1-C-C1-1-CTD-1	Yes	50.53	Not an O	Dutlier	Low	Yes	No
FHT2	RTD	В	FHT2-B-C1-1-RTD-8	Yes	30.80	Not an O	Dutlier	Low	Yes	No
FHT2	ETW	А	FHT2-A-C1-1-ETW-12	Yes	16.35	Not an O	Dutlier	Low	Yes	Yes
IPS 0.2% Offset	ETW	С	IPS-C-C2-1-ETW-4	N	•	Yes	1.830	High	Yes	No
IPS 5% Strain	ETD	С	IPS-C-C2-1-ETD-3	11/2	NA		4.990	High	Yes	No
OHC1	RTD	А	OHC1-A-C2-1-RTD-4	Yes	30.30	Yes	29.94	Low	No	Yes
OHC1	RTD	С	OHC1-C-C2-1-RTD-1	Yes	32.56	Yes	32.90	High	Yes	No
OHC1	ETW	В	OHC1-B-C1-1-ETW-9	Yes	26.31	Yes	26.00	High	Yes	Yes
OHT2	CTD	В	OHT2-B-C1-1-CTD-1	Not an	Outlier	Yes	32.68	Low	Yes	Yes
OHT3	RTD	А	OHT3-A-C2-1-RTD-8	Yes	50.04	Yes	49.60	Low	Yes	No
OHT3	ETW	С	OHT3-C-C1-1-ETW-8	Not an	Outlier	Yes	39.60	Low	Yes	No
SBS1	RTD	В	SBS1-B-C2-1-RTD-1	N	•	Yes	7.810	Low	Yes	No
SBS1	ETW	С	SBS1-C-C1-1-ETW-2	192	-	Yes	4.040	High	No	Yes
SSB1 2% Offset	RTD	А	SSB1-A-C1-1-RTD-3	Yes	78.43	Not an O	Dutlier	Low	No	Yes
SSB1 Ult. Str.	RTD	С	SSB1-C-C1-1-RTD-2	Yes	99.80	Not an O	Dutlier	Low	Yes	No
SSB3 2% Offset	ETW	А	SSB3-A-C1-1-ETW-1	Yes	53.13	Yes	53.32	Low	Yes	No
UNC1	ETW	В	UNC1-B-C2-1-ETW-8	Yes	24.11	Not an O	Dutlier	Low	No	Yes
UNT2	RTD	С	UNT2-C-C2-1-RTD-11	Yes	37.76	Yes	38.80	Low	Yes	No
UNT3	RTD	С	UNT3-C-C1-1-RTD-8	Yes	90.55	Not an (	Dutlier	Low	Yes	No
WC	ETD	В	WC-B-C1-1-ETD-13	Not an	Outlier	Yes	57.50	High	Yes	No
WC	ETD	С	WC-C-C1-1-ETD-3	Not an	Outlier	Yes	47.10	Low	No	Yes
WT	CTD	В	WT-B-C2-1-CTD-1	Yes	125.3	Not an O	Dutlier	High	Yes	No
WT	RTD	С	WT-C-C1-1-RTD-2	Yes	114.5	Not an O	Dutlier	High	Yes	No
NA: Property not nor	malized									

Table 5-1: List of OutliersPage 110 of 111

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