WICHITA STATE UNIVERSITY NATIONAL INSTITUTE FOR AVIATION RESEARCH Report No: NCP-RP-2023-002 Rev A Report Date: February 12, 2025



NIA



# Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Uni-Directional Slit Tape (0.25 inch) Material Allowables Statistical Analysis Report

NCAMP Project Number: NPN 052101

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Report Date: February 12, 2025

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## 1. Introduction

This report contains statistical analysis of the Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape (0.25 inch) material property data published in NCAMP Test Report CAM-RP-2023-002 Rev N/C. The lamina and laminate material property data have been generated with NCAMP oversight through NCAMP Special Project Number NPN 052101 and also meet the requirements outlined in NCAMP Standard Operating Procedure NSP 100. The test panels, test specimens, and test setups have been inspected by NCAMP Authorized Inspection Representatives (AIR) and the testing has been witnessed by NCAMP Authorized Engineering Representative (AER).

B-Basis values, A-estimates, and B-estimates were calculated using a variety of techniques that are detailed in section two. The qualification material was utilizing NCAMP Material Specification NMS 397/3 Rev – dated January 24, 2024, NMS 397/3 lists the information for procurement. The qualification test panels were cured in accordance with NCAMP Process Specification NPS 83961AFP "C" cure cycle Rev - dated January 25, 2023. The NCAMP Test Plan NTP 3963Q1 Rev B was used for this qualification program.

The panels were fabricated at Advanced Technologies Lab for Aerospace Systems (ATLAS), National Institute for Aviation Research, Wichita State University, 1845 N. Fairmount, Wichita, KS 67260-0093. The testing was performed at the National Institute for Aviation Research (NIAR) in Wichita, Kansas.

Basis numbers are labeled as 'values' when the data meets all the requirements of CMH-17-1H. When those requirements are not met, they will be labeled as 'estimates.' When the data does not meet all requirements, the failure to meet these requirements is reported and the specific requirement(s) the data fails to meet is identified. The method used to compute the basis value is noted for each basis value provided. When appropriate, in addition to the traditional computational methods, values computed using the modified coefficient of variation method is also provided.

The material property data acquisition process is designed to generate basic material property data with sufficient pedigree for submission to Complete Documentation sections of the Composite Materials Handbook (CMH-17-1H).

Part fabricators that wish to utilize the material property data, allowables, and specifications may be able to do so by demonstrating the capability to reproduce the original material properties; a process known as equivalency. More information about this equivalency process including the test statistics and its limitations can be found in Section 6 of DOT/FAA/AR-03/19 and Section 8.4.1 of CMH-17-1H. The applicability of equivalency process must be evaluated on program-by-program basis by the applicant and certifying agency. The applicant and certifying agency must agree that the equivalency test plan along with the equivalency process described in Section 6 of DOT/FAA/AR-03/19 and Section 8.4.1 of CMH-17-1H are adequate for the given program.

Aircraft companies should not use the data published in this report without specifying NCAMP Material Specification NMS 397/3. NMS 397/3 has additional requirements that are listed in its prepreg process control document (PCD), fiber specification, fiber PCD, and other raw material specifications and PCDs which impose essential quality controls on the raw materials and raw material manufacturing equipment and processes. *Aircraft companies and certifying agencies should assume that the material property data published in this report is not applicable when the material is not procured to NCAMP Material Specification NMS 397/3. NMS 397/3 is a free, publicly available, non-proprietary aerospace industry material specification.* 

The data in this report is intended for general distribution to the public, either freely or at a price that does not exceed the cost of reproduction (e.g. printing) and distribution (e.g. postage).

Test Property	Abbreviation
Longitudinal Compression	LC
Longitudinal Tension	LT
Transverse Compression	TC
Transverse Tension	TT
In-Plane Shear	IPS
In-Plane Shear V-Notched	VNS
Short Beam Strength	SBS
Laminate Short Beam Strength	SBS1
Unnotched Tension	UNT
Unnotched Compression	UNC
Filled Hole Tension	FHT
Filled Hole Compression	FHC
Open Hole Tension	OHT
Open Hole Compression	OHC
Single Shear Bearing	SSB
Interlaminar Tension	ILT
Curved Beam Strength	CBS
Compression After Impact	CAI

# **1.1 Symbols and Abbreviations**

Table 1-1: Test Property Abbreviations

Test Property	Symbol
Longitudinal Compression Strength	F1 <sup>cu</sup>
Longitudinal Compression Modulus	E1 <sup>c</sup>
Longitudinal Compression Poisson's	<b>V</b> 12 <sup>C</sup>
Ratio	
Longitudinal Tension Strength	F1 <sup>tu</sup>
Longitudinal Tension Modulus	E1 <sup>t</sup>
Longitudinal Tension Poisson's Ratio	V <sub>12</sub> <sup>t</sup>
Transverse Compression Strength	F <sub>2</sub> <sup>cu</sup>
Transverse Compression Modulus	E <sub>2</sub> c
Transverse Tension Strength	$F_2^{tu}$
Transverse Tension Modulus	$E_2^t$
In-Plane Shear Ultimate Strength	$F_{12}^{su}$
In-Plane Shear Strength at 5% strain	F <sub>12</sub> <sup>s5%</sup>
	strain
In-Plane Shear Strength at 0.2% offset	F <sub>12</sub> <sup>s0.2%</sup>
In-Plane Shear Modulus	G <sub>12</sub> <sup>s</sup>

Table 1-2: Test Property Symbols

Environmental Condition	Abbreviation	Temperature
Cold Temperature Ambient	CTA	–65° F
Room Temperature Ambient	RTA	70° F
Elevated Temperature Ambient	ETA1	180° F
Elevated Temperature Ambient	ETA2	250° F
Elevated Temperature Wet	ETW1	180° F
Elevated Temperature Wet	ETW2	250° F

**Table 1-3: Environmental Conditions Abbreviations** 

Tests with a number immediately after the abbreviation indicate the lay-up:

1 refers to a 25/50/25 layup. This is also referred to as "Quasi-Isotropic" 2 refers to a 10/80/10 layup. This is also referred to as "Soft" 3 refers to a 50/40/10 layup. This is also referred to as "Hard"

EX: OHT1 is an open hole tension test with a 25/50/25 layup

Detailed information about the test methods and conditions used is given in NCAMP Test Report CAM-RP-2023-002 Rev A.

# **1.2 Pooling Across Environments**

When pooling across environments was allowable, the pooled co-efficient of variation was used. CMH17 STATS (CMH17 Approved **S**tatistical Analysis Program) was used to determine if pooling was allowable and to compute the pooled coefficient of variation for those tests. In these cases, the modified coefficient of variation based on the pooled data was used to compute the basis values.

When pooling across environments was not advisable because the data was not eligible for pooling and engineering judgment indicated there was no justification for overriding the result, then B-Basis values were computed for each environmental condition separately, which are also provided by CMH17 STATS.

## **1.3 Basis Value Computational Process**

The general form to compute engineering basis values is: basis value =  $\overline{X} - kS$  where k is a factor based on the sample size and the distribution of the sample data. There are many different methods to determine the value of k in this equation, depending on the sample size and the distribution of the data. In addition, the computational formula used for the standard deviation, S, may vary depending on the distribution of the data. The details of those different computations and when each should be used are in section 2.0.

# **1.4 Modified Coefficient of Variation (CV) Method**

A common problem with new material qualifications is that the initial specimens produced and tested do not contain all of the variability that will be encountered when the material is being produced in larger amounts over a lengthy period of time. This can result in setting basis values that are unrealistically high. The variability as measured in the qualification program is often lower than the actual material variability because of several reasons. The materials used in the qualification programs are usually manufactured within a short period of time, typically 2-3 weeks only, which is not representative of the production material. Some raw ingredients that are used to manufacture the multi-batch qualification materials may actually be from the same production batches or manufactured within a short period of time so the qualification materials, although regarded as multiple batches, may not truly be multiple batches so they are not representative of the actual production material variability.

The modified Coefficient of Variation (CV) used in this report is in accordance with section 8.4.4 of CMH-17-1H. It is a method of adjusting the original basis values downward in anticipation of the expected additional variation. Composite materials are expected to have a CV of at least 6%. The modified coefficient of variation (CV) method increases the measured coefficient of variation when it is below 8% prior to computing basis values. A higher CV will result in lower or more conservative basis values and lower specification limits. The use of the modified CV method is intended for a temporary period of time when there is minimal data available. When a sufficient number of production batches (approximately 8 to 15) have been produced and tested, the as-measured CV may be used so that the basis values and specification limits may be adjusted higher.

The material allowables in this report are calculated using both the as-measured CV and modified CV, so users have the choice of using either one. When the measured CV is greater than 8%, the modified CV method does not change the basis value. NCAMP recommended values make use of the modified CV method when it is appropriate for the data.

When the data fails the Anderson-Darling K-sample test for batch to batch variability or when the data fails the normality test, the modified CV method is not appropriate and no modified CV basis value will be provided. When the ANOVA method is used, it may produce excessively conservative basis values. When appropriate, a single batch or two batch estimate may be provided in addition to the ANOVA estimate.

In some cases a transformation of the data to fit the assumption of the modified CV resulted in the transformed data passing the ADK test and thus the data can be pooled only for the modified CV method.

NCAMP recommends that if a user decides to use the basis values that are calculated from as-measured CV, the specification limits and control limits be calculated with asmeasured CV also. Similarly, if a user decides to use the basis values that are calculated from modified CV, the specification limits and control limits be calculated with modified CV also. This will ensure that the link between material allowables, specification limits, and control limits is maintained.

# 2. Background

Statistical computations are performed with CMH17 STATS. Pooling across environments will be used whenever it is permissible according to CMH-17-1H guidelines. If pooling is not permissible, the results of a single point analysis provided by CMH17 STATS is included instead. If the data does not meet CMH-17-1H requirements for a single point analysis, estimates are created by a variety of methods depending on which is most appropriate for the dataset available. Specific procedures used are presented in the individual sections where the data is presented.

# 2.1 CMH17 STATS Statistical Formulas and Computations

This section contains the details of the specific formulas CMH17 STATS uses in its computations.

### 2.1.1 Basic Descriptive Statistics

The basic descriptive statistics shown are computed according to the usual formulas, which are shown below:

Mean:
$$\overline{X} = \sum_{i=1}^{n} \frac{X_i}{n}$$
Equation 1Std. Dev.: $S = \sqrt{\frac{1}{n-1} \sum_{i=1}^{n} (X_i - \overline{X})^2}$ Equation 2% Co. Variation: $\frac{S}{\overline{X}} \times 100$ Equation 3

Where *n* refers to the number of specimens in the sample and  $X_i$  refers to the individual specimen measurements.

### 2.1.2 Statistics for Pooled Data

Prior to computing statistics for the pooled dataset, the data is normalized to a mean of one by dividing each value by the mean of all the data for that condition. This transformation does not affect the coefficients of variation for the individual conditions.

### 2.1.2.1 Pooled Standard Deviation

The formula to compute a pooled standard deviation is given below:

Pooled Std. Dev.: 
$$S_{p} = \sqrt{\frac{\sum_{i=1}^{k} (n_{i} - 1)S_{i}^{2}}{\sum_{i=1}^{k} (n_{i} - 1)}}$$
Equation 4

Where *k* refers to the number of batches,  $S_i$  indicates the standard deviation of *i*<sup>th</sup> sample, and  $n_i$  refers to the number of specimens in the *i*<sup>th</sup> sample.

### 2.1.2.2 Pooled Coefficient of Variation

Since the mean for the normalized data is 1.0 for each condition, the pooled normalized data also has a mean of one. The coefficient of variation for the pooled normalized data is the pooled standard deviation divided by the pooled mean, as in equation 3. Since the mean for the pooled normalized data is one, the pooled coefficient of variation is equal to the pooled standard deviation of the normalized data.

Pooled Coefficient of Variation 
$$=\frac{S_p}{1}=S_p$$
 Equation 5

### 2.1.3 Basis Value Computations

Basis values are computed using the mean and standard deviation for that environment, as follows: The mean is always the mean for the environment, but if the data meets all requirements for pooling,  $S_p$  can be used in place of the standard deviation for the environment, S.

Basis Values:  

$$\frac{A - basis = \overline{X} - K_a S}{B - basis = \overline{X} - K_b S}$$
Equation 6

### 2.1.3.1 K-factor computations

 $K_a$  and  $K_b$  are computed according to the methodology documented in section 8.3.5 of CMH-17-1H. The approximation formulas are given below:

$$K_{a} = \frac{2.3263}{\sqrt{q(f)}} + \sqrt{\frac{1}{c_{A}(f) \cdot n_{j}}} + \left(\frac{b_{A}(f)}{2c_{A}(f)}\right)^{2}} - \frac{b_{A}(f)}{2c_{A}(f)}$$
Equation 7
$$K_{b} = \frac{1.2816}{\sqrt{q(f)}} + \sqrt{\frac{1}{c_{B}(f) \cdot n_{j}}} + \left(\frac{b_{B}(f)}{2c_{B}(f)}\right)^{2}} - \frac{b_{B}(f)}{2c_{B}(f)}$$
Equation 8

Where

r = the number of environments being pooled together

 $n_j$  = number of data values for environment j

$$\begin{split} N &= \sum_{j=1}^{r} n_{j} \\ f &= N - r \end{split} \\ & q(f) = 1 - \frac{2.323}{\sqrt{f}} + \frac{1.064}{f} + \frac{0.9157}{f\sqrt{f}} - \frac{0.6530}{f^{2}} \\ & \text{Equation 9} \\ & b_{B}(f) = \frac{1.1372}{\sqrt{f}} - \frac{0.49162}{f} + \frac{0.18612}{f\sqrt{f}} \\ & \text{Equation 10} \\ & c_{B}(f) = 0.36961 + \frac{0.0040342}{\sqrt{f}} - \frac{0.71750}{f} + \frac{0.19693}{f\sqrt{f}} \\ & \text{Equation 11} \\ & b_{A}(f) = \frac{2.0643}{\sqrt{f}} - \frac{0.95145}{f} + \frac{0.51251}{f\sqrt{f}} \\ & \text{Equation 12} \\ & c_{A}(f) = 0.36961 + \frac{0.0026958}{\sqrt{f}} - \frac{0.65201}{f} + \frac{0.011320}{f\sqrt{f}} \\ & \text{Equation 13} \end{split}$$

### 2.1.4 Modified Coefficient of Variation

The coefficient of variation is modified according to the following rules:

Modified CV = 
$$CV^* = \begin{cases} .06 & \text{if } CV < .04 \\ \frac{CV}{2} + .04 & \text{if } .04 \le CV < .08 \\ CV & \text{if } CV \ge .08 \end{cases}$$
 Equation 14

This is converted to percent by multiplying by 100%.

 $CV^*$  is used to compute a modified standard deviation  $S^*$ .

$$S^* = CV^* \cdot \overline{X}$$
 Equation 15

To compute the pooled standard deviation based on the modified CV:

$$S_p^* = \sqrt{\frac{\sum_{i=1}^k \left( (n_i - 1) \left( CV_i^* \cdot \overline{X}_i \right)^2 \right)}{\sum_{i=1}^k (n_i - 1)}}$$
Equation 16

The A-basis and B-basis values under the assumption of the modified CV method are computed by replacing S with S $^{\!\star}$ 

### 2.1.4.1 Transformation of data based on Modified CV

In order to determine if the data would pass the diagnostic tests under the assumption of the modified CV, the data must be transformed such that the batch means remain the

same while the standard deviation of transformed data (all batches) matches the modified standard deviation.

To accomplish this requires a transformation in two steps:

Step 1: Apply the modified CV rules to each batch and compute the modified standard deviation  $S_i^* = CV^* \cdot \overline{X}_i$  for each batch. Transform the individual data values (*X<sub>ij</sub>*) in each batch as follows:

$$X'_{ij} = C_i \left( X_{ij} - \overline{X}_i \right) + \overline{X}_i$$
Equation 17
$$C_i = \frac{S_i^*}{S_i}$$
Equation 18

Run the Anderson-Darling k-sample test for batch equivalence (see section 2.1.6) on the transformed data. If it passes, proceed to step 2. If not, stop. The data cannot be pooled.

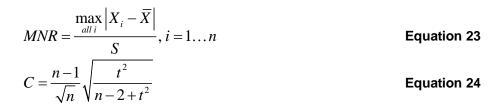
Step 2: Another transformation is needed as applying the modified CV to each batch leads to a larger CV for the combined data than when applying the modified CV rules to the combined data (due to the addition of between batch variation when combining data from multiple batches). In order to alter the data to match  $S^*$ , the transformed data is transformed again, this time setting using the same value of C' for all batches.

$X_{ij}'' = C' \left( X_{ij}' - \overline{X}_i \right) + \overline{X}_i$	Equation 19
$C' = \sqrt{\frac{SSE^*}{SSE'}}$	Equation 20
$SSE^* = (n-1)(CV^* \cdot \overline{X})^2 - \sum_{i=1}^k n_i (\overline{X}_i - \overline{X})^2$	Equation 21
$SSE' = \sum_{i=1}^{k} \sum_{j=1}^{n_i} \left( X'_{ij} - \overline{X}_i \right)^2$	Equation 22

Once this second transformation has been completed, the k-sample Anderson Darling test for batch equivalence can be run on the transformed data to determine if the modified co-efficient of variation will permit pooling of the data.

### 2.1.5 Determination of Outliers

All outliers are identified in text and graphics. If an outlier is removed from the dataset, it will be specified and the reason why will be documented in the text. Outliers are identified using the Maximum Normed Residual Test for Outliers as specified in section 8.3.3 of CMH-17-1H.



where t is the  $1-\frac{.05}{2n}$  quartile of a t distribution with n-2 degrees of freedom, n being the total number of data values.

If MNR > C, then the  $X_i$  associated with the MNR is considered to be an outlier. If an outlier exists, then the  $X_i$  associated with the MNR is dropped from the dataset and the MNR procedure is applied again. This process is repeated until no outliers are detected. Additional information on this procedure can be found in references 1 and 2.

### 2.1.6 The k-Sample Anderson Darling Test for Batch Equivalency

The k-sample Anderson-Darling test is a nonparametric statistical procedure that tests the hypothesis that the populations from which two or more groups of data were drawn are identical. The distinct values in the combined data set are ordered from smallest to largest, denoted  $z_{(1)}, z_{(2)}, \ldots z_{(L)}$ , where *L* will be less than n if there are tied observations. These rankings are used to compute the test statistic.

The k-sample Anderson-Darling test statistic is:

$$ADK = \frac{n-1}{n^{2}(k-1)} \sum_{i=1}^{k} \left[ \frac{1}{n_{i}} \sum_{j=1}^{L} h_{j} \frac{\left(nF_{ij} - n_{i}H_{j}\right)^{2}}{H_{j}\left(n - H_{j}\right) - \frac{nh_{j}}{4}} \right]$$
Equation 25

Where

 $n_i$  = the number of test specimens in each batch

 $n = n_1 + n_2 + \ldots + n_k$ 

 $h_j$  = the number of values in the combined samples equal to  $z_{(j)}$ 

 $H_j$  = the number of values in the combined samples less than  $z_{(j)}$  plus ½ the number of values in the combined samples equal to  $z_{(j)}$ 

 $F_{ij}$  = the number of values in the *i*<sup>th</sup> group which are less than  $z_{(j)}$  plus ½ the number of values in this group which are equal to  $z_{(j)}$ .

The critical value for the test statistic at  $1-\alpha$  level is computed:

 $ADC = 1 + \sigma_n \left[ z_{\alpha} + \frac{0.678}{\sqrt{k-1}} - \frac{0.362}{k-1} \right]$  Equation 26

This formula is based on the formula in reference 3 at the end of section 5, using a Taylor's expansion to estimate the critical value via the normal distribution rather than using the t distribution with k-1 degrees of freedom.

$$\sigma_n^2 = VAR(ADK) = \frac{an^3 + bn^2 + cn + d}{(n-1)(n-2)(n-3)(k-1)^2}$$
 Equation 27

With

$$a = (4g - 6)(k - 1) + (10 - 6g)S$$
  

$$b = (2g - 4)k^{2} + 8Tk + (2g - 14T - 4)S - 8T + 4g - 6$$
  

$$c = (6T + 2g - 2)k^{2} + (4T - 4g + 6)k + (2T - 6)S + 4T$$
  

$$d = (2T + 6)k^{2} - 4Tk$$
  

$$S = \sum_{i=1}^{k} \frac{1}{n_{i}}$$
  

$$T = \sum_{i=1}^{n-1} \frac{1}{i}$$
  

$$g = \sum_{i=1}^{n-2} \sum_{i=i+1}^{n-1} \frac{1}{(n-i)j}$$

The data is considered to have failed this test (i.e. the batches are not from the same population) when the test statistic is greater than the critical value. For more information on this procedure, see reference 3.

### 2.1.7 The Anderson Darling Test for Normality

**Normal Distribution:** A two parameter ( $\mu$ ,  $\sigma$ ) family of probability distributions for which the probability that an observation will fall between *a* and *b* is given by the area under the curve between a and b:

$$F(x) = \int_{a}^{b} \frac{1}{\sigma\sqrt{2\pi}} e^{-\frac{(x-\mu)^{2}}{2\sigma^{2}}} dx$$
 Equation 28

A normal distribution with parameters ( $\mu$ ,  $\sigma$ ) has population mean  $\mu$  and variance  $\sigma^2$ .

The normal distribution is considered by comparing the cumulative normal distribution function that best fits the data with the cumulative distribution function of the data. Let

$$z_{(i)} = \frac{x_{(i)} - \overline{x}}{s}$$
, for i = 1,...,n Equation 29

where  $x_{(i)}$  is the smallest sample observation,  $\overline{x}$  is the sample average, and s is the sample standard deviation.

The Anderson Darling test statistic (AD) is:

$$AD = \sum_{i=1}^{n} \frac{1-2i}{n} \left\{ \ln \left[ F_0(z_{(i)}) \right] + \ln \left[ 1 - F_0(z_{(n+1-i)}) \right] \right\} - n$$
 Equation 30

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Where  $F_0$  is the standard normal distribution function. The observed significance level (OSL) is

$$OSL = \frac{1}{1 + e^{-0.48 + 0.78 \ln(AD^*) + 4.58 AD^*}}, \quad AD^* = \left(1 + \frac{4}{n} - \frac{25}{n^2}\right) AD \quad \text{Equation 31}$$

This OSL measures the probability of observing an Anderson-Darling statistic at least as extreme as the value calculated if, in fact, the data are a sample from a normal population. If OSL > 0.05, the data is considered sufficiently close to a normal distribution.

### 2.1.8 Levene's Test for Equality of Coefficient of Variation

Levene's test performs an Analysis of Variance on the absolute deviations from their sample medians. The absolute value of the deviation from the median is computed for each data value.  $w_{ij} = |y_{ij} - \tilde{y}_i|$  An F-test is then performed on the transformed data values as follows:

$$F = \frac{\sum_{i=1}^{k} n_i (\overline{w}_i - \overline{w})^2 / (k-1)}{\sum_{i=1}^{k} \sum_{j=1}^{n_i} (w_{ij} - \overline{w}_i)^2 / (n-k)}$$
 Equation 32

If this computed F statistic is less than the critical value for the F-distribution having k-1 numerator and n-k denominator degrees of freedom at the 1- $\alpha$  level of confidence, then the data is not rejected as being too different in terms of the co-efficient of variation. CMH-17 STATS provides the appropriate critical values for F at  $\alpha$  levels of 0.10, 0.05, 0.025, and 0.01. For more information on this procedure, see references 4 and 5.

### 2.1.9 Distribution Tests

In addition to testing for normality using the Anderson-Darling test (see 2.1.7), CMH17 STATS also tests to see if the Weibull or Lognormal distribution is a good fit for the data.

Each distribution is considered using the Anderson-Darling test statistic which is sensitive to discrepancies in the tail regions. The Anderson-Darling test compares the cumulative distribution function for the distribution of interest with the cumulative distribution function of the data.

An observed significance level (OSL) based on the Anderson-Darling test statistic is computed for each test. The OSL measures the probability of observing an Anderson-Darling test statistic at least as extreme as the value calculated if the distribution under consideration is in fact the underlying distribution of the data. In other words, the OSL is the probability of obtaining a value of the test statistic at least as large as that obtained if the hypothesis that the data are actually from the distribution being tested is true. If the OSL is less than or equal to 0.05, then the assumption that the data are from the distribution being tested is rejected with at most a five percent risk of being in error.

If the normal distribution has an OSL greater than 0.05, then the data is assumed to be from a population with a normal distribution. If not, then if either the Weibull or lognormal distributions has an OSL greater than 0.05, then one of those can be used. If neither of these distributions has an OSL greater than 0.05, a non-parametric approach is used.

In what follows, unless otherwise noted, the sample size is denoted by n, the sample observations by  $x_1, ..., x_n$ , and the sample observations ordered from least to greatest by  $x_{(1)}, ..., x_{(n)}$ .

# 2.1.9.1 One-sided B-basis tolerance factors, $k_B$ , for the normal distribution when sample size is greater than 15.

The exact computation of k<sub>B</sub> values is  $1/\sqrt{n}$  times the 0.95th quantile of the noncentral t-distribution with noncentrality parameter  $1.282\sqrt{n}$  and n – 1 degrees of freedom. Since this in not a calculation that Excel can handle, the following approximation to the k<sub>B</sub> values is used:

$$k_B \approx 1.282 + \exp\{0.958 - 0.520\ln(n) + 3.19/n\}$$
 Equation 33

This approximation is accurate to within 0.2% of the tabulated values for sample sizes greater than or equal to 16.

### 2.1.9.2 One-sided A-basis tolerance factors, $k_A$ , for the normal distribution

The exact computation of  $k_A$  values is  $1/\sqrt{n}$  times the 0.95th quantile of the noncentral t-distribution with noncentrality parameter  $2.326\sqrt{n}$  and n - 1 degrees of freedom (Reference 11). Since this is not a calculation that Excel can handle easily, the following approximation to the  $k_A$  values is used:

$$k_A \approx 2.326 + \exp\{1.34 - 0.522\ln(n) + 3.87/n\}$$
 Equation 34

This approximation is accurate to within 0.2% of the tabulated values for sample sizes greater than or equal to 16.

### 2.1.9.3 Two-parameter Weibull Distribution

A probability distribution for which the probability that a randomly selected observation from this population lies between *a* and *b*  $(0 < a < b < \infty)$  is given by

$$e^{-\left(\frac{a}{\alpha}\right)^{\beta}}-e^{-\left(\frac{b}{\alpha}\right)^{\beta}}$$

Equation 35

where  $\alpha$  is called the scale parameter and  $\beta$  is called the shape parameter.

In order to compute a check of the fit of a data set to the Weibull distribution and compute basis values assuming Weibull, it is first necessary to obtain estimates of the population shape and scale parameters (Section 2.1.9.3.1). Calculations specific to the goodness-of-fit test for the Weibull distribution are provided in section 2.1.9.3.2.

## 2.1.9.3.1 Estimating Weibull Parameters

This section describes the *maximum likelihood* method for estimating the parameters of the two-parameter Weibull distribution. The maximum-likelihood estimates of the shape and scale parameters are denoted  $\hat{\beta}$  and  $\hat{\alpha}$ . The estimates are the solution to the pair of equations:

$$\hat{\alpha}\hat{\beta}n - \frac{\hat{\beta}}{\hat{\alpha}^{\hat{\beta}-1}} \sum_{i=1}^{n} x_{i}^{\hat{\beta}} = 0 \qquad \text{Equation 36}$$

$$\frac{n}{\hat{\beta}} - n\ln\hat{\alpha} + \sum_{i=1}^{n} \ln x_{i} - \sum_{i=1}^{n} \left[\frac{x_{i}}{\hat{\alpha}}\right]^{\hat{\beta}} \left(\ln x_{i} - \ln\hat{\alpha}\right) = 0 \qquad \text{Equation 37}$$

CMH17 STATS solves these equations numerically for  $\hat{\beta}$  and  $\hat{\alpha}$  in order to compute basis values.

### 2.1.9.3.2 Goodness-of-fit test for the Weibull distribution

The two-parameter Weibull distribution is considered by comparing the cumulative Weibull distribution function that best fits the data with the cumulative distribution function of the data. Using the shape and scale parameter estimates from section 2.1.9.3.1, let

$$z_{(i)} = \left[ x_{(i)} / \hat{\alpha} \right]^{\hat{\beta}}$$
, for  $i = 1, ..., n$  Equation 38

The Anderson-Darling test statistic is

 $AD = \sum_{i=1}^{n} \frac{1-2i}{n} \Big[ \ln \Big[ 1 - \exp(-z_{(i)}) \Big] - z_{(n+1-i)} \Big] - n$  Equation 39

and the observed significance level is

$$OSL = 1/\{1 + exp[-0.10 + 1.24 \ln(AD^*) + 4.48 AD^*]\}$$
 Equation 40

where

$$AD^* = \left(1 + \frac{0.2}{\sqrt{n}}\right)AD$$
 Equation 41

This OSL measures the probability of observing an Anderson-Darling statistic at least as extreme as the value calculated if in fact the data is a sample from a two-parameter Weibull distribution. If OSL  $\leq$  0.05, one may conclude (at a five percent risk of being in error) that the population does not have a two-parameter Weibull distribution. Otherwise, the hypothesis that the population has a two-parameter Weibull distribution is not rejected. For further information on these procedures, see reference 6.

### 2.1.9.3.3 Basis value calculations for the Weibull distribution

For the two-parameter Weibull distribution, the B-basis value is

 $B = \hat{q}e^{\left(-\frac{V}{\hat{\beta}\sqrt{n}}\right)}$ 

where

 $\hat{q} = \hat{\alpha} \left( 0.10536 \right)^{\frac{1}{\beta}}$ 

To calculate the A-basis value, substitute the equation below for the equation above.  $\hat{q} = \hat{\alpha}(0.01005)^{1/\beta}$  Equation 44

V is the value in Table 2-1 when the sample size is less than 16. For sample sizes of 16 or larger, a numerical approximation to the V values is given in the two equations immediately below.

$$V_B \approx 3.803 + \exp\left[1.79 - 0.516\ln(n) + \frac{5.1}{n-1}\right]$$
 Equation 45

Equation 43

Equation 42

$$V_A \approx 6.649 + \exp\left[2.55 - 0.526\ln(n) + \frac{4.76}{n}\right]$$

**Equation 46** 

This approximation is accurate within 0.5% of the tabulated values for n greater than or equal to 16.

Weibull Dist. K Factors for N<16			
Ν	B-basis	A-basis	
2	690.804	1284.895	
3	47.318	88.011	
4	19.836	36.895	
5	13.145	24.45	
6	10.392	19.329	
7	8.937	16.623	
8	8.047	14.967	
9	7.449	13.855	
10	6.711	12.573	
11	6.477	12.093	
12	6.286	11.701	
13	6.127	11.375	
14	5.992	11.098	
15	5.875	10.861	

 Table 2-1: Weibull Distribution Basis Value Factors

## 2.1.9.4 Lognormal Distribution

A probability distribution for which the probability that an observation selected at random from this population falls between a and b  $(0 < a < b < \infty)$  is given by the area under the normal distribution between ln(a) and ln(b).

The lognormal distribution is a positively skewed distribution that is simply related to the normal distribution. If something is lognormally distributed, then its logarithm is normally distributed. The natural (base e) logarithm is used.

### 2.1.9.4.1 Goodness-of-fit test for the Lognormal distribution

In order to test the goodness-of-fit of the lognormal distribution, take the logarithm of the data and perform the Anderson-Darling test for normality from Section 2.1.7. Using the natural logarithm, replace Equation 29 above with Equation 47 below:

$$z_{(i)} = \frac{\ln(x_{(i)}) - \overline{x}_L}{s_L}, \quad \text{for } i = 1, \dots, n$$
 Equation 47

where  $x_{(i)}$  is the i<sup>th</sup> smallest sample observation,  $\overline{x}_L$  and  $s_L$  are the mean and standard deviation of the  $ln(x_i)$  values.

The Anderson-Darling statistic is then computed using Equation 30 above and the observed significance level (OSL) is computed using Equation 31 above. This OSL measures the probability of observing an Anderson-Darling statistic at least as extreme as the value calculated if in fact the data are a sample from a lognormal distribution. If

 $OSL \le 0.05$ , one may conclude (at a five percent risk of being in error) that the population is not lognormally distributed. Otherwise, the hypothesis that the population is lognormally distributed is not rejected. For further information on these procedures, see reference 6.

### 2.1.9.4.2 Basis value calculations for the Lognormal distribution

If the data set is assumed to be from a population with a lognormal distribution, basis values are calculated using the equation above in section 2.1.3. However, the calculations are performed using the logarithms of the data rather than the original observations. The computed basis values are then transformed back to the original units by applying the inverse of the log transformation.

### 2.1.10 Non-parametric Basis Values

Non-parametric techniques do not assume any particularly underlying distribution for the population the sample comes from. It does require that the batches be similar enough to be grouped together, so the ADK test must have a positive result. While it can be used instead of assuming the normal, lognormal or Weibull distribution, it typically results in lower basis values. One of following two methods should be used, depending on the sample size.

### 2.1.10.1 Non-parametric Basis Values for large samples

The required sample sizes for this ranking method differ for A and B basis values. A sample size of at least 29 is needed for the B-basis value while a sample size of 299 is required for the A-basis.

To calculate a B-basis value for n > 28, the value of r is determined with the following formulas:

For B-basis values:

$$r_{B} = \frac{n}{10} - 1.645 \sqrt{\frac{9n}{100}} + 0.23$$
 Equation 48

For A-Basis values:

$$r_A = \frac{n}{100} - 1.645 \sqrt{\frac{99n}{10,000}} + 0.29 + \frac{19.1}{n}$$
 Equation 49

The formula for the A-basis values should be rounded to the nearest integer. This approximation is exact for most values and for a small percentage of values (less than 0.2%), the approximation errs by one rank on the conservative side.

The B-basis value is the  $r_B^{th}$  lowest observation in the data set, while the A-basis value is the  $r_A^{th}$  lowest observation in the data set. For example, in a sample of size n = 30, the

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lowest (r = 1) observation is the B-basis value. Further information on this procedure may be found in reference 7.

### 2.1.10.2 Non-parametric Basis Values for small samples

The Hanson-Koopmans method (references 8 and 9) is used for obtaining a B-basis value for sample sizes not exceeding 28 and A-basis values for sample sizes less than 299. This procedure requires the assumption that the observations are a random sample from a population for which the logarithm of the cumulative distribution function is concave, an assumption satisfied by a large class of probability distributions. There is substantial empirical evidence that suggests that composite strength data satisfies this assumption.

The Hanson-Koopmans B-basis value is:

$$B = x_{(r)} \left[ \frac{x_{(1)}}{x_{(r)}} \right]^k$$

The A-basis value is:

$$A = x_{(n)} \left[ \frac{x_{(1)}}{x_{(n)}} \right]^k$$

Equation 50

Equation 51

where  $x_{(n)}$  is the largest data value,  $x_{(1)}$  is the smallest, and  $x_{(r)}$  is the r<sup>th</sup> largest data value. The values of r and k depend on n and are listed in Table 2-2. This method is not used for the B-basis value when  $x_{(r)} = x_{(1)}$ .

The Hanson-Koopmans method can be used to calculate A-basis values for n less than 299. Find the value  $k_A$  corresponding to the sample size n in Table 2-3. For an A-basis value that meets all the requirements of CMH-17-1H, there must be at least five batches represented in the data and at least 55 data points. For a B-basis value, there must be at least three batches represented in the data and at least 18 data points.

B-Basis Hanson-Koopmans Table			
n	r	k	
2	2	35.177	
2 3	2 3 4	7.859	
4		4.505	
5	4 5 5	4.101	
6	5	3.064	
7	5	2.858	
8	6	2.382	
9	6	2.253	
10	6	2.137	
10 11 12	6 6 7 7 7 7	2.253 2.137 1.897 1.814 1.738 1.599	
12	7	1.814	
13	7	1.738	
14 15	8	1.599	
15	8	1.540 1.540 1.485 1.434 1.354	
16	8	1.485	
17	8	1.434	
18	9	1.354	
19	9	1.311	
20	10	1.311 1.253 1.218	
21	10	1.218	
22	10	1.184	
23	11	1.184 1.143	
24	11	1.114 1.087	
25	11	1.087	
26	11	1.060	
27	11	1.035	
28	12	1.010	

 Table 2-2: B-Basis Hanson-Koopmans Table

	A-Basis	Hanson-	Koopmans	Table	
n	k	n	k	n	k
2	80.00380	38	1.79301	96	1.32324
3	16.91220	39	1.77546	98	1.31553
4	9.49579	40	1.75868	100	1.30806
5	6.89049	41	1.74260	105	1.29036
6	5.57681	42	1.72718	110	1.27392
7	4.78352	43	1.71239	115	1.25859
8	4.25011	44	1.69817	120	1.24425
9	3.86502	45	1.68449	125	1.23080
10	3.57267	46	1.67132	130	1.21814
11	3.34227	47	1.65862	135	1.20620
12	3.15540	48	1.64638	140	1.19491
13	3.00033	49	1.63456	145	1.18421
14	2.86924	50	1.62313	150	1.17406
15	2.75672	52	1.60139	155	1.16440
16	2.65889	54	1.58101	160	1.15519
17	2.57290	56	1.56184	165	1.14640
18	2.49660	58	1.54377	170	1.13801
19	2.42833	60	1.52670	175	1.12997
20	2.36683	62	1.51053	180	1.12226
21	2.31106	64	1.49520	185	1.11486
22	2.26020	66	1.48063	190	1.10776
23	2.21359	68	1.46675	195	1.10092
24	2.17067	70	1.45352	200	1.09434
25	2.13100	72	1.44089	205	1.08799
26	2.09419	74	1.42881	210	1.08187
27	2.05991	76	1.41724	215	1.07595
28	2.02790	78	1.40614	220	1.07024
29	1.99791	80	1.39549	225	1.06471
30	1.96975	82	1.38525	230	1.05935
31	1.94324	84	1.37541	235	1.05417
32	1.91822	86	1.36592	240	1.04914
33	1.89457	88	1.35678	245	1.04426
34	1.87215	90	1.34796	250	1.03952
35	1.85088	92	1.33944	275	1.01773
36	1.83065	94	1.33120	299	1.00000
37	1.81139				

Table 2-3: A-Basis Hanson-Koopman	3 Table
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### 2.1.11 Analysis of Variance (ANOVA) Basis Values

ANOVA is used to compute basis values when the batch to batch variability of the data does not pass the ADK test. Since ANOVA makes the assumption that the different batches have equal variances, the data is checked to make sure the assumption is valid. Levene's test for equality of variance is used (see section 2.1.8). If the dataset fails Levene's test, the basis values computed are likely to be conservative. Thus this method can still be used but the values produced will be listed as estimates.

### 2.1.11.1 Calculation of basis values using ANOVA

The following calculations address batch-to-batch variability. In other words, the only grouping is due to batches and the k-sample Anderson-Darling test (Section 2.1.6) indicates that the batch to batch variability is too large to pool the data. The method is based on the one-way analysis of variance random-effects model, and the procedure is documented in reference 10.

ANOVA separates the total variation (called the sum of squares) of the data into two sources: between batch variation and within batch variation.

First, statistics are computed for each batch, which are indicated with a subscript  $(n_i, \overline{x_i}, s_i^2)$  while statistics that were computed with the entire dataset do not have a subscript. Individual data values are represented with a double subscript, the first number indicated the batch and the second distinguishing between the individual data values within the batch. *k* stands for the number of batches in the analysis. With these statistics, the Sum of Squares Between batches (SSB) and the Total Sum of Squares (SST) are computed:

 $SSB = \sum_{i=1}^{k} n_i \overline{x}_i^2 - n \overline{x}^2$ Equation 52  $SST = \sum_{i=1}^{k} \sum_{j=1}^{n_i} x_{ij}^2 - n \overline{x}^2$ Equation 53

The within-batch, or error, sum of squares (SSE) is computed by subtraction

Next, the mean sums of squares are computed:

$MSB = \frac{SSB}{k-1}$	Equation 55
$MSE = \frac{SSE}{n-k}$	Equation 56

Since the batches need not have equal numbers of specimens, an 'effective batch size,' is defined as

 $n' = \frac{n - \frac{1}{n} \sum_{i=1}^{k} n_i^2}{k - 1}$ 

Using the two mean squares and the effective batch size, an estimate of the population standard deviation is computed:

$$S = \sqrt{\frac{MSB}{n'}} + \left(\frac{n'-1}{n'}\right)MSE$$

Equation 58

Equation 57

Two k-factors are computed using the methodology of section 8.3.5 of CMH-17-1Husing a sample size of n (denoted  $k_0$ ) and a sample size of k (denoted  $k_1$ ). Whether this value is an A- or B-basis value depends only on whether  $k_0$  and  $k_1$  are computed for A or B-basis values.

Denote the ratio of mean squares by

$$u = \frac{MSB}{MSE}$$
 Equation 59

If u is less than one, it is set equal to one. The tolerance limit factor is

 $T = \frac{k_0 - \frac{k_1}{\sqrt{n'}} + (k_1 - k_0)\sqrt{\frac{u}{u + n' - 1}}}{1 - \frac{1}{\sqrt{n'}}}$ 

Equation 60

The basis value is  $\overline{x} - TS$ .

The ANOVA method can produce extremely conservative basis values when a small number of batches are available. Therefore, when less than five (5) batches are available and the ANOVA method is used, the basis values produced will be listed as estimates.

# 2.2 Single Batch and Two Batch Estimates using Modified CV

This method has not been approved for use by the CMH-17 organization. Values computed in this manner are estimates only. It is used only when fewer than three batches are available and no valid B-basis value could be computed using any other method. The estimate is made using the mean of the data and setting the coefficient of variation to 8 percent if it was less than that. A modified standard deviation ( $S_{adj}$ ) was computed by multiplying the mean by 0.08 and computing the A and B-basis values using this inflated value for the standard deviation.

Estimated B-Basis = 
$$\overline{X} - k_b S_{adj} = \overline{X} - k_b \cdot 0.08 \cdot \overline{X}$$
 Equation 61

# 2.3 0º Lamina Strength Derivation

Lamina strength values in the 0° direction were not obtained directly for any conditions during compression tests. They are derived from the cross-ply lamina test results using a back out formula. Unless stated otherwise, the 0° lamina strength values were derived using the following formula:

 $F_{0^{\circ}/90^{\circ}}^{u} = F_{0^{\circ}/90^{\circ}}^{u} \cdot BF \text{ where BF is the backout factor.}$   $F_{0^{\circ}/90^{\circ}}^{u} = \text{UNC0 or UNT0 strength values}$   $BF = \frac{E_{1} \left[ V_{0}E_{2} + (1 - V_{0})E_{1} \right] - (v_{12}E_{2})^{2}}{\left[ V_{0}E_{1} + (1 - V_{0})E_{2} \right] \left[ V_{0}E_{2} + (1 - V_{0})E_{1} \right] - (v_{12}E_{2})^{2}} \text{ Equation 62}$ 

 $V_0$ =fraction of 0° plies in the cross-ply laminate ( $\frac{1}{2}$  for UNT0 and  $\frac{1}{3}$  for UNC0) E<sub>1</sub> = Average across of batches of modulus for LC and LT as appropriate E<sub>2</sub> = Average across of batches of modulus for TC and TT as appropriate v<sub>12</sub> = major Poisson's ratio of 0° plies from an average of all batches

This formula can also be found in section 2.4.2, equation 2.4.2.1(b) of CMH-17-1H.

In computing these strength values, the values for each environment are computed separately. The compression values are computed using only compression data, the tension values are computed using only tension data. Both normalized and as-measured computations are done using the as-measured and normalized strength values from the UNC0 and UNT0 strength values.

### 2.3.1 0º Lamina Strength Derivation (Alternate Formula)

In some cases, the previous formula cannot be used. For example, if there were no ETD tests run for transverse tension and compression, the value for  $E_2$  would not be available. In that case, this alternative formula is used to compute the strength values for longitudinal tension and compression. It is similar to, but not quite the same as the formula detailed above. It requires the UNC0 and UNT0 strength and modulus data in addition to the LC and LT modulus data.

The 0° lamina strength values for the LC ETD condition were derived using the formula:

$$F_{0^{\circ}}^{cu} = F_{0^{\circ}/90^{\circ}}^{cu} \frac{E_{1}^{c}}{E_{0^{\circ}/90^{\circ}}^{c}}, \quad F_{0^{\circ}}^{tu} = F_{0^{\circ}/90^{\circ}}^{tu} \frac{E_{1}^{t}}{E_{0^{\circ}/90^{\circ}}^{t}}$$
 Equation 63

with

 $F_{0^{\circ}}^{cu}$ ,  $F_{0^{\circ}}^{tu}$  the derived mean lamina strength value for compression and tension respectively

 $F_{0^{\circ}/90^{\circ}}^{cu}$ ,  $F_{0^{\circ}/90^{\circ}}^{tu}$  are the mean strength values for UNC0 and UNT0 respectively

 $E_1^c$ ,  $E_1^t$  are the modulus values for LC and LT respectively

 $E_{0^{\circ}/90^{\circ}}^{c}$ ,  $E_{0^{\circ}/90^{\circ}}^{t}$  are the modulus values for UNC0 and UNT0 respectively This formula can also be found in section 2.4.2, equation 2.4.2.1(d) of CMH-17-1H.

# 3. Summary of Results

The basis values for all tests are summarized in the following tables. The NCAMP recommended B-basis values meet all requirements of CMH-17-1H. However, not all test data meets those requirements. The summary tables provide a complete listing of all computed basis values and estimates of basis values. Data that does not meet the requirements of CMH-17-1H are shown in shaded boxes and labeled as estimates. Basis values computed with the modified coefficient of variation (CV) are presented whenever possible. Basis values and estimates computed without that modification are presented for all tests.

## 3.1 NCAMP Recommended B-basis Values

The following rules are used in determining what B-basis value, if any, is included in tables Table 3-1 and Table 3-2 of recommended values.

- 1. Recommended values are NEVER estimates. Only B-basis values that meet all requirements of CMH-17-1H are recommended.
- 2. Modified CV basis values are preferred. Recommended values will be the modified CV basis value when available. The CV provided with the recommended basis value will be the one used in the computation of the basis value.
- 3. Only normalized basis values are given for properties that are normalized.
- 4. ANOVA B-basis values are not recommended since only three batches of material are available and CMH-17-1H recommends that no less than five batches be used when computing basis values with the ANOVA method.
- 5. Basis values of 90% or more of the mean value imply that the CV is unusually low and may not be conservative. Caution is recommended with B-Basis values calculated from CMH-17 STATS when the B-basis value is 90% or more of the average value. Such values will be indicated.
- If the data appear questionable (e.g. when the CTA-RTA-ETW trend of the basis values is not consistent with the CTA-RTA-ETW trend of the average values), then the B-basis values will not be recommended.

### NCAMP Recommended B-basis Values for

Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slip Tape (0.25 inch) All B-basis values in this table meet the standards for publication in CMH-17-1G Handbook

Values are for normalized data unless otherwise noted

#### Lamina Strength Tests

Environment	<u>Ctotiotio</u>	LC	1.7	TO*	<b>TT</b> *	UNCO	I	PS*		VNS*		000*
Environment	Statistic	from UNC0**	LT	TC*	11.	TT* [0/90]		5% Strain	0.2% Offset	5% Strain	Ultimate	SBS*
	B-basis	190.3	458.3	44.17	6.685	72.10	9.720	14.78	10.02	17.31	26.37	19.32
CTA (-65º F)	Mean	300.0	518.2	49.11	8.094	113.7	10.76	16.42	11.77	19.21	29.32	22.01
	CV	8.659	6.000	6.351	8.813	8.659	6.000	6.000	8.287	6.000	6.000	6.199
	B-basis	240.2	451.2	33.09	5.877	90.21	7.077	11.79	8.097	13.45	21.57	14.84
RTA (70° F)	Mean	280.7	527.7	38.01	9.399	105.4	8.119	13.43	9.185	15.35	24.53	16.83
	CV	7.319	7.348	6.000	18.98	7.319	6.000	6.000	6.000	6.000	6.000	6.000
	B-basis	NA: I		NA: I		NA: I						NA: I
ETA1 (180° F)	Mean	259.2		29.13		96.45						12.88
	CV	2.768		2.149		2.768						1.488
	B-basis	NA: I		NA: I		NA: I						NA: I
ETA2 (250° F)	Mean	250.4		22.92		92.70						10.44
	CV	8.427		3.764		8.427						2.556
	B-basis	NA: I	NA: I	NA: I	NA: I	NA: I	NA: I	NA: I	NA: I	NA: I	NA: I	NA: I
ETW1 (180° F)	Mean	256.5	504.5	23.87	6.684	94.93	5.678	8.473	6.490	10.08	16.72	11.39
	CV	4.803	8.447	0.8927	4.279	4.803	1.071	1.304	1.644	1.885	1.597	3.113
	B-basis	160.8	426.6	13.55	NA: A	58.10	NA: A	NA: A	3.617	5.656	NA: A	6.752
ETW2 (250° F)	Mean	200.8	489.2	15.45	3.921	72.55	3.261	5.253	4.113	6.420	11.39	7.865
	CV	10.02	6.568	6.232	6.691	10.02	5.898	5.350	6.108	6.026	4.758	7.164

Notes: The modified CV B-basis value is recommended when available.

The CV provided corresponds with the B-basis value given.

NA implies that tests were run but data did not meet NCAMP recommended requirements.

"NA: A" indicates ANOVA with 3 batches, "NA: I" indicates insufficient data,

Shaded empty boxes indicate that no test data is available for that property and condition.

\* Data is as-measured rather than normalized

\*\* Derived from cross-ply using back-out factor

\*\*\* indicates the Stat17 B-basis value is greater than 90% of the mean value.

#### Table 3-1: NCAMP Recommended B-basis Values for Lamina Test Data

### NCAMP Recommended B-basis Values for

Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slip Tape (0.25 inch) All B-basis values in this table meet the standards for publication in CMH-17-1G Handbook Values are for normalized data unless otherwise noted

Lamma	ate Stren	igui resi	.5								
Lay-up	ENV	Statistic	OHT	ОНС	FHT	FHC	UNT	UNC	SSB Proc. C 2% Offset	SSB Proc. C Ultimate	SBS1*
	СТА	B-basis	73.58		77.30		132.6				
	(-65° F)	Mean	83.15		87.50		149.7				
	(-03 1)	CV	6.000		6.000		6.010				
25	RTA	B-basis	82.25	43.75	83.14	66.28	144.0	100.4	96.24	135.0	11.49
20/2	(70° F)	Mean	91.82	49.63	93.35	74.94	161.2	111.2	109.2	153.1	13.03
25/50/25	(701)	CV	6.000	6.000	6.000	6.000	6.087	6.218	6.000	6.000	6.000
	ETW2	B-basis	102.6	31.46	96.05	44.53	139.7	56.08	NA:A	96.68	NA:A
	(250° F)	Mean	116.4	35.74	106.3	50.52	158.5	66.92	93.67	112.0	4.059
	(230 1)	CV	6.000	6.058	6.000	6.000	6.000	7.574	9.208	6.914	7.913
	СТА	B-basis	52.89		58.65		77.40				
	(-65° F)	Mean	58.92		64.96		85.87				
	(-03 1)	CV	6.000		6.000		6.000				
10/80/10	RTA	B-basis	52.38	39.59	56.28	57.93	75.56	67.77	100.7	133.3	
/80	(70° F)	Mean	58.42	43.60	62.59	63.58	84.03	74.78	114.2	147.6	
10,	(/01)	CV	6.000	6.082	6.000	6.000	6.000	6.000	6.000	6.000	
	ETW2	B-basis	46.85	22.99	43.24	31.09	59.45	38.11	NA:A	95.19	
	(250° F)	Mean	52.89	26.99	49.55	36.75	67.92	45.09	93.16	109.4	
	(200 1)	CV	6.000	6.000	6.000	6.135	6.000	7.006	6.953	6.045	
	СТА	B-basis	119.6		115.7		241.4**				
	(-65° F)	Mean	138.3		134.9		264.5				
	(001)	CV	6.000		6.132		4.581				
/10	RTA	B-basis	134.2	64.57	128.9	88.33	250.5	148.2	99.68	130.3	
50/40/10	(70° F)	Mean	152.8	71.33	148.1	97.69	284.1	168.1	113.1	147.8	
50	(101)	CV	6.000	6.000	6.322	6.000	6.000	6.000	6.000	6.000	
	ETW2	B-basis	205.0	42.33	157.4	53.60	223.4**	NA:A	NA:A	NA:A	
	(250° F)	Mean	223.7	49.09	176.4	62.96	237.2	103.1	87.34	105.9	
	(200 1)	CV	6.000	6.193	7.800	6.823	2.944	8.777	10.15	7.913	

### Laminate Strength Tests

Notes: The modified CV B-basis value is recommended when available.

The CV provided corresponds with the B-basis value given.

NA implies that tests were run but data did not meet NCAMP recommended requirements. "NA: A" indicates ANOVA with 3 batches, "NA: I" indicates insufficient data,

Shaded empty boxes indicate that no test data is available for that property and condition. \* Data is as-measured rather than normalized

\*\* indicates the Stat17 B-basis value is greater than 90% of the mean value.

Table 3-2: NCAMP Recommended B-basis Values for Laminate Test Data

# 3.2 Lamina and Laminate Summary Tables

Material: Toray 396 Material Specification: NMS 397/ Process Specification: NPS 8396	3	1E Gr 192 R	C 33.5% 24K Unidirectional Slip	Tape (0.25 inch)	Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape (0.25 inch) Lamina Properties Summary
Fiber: T1100G-24	4000-71E		<b>Resin:</b> 3960		
<b>Tg(dry):</b> 373.37° F			<b>Tg(wet):</b> 306.95° F	Tg METH	IOD: ASTM D7028
	Lot #1 (A)	Lot #2 (B)	Lot #3 (C)		
Fiber Lot	A1120K2	A1120K2	A1120J1		
Date of fiber manufacture	10/31/2020	10/31/2020	9/30/2020	Date of	of testing 8/23/2022 to 6/1/2023
Resin Lot	Multiple	Multiple	Multiple	Date of	of data submittal 6/26/2023
Date of resin manufacture	Multiple	Multiple	Multiple		
Prepreg Lot	A5210392	A5210797	A3201290		
Date of prepreg manufacture	3/11/2021	7/30/2021	12/8/2020	Date of	of analysis 7/5/2023 to 7/10/2023
Date of composite manufacture	6/3/2	2022 - 11/29/	2022		
_			MECHANICAL PROPERTY B-B		
•			owed by normalized values in	•	
			xes do not meet CMH-17-1G r		
These	alues may	notbeused	for certification unless specif	ically allowed by the	he certifying agency

		CTA (-65° F		r	RTA (70° F)	_		TW1 (180° I			TW2 (250°	F)
Properties	B-Basis	Modified CV B-basis	Mean									
F1 <sup>tu</sup>	475.2	456.7	518.2	463.5	454.3	528.7	401.6	393.5	505.0	441.8	424.8	483.2
[ksi]	(467.0)	(458.3)	(518.2)	(476.0)	(451.2)	(527.7)	(386.1)	NA	(504.5)	(440.2)	(426.6)	(489.2)
E1t			24.58			24.73			25.58			25.31
[Msi]			(24.51)			(24.67)			(25.54)			(25.59)
$V_{12}^{t}$			0.3217			0.3344			0.3365			0.3715
F2 <sup>tu</sup> [ksi]	6.685	NA	8.094	5.877	NA	9.399	5.818	5.073	6.684	2.677	NA	3.921
E <sub>2</sub> <sup>t</sup> [Msi]			1.476			1.330			1.111			0.6996
F1 <sup>cu</sup> [ksi]	190.3	NA	299.3	242.4	238.6	280.8	226.0	195.7	257.8	160.1	NA	200.8
from UNC0*	(190.3)	NA	(300.0)	(244.6)	(240.2)	(280.7)	(219.2)	(194.7)	(256.5)	(160.8)	NA	(200.8)
E1c			21.72			21.71			21.87			21.64
[Msi]			(21.63)			(21.62)			(21.46)			(21.52)
V <sub>12</sub> <sup>c</sup>			0.3383			0.3492			0.3943			0.4157
F2 <sup>cu</sup> [ksi]	44.55	44.17	49.11	36.22	33.09	38.01	23.23	18.12	23.87	14.09	13.55	15.45
E <sub>2</sub> <sup>c</sup> [Msi]			1.495			1.386			1.198			0.9105
UNC0 [0/90] Strength	72.06	NA	113.4	91.02	89.56	105.4	83.50	72.29	95.24	57.81	NA	72.52
[ksi]	(72.10)	NA	(113.7)	(91.89)	(90.21)	(105.4)	(81.12)	(72.05)	(94.93)	(58.10)	NA	(72.55)
UNC0 [0/90] Modulus			8.000			8.028			8.231			8.231
[Msi]			(8.023)			(8.033)			(8.202)			(8.231)
(IPS) F <sub>12</sub> <sup>s0.2%</sup> [ksi]	9.634	9.720	10.76	7.629	7.077	8.119	5.494	4.309	5.678	2.349	NA	3.261
(IPS) F12 <sup>s5% strain</sup> [ksi]	14.30	14.78	16.42	12.31	11.79	13.43	8.138	6.431	8.473	3.311	NA	5.253
(IPS) G <sub>12</sub> <sup>s</sup> [Msi]			0.8492			0.7338			0.5418			0.3310
(VNS) F <sub>12</sub> <sup>s0.2%</sup> [ksi]	10.02	NA	11.77	8.929	8.097	9.185	6.166	4.926	6.490	3.771	3.617	4.113
(VNS) F12 <sup>s5%strain</sup> [ksi]	17.99	17.31	19.21	14.90	13.45	15.35	9.507	7.653	10.08	4.984	5.656	6.420
(VNS) F <sub>12</sub> <sup>su</sup> [ksi]	28.01	26.37	29.32	22.84	21.57	24.53	15.91	12.69	16.72	7.648	NA	11.39
(VNS) G <sub>12</sub> <sup>s</sup> [Msi]			0.8960			0.7615			0.5709			0.4036
SBS [ksi]	17.40	19.32	22.01	14.78	14.84	16.83	10.32	8.645	11.39	6.882	6.752	7.865

\* Derived from cross-ply using back-out factor.

In-Plane Shear (IPS) data was calculated per ASTM D3518.

In-Plane Shear V-Notched (VNS) data was calculated per ASTM D5379.

Table 3-3: Summary of Test Results for Lamina Data

LAMINA M	ECHANICA	L PROPER	TY B-BASI	S SUMMAF	RY Cont.			
	E	TA1 (180° F	-)	ETA2 (250° F)				
Properties	B-Basis	Modified CV B-basis	Mean	B-Basis	Modified CV B-basis	Mean		
F1 <sup>cu</sup> [ksi]	239.7	197.6	260.4	187.0	NA	252.3		
from UNC0*	(237.5)	(196.8)	(259.2)	(186.5)	NA	(250.4)		
E1 <sup>c</sup>			22.15			21.90		
[Msi]			(21.78)			(21.51)		
V <sub>12</sub> <sup>c</sup>			0.3646			0.3730		
F2 <sup>cu</sup> [ksi]	27.23	22.11	29.13	20.31	17.40	22.92		
E <sub>2</sub> <sup>c</sup> [Msi]			1.279			1.201		
UNC0 [0/90] Strength	89.03	73.40	96.70	69.10	NA	93.24		
[ksi]	(88.36)	(73.20)	(96.45)	(69.04)	NA	(92.70)		
UNC0 [0/90] Modulus			7.924			8.024		
[Msi]			(7.903)			(7.979)		
SBS [ksi]	12.30	9.779	12.88	9.632	7.924	10.44		

\* Derived from cross-ply using back-out factor

Table 3-4: Summary of Test Results for Lamina Data

### February 12, 2025

### NCP-RP-2023-002 Rev A

Material Specification: Process Specification: Fiber:	NMS 397/3	1100GC 71E Gi 00-71E I	Resin:			na onp tap	= (U.∠Ə INC	""	RC 3	y 3960/T11 3.5% 24K ape (0.25 i Propertie	Unidirectio	onal Sli nate
Tg(dry):	373.37° F	Тд	(wet):	306.95° F		Тд	METHOD:	ASTM D7	028			
iber Lot ate of fiber manufactu esin Lot ate of resin manufactu				Multiple Multiple	Lot #2 (B) A1120K2 10/31/2020 Multiple Multiple A5210797	Multiple Multiple		Date of te Date of d	•		to 6/1/202 6/26/23	3
repreg Lot ate of prepreg manufa ate of composite man				3/11/2021		12/8/2020		Date of a	nalysis	7/5/2023 t	o 7/10/202	3
		LAMI	NATE	MECHANIC	AL PROPER	TY B-BASIS	SUMMA	RY				
						normalizing						
	These valu	Values show es may not be									ly	
		_ayup:		Isotropic 25			oft" 10/80/			ard" 50/40	/10	
Test	Property	Test Condition	Unit	B-value	Mod. CV	Mean	B-value	Mod. CV	Mean	B-value	Mod. CV	Mear
		CTA (-65° F)	ksi	79.68	B-value 73.58	83.15	56.90	B-value 52.89	58.92	131.3	B-value 119.6	138.3
OHT	Strength	RTA (70° F)	ksi	85.77	82.25	91.82	56.90	52.39	58.42	145.8	134.2	152.8
(normalized)	Strength	ETW1 (180° F)	ksi	81.42	74.89	98.66						
		ETW2 (250° F)	ksi	112.7	102.6	116.4	48.75	46.85	52.89	216.7	205.0	223.
OHC	Strength	RTA (70° F)	ksi	47.32	43.75	49.63	33.77	39.59	43.60	67.19	64.57	71.3
(normalized)	Strength	ETW1 (180° F) ETW2 (250° F)	ksi ksi	37.68 33.51	31.89 31.46	42.02 35.74	 24.88	 22.99	 26.99	 44.95	 42.33	 49.0
	Strength		ksi	138.1	132.6	149.7	75.66	77.40	85.87	241.4	NA	264.
	Modulus	CTA (–65° F)	Msi			9.265			5.909			14.5
	Strength	RTA (70° F)	ksi	149.6	144.0	161.2	82.00	75.56	84.03	264.1	250.5	284.
UNT (normalized)	Modulus	,	Msi			9.122			5.669			14.3
(normalized)	Strength Modulus	ETW1 (180° F)	ksi Msi	159.0	127.2	167.6 9.007						
	Strength		ksi	125.6	139.7	158.5	63.57	59.45	67.92	223.4	NA	237.
	Modulus	ETW2 (250° F)	Msi			8.626			4.464			14.09
	Strength	RTA (70° F)	ksi	102.9	100.4	111.2	70.26	67.77	74.78	155.7	148.2	168.1
UNC	Modulus Strength		Msi ksi	85.14	82.26	8.088 94.69			5.046			12.53
(normalized)	Modulus	ETW1 (180° F)	Msi	03.14	02.20	94.09 7.839						
	Strength	ETW2 (250° F)	ksi	58.59	56.08	66.92	39.96	38.11	45.09	56.45	NA	103.1
	Modulus	E1002 (250° F)	Msi			7.810			4.365			12.64
		CTA (-65° F)	ksi	82.32	77.30	87.50	62.93	58.65	64.96	104.1	115.7	134.9
FHT (normalized)	Strength	RTA (70° F) ETW1 (180° F)	ksi ksi	88.16 95.93	83.14 90.14	93.35 101.9	60.56	56.28	62.59	134.5	128.9	148.
()		ETW2 (250° F)	ksi	101.1	96.05	101.9	47.53	43.24	49.55	159.4	157.4	176.4
FHC		RTA (70° F)	ksi	69.98	66.28	74.94	51.66	57.93	63.58	93.07	88.33	97.6
(normalized)	Strength	ETW1 (180° F)	ksi	62.67	50.33	66.31						
· · · · · · · · · · · · · · · · · · ·	1	ETW2 (250° F)	ksi ksi	46.63 12.50	44.53	50.52	33.69	31.09	36.75	45.13	53.60	62.9
· · · · · · · · · · · · · · · · · · ·			I KGI		11.49	13.03						
SBS1	Strength	RTA (70° F) ETW1 (180° F)	-		6 472	8 527						
. ,	Strength	RTA (70° F) ETW1 (180° F) ETW2 (250° F)	ksi ksi	6.792 2.135	6.472 NA	8.527 4.059						
SBS1 (as-measured)		ETW1 (180° F) ETW2 (250° F) RTA (70° F)	ksi	6.792 2.135 103.1	NA 96.24	4.059 109.2					 99.68	
SBS1	Strength 2%Offset Strength	ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F)	ksi ksi ksi ksi	6.792 2.135 103.1 98.82	NA 96.24 84.69	4.059 109.2 111.6	 108.1 	 100.7 	 114.2 	 106.2 	99.68 	113. <sup>-</sup> 
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized)	2%Offset Strength	ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW2 (250° F)	ksi ksi ksi ksi	6.792 2.135 103.1 98.82 35.90	NA 96.24 84.69 NA	4.059 109.2 111.6 93.67	<b>108.1</b>  53.61	 100.7  NA	 114.2  93.16	106.2  29.85	99.68  NA	113. <sup>-</sup>  87.34
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized) Single Shear Bearing	2%Offset Strength Ultimate	ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F)	ksi ksi ksi ksi	6.792 2.135 103.1 98.82	NA 96.24 84.69	4.059 109.2 111.6	 108.1 	 100.7 	 114.2 	 106.2 	99.68 	113.  87.3
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized)	2%Offset Strength	ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW2 (250° F) RTA (70° F)	ksi ksi ksi ksi ksi	6.792 2.135 103.1 98.82 35.90 143.1	NA 96.24 84.69 NA 135.0	4.059 109.2 111.6 93.67 153.1 130.2 112.0	 108.1  53.61 140.5	 100.7  NA 133.3	 114.2  93.16 147.6  109.4	106.2  29.85	99.68  NA 130.3	113. <sup>-</sup>  87.34 147.8 
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized) Single Shear Bearing	2%Offset Strength Ultimate	ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW1 (180° F) ETW2 (250° F) RTA (70° F)	ksi ksi ksi ksi ksi ksi ksi ksi	6.792 2.135 103.1 98.82 35.90 143.1 121.4 73.44	NA 96.24 84.69 NA 135.0 98.81 96.68	4.059 109.2 111.6 93.67 153.1 130.2 112.0 1.878	 108.1  53.61 140.5  81.27	 100.7  NA 133.3  95.19 	 114.2  93.16 147.6  109.4 1.318	 106.2  29.85 139.9  51.76 	99.68  NA 130.3  NA 	113. <sup>7</sup>  87.34 147.8  105.9
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized)	2% Offset Strength Ultimate Strength	ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F)	ksi ksi ksi ksi ksi ksi ksi Msi	6.792 2.135 103.1 98.82 35.90 143.1 121.4 73.44	NA 96.24 84.69 NA 135.0 98.81 96.68	4.059 109.2 111.6 93.67 153.1 130.2 112.0 1.878 2.060	108.1  53.61 140.5  81.27 	 100.7  NA 133.3  95.19  	 114.2  93.16 147.6  109.4 1.318 	 106.2  29.85 139.9  51.76  	99.68  NA 130.3  NA  	113.  87.3 147.1  105.9 1.76
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized)	2% Offset Strength Ultimate Strength Chord	ETW1 (180° F) ETW2 (250° F) ETW2 (250° F) ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW1 (180° F) RTA (70° F) ETW1 (180° F) ETW1 (180° F)	ksi ksi ksi ksi ksi ksi ksi Msi Msi	6.792 2.135 103.1 98.82 35.90 143.1 121.4 73.44  	NA 96.24 84.69 NA 135.0 98.81 96.68  	4.059 109.2 111.6 93.67 153.1 130.2 112.0 1.878 2.060 1.721	108.1  53.61 140.5  81.27  	 100.7  NA 133.3  95.19   	 114.2  93.16 147.6  109.4 1.318  1.260	 106.2  29.85 139.9  51.76    	99.68  NA 130.3  NA   	113.  87.3 147.3  105.9 1.76  1.68
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized) CBS*	2% Offset Strength Ultimate Strength Chord	ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F)	ksi ksi ksi ksi ksi ksi ksi Msi	6.792 2.135 103.1 98.82 35.90 143.1 121.4 73.44	NA 96.24 84.69 NA 135.0 98.81 96.68	4.059 109.2 111.6 93.67 153.1 130.2 112.0 1.878 2.060	108.1  53.61 140.5  81.27 	 100.7  NA 133.3  95.19  	 114.2  93.16 147.6  109.4 1.318 	 106.2  29.85 139.9  51.76  	99.68  NA 130.3  NA  	113.1
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized)	2% Offset Strength Ultimate Strength Chord Modulus	ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW2 (250° F) RTA (70° F) ETW2 (250° F) ETW1 (180° F) ETW2 (250° F) CTA (-65° F)	ksi ksi ksi ksi ksi ksi ksi Msi Msi Msi Ib	6.792 2.135 103.1 98.82 35.90 143.1 121.4 73.44  	NA 96.24 84.69 NA 135.0 98.81 96.68  	4.059 109.2 111.6 93.67 153.1 130.2 112.0 1.878 2.060 1.721 640.3	 108.1  53.61 140.5  81.27   	 100.7  NA 133.3  95.19   	 114.2  93.16 147.6  109.4 1.318  1.260 	 106.2  29.85 139.9  51.76    	99.68  NA 130.3  NA   	113.  87.34 147.8  105.9 1.768  1.682
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized) CBS* (as-measured)	2% Offset Strength Ultimate Strength Chord Modulus Strength	ETW1 (180° F) ETW2 (250° F) ETW2 (250° F) ETW1 (180° F) ETW2 (250° F) ETW2 (250° F) ETW2 (250° F) ETW2 (250° F) ETW1 (180° F) ETW2 (250° F) CTA (-65° F) ETW2 (250° F) CTA (-65° F)	ksi ksi ksi ksi ksi ksi ksi Msi Msi Msi Ib Ib	6.792 2.135 103.1 98.82 35.90 143.1 121.4 73.44   	NA 96.24 84.69 NA 135.0 98.81 96.68  	4.059 109.2 111.6 93.67 153.1 130.2 112.0 1.878 2.060 1.721 640.3 482.2	 108.1  53.61 140.5  81.27   	 100.7  NA 133.3  95.19     	 93.16 147.6  109.4 1.318  1.260  	 106.2  29.85 139.9  51.76    	99.68  NA 130.3  NA    	113.1  87.34 147.8  1.05.9 1.768  1.682
SBS1 (as-measured) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized) Single Shear Bearing Proc. C (normalized) CBS*	2% Offset Strength Ultimate Strength Chord Modulus	ETW1 (180° F) ETW2 (250° F) RTA (70° F) ETW1 (180° F) ETW2 (250° F) ETW2 (250° F) ETW2 (250° F) RTA (70° F) ETW2 (250° F) CTA (-65° F) RTA (70° F) ETW2 (250° F)	ksi ksi ksi ksi ksi ksi ksi Msi Msi Ib Ib Ib	6.792 2.135 103.1 98.82 35.90 143.1 121.4 73.44   	NA 96.24 84.69 NA 135.0 98.81 96.68    	4.059 109.2 111.6 93.67 153.1 130.2 112.0 1.878 2.060 1.721 640.3 482.2 111.4	 108.1  53.61 140.5  81.27     	 100.7  NA 133.3  95.19      	 114.2  93.16 147.6  109.4 1.318  1.260   	 106.2  29.85 139.9  51.76      	99.68  NA 130.3  NA    	113.1  87.34 147.8  105.5 1.768  1.682  

\* The actual layup for ILT is [0]22, (100/0/0).

Table 3-5: Summary of Test Results for Laminate Data

#### 4. Test Results, Statistics, Basis Values, and Graphs

Test data for fiber dominated properties was normalized according to nominal cured ply thickness. Both normalized and as-measured statistics were included in the tables, but only the normalized data values were graphed. Test failures, outliers and explanations regarding computational choices were noted in the accompanying text for each test.

All individual specimen results are graphed for each test by batch and environmental condition with a line indicating the recommended basis values for each environmental condition. The data is jittered (moved slightly to the left or right) in order for all specimen values to be clearly visible. The strength values are always graphed on the vertical axis with the scale adjusted to include all data values and their corresponding basis values. The vertical axis may not include zero. The horizontal axis values will vary depending on the data and how much overlapping there was of the data within and between batches. When there was little variation, the batches were graphed from left to right. The environmental conditions were identified by the shape and color of the symbol used to plot the data. Otherwise, the environmental conditions were graphed from left to right and the batches were identified by the shape and color of the symbol.

When a dataset fails the Anderson-Darling k-sample (ADK) test for batch-to-batch variation, an ANOVA analysis is required. In order for B-basis values to be computed using the ANOVA method, data from five batches are required. Since this qualification dataset has only three batches, the basis values computed using ANOVA are considered estimates only. However, the basis values resulting from the ANOVA method using only three batches may be overly conservative. The ADK test is performed again after a transformation of the data according to the assumptions of the modified CV method (see section 2.1.4 for details). If the dataset still passes the ADK test at this point, modified CV basis values are provided. If the dataset does not pass the ADK test after the transformation, estimates may be computed using the modified CV method per the guidelines in CMH-17 Vol 1 Chapter 8 section 8.3.10.

#### 4.1 Longitudinal Tension (LT)

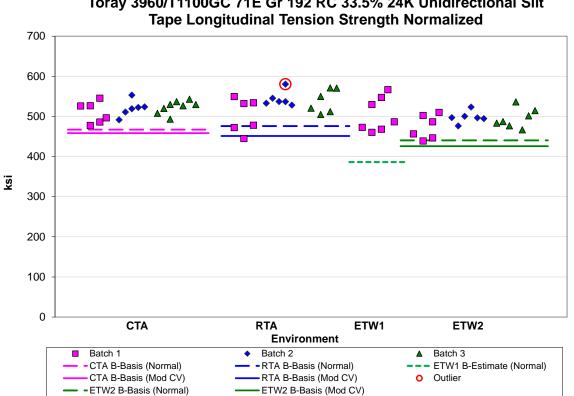
The LT data is normalized, so both normalized and as-measured values are provided. Data is available for two properties, strength and modulus, LT tests were performed at four different environmental conditions. The ETW1 condition lacked sufficient specimens to meet CMH-17 guidelines, so only estimates of basis values are provided for that condition.

Pooling was appropriate for the normalized CTA and RTA conditions. The pooled asmeasured CTA and RTA datasets failed the normality test.

The ETW1 normalized dataset had a CV higher than 8%, so modified CV basis values could not be provided for that dataset.

There was one outlier. The largest value in the batch two of the RTA condition was an outlier for batch two but not for the RTA condition. It was an outlier for both the normalized and as-measured datasets. It was retained for this analysis.

Statistics, basis values and estimates are given for strength data in Table 4-1 and for the modulus data in Table 4-2. The normalized data, B-basis values and B-estimates are shown graphically in Figure 4-1.



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit

Figure 4-1 Batch plot for LT strength normalized

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	Longitudinal Tension Strength Basis Values and Statistics									
		Norm	alized			As-me	asured			
Env	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)		
Mean	518.2	527.7	504.5	489.2	518.2	528.7	505.0	483.2		
Stdev	20.64	35.34	42.61	25.12	22.34	33.01	37.22	21.28		
CV	3.982	6.696	8.447	5.135	4.312	6.243	7.371	4.403		
Mod CV	6.000	7.348	8.447	6.568	6.156	7.122	8.000	6.201		
Min	477.4	444.8	460.4	438.7	476.5	449.6	467.3	446.5		
Max	553.0	580.4	566.5	536.4	562.6	576.7	559.6	537.0		
No. Batches	3	3	2	3	3	3	2	3		
No. Spec.	20	18	7	19	20	18	7	19		
			Basis V	alue and Es	timates					
B-basis Value	467.0	476.0		440.2	475.2	463.5		441.8		
B-Estimate			386.1				401.6			
A-Estimate	431.8	440.9	302.9	405.5	444.5	417.3	328.9	412.3		
Method	pooled	pooled	Normal	Normal	Normal	Normal	Normal	Normal		
		M	odified CV B	asis Values	and Estimat	es				
B-basis Value	458.3	451.2		426.6	456.7	454.3		424.8		
B-Estimate			NA				393.5			
A-Estimate	415.8	397.0		382.2	413.1	401.8	317.2	383.4		
Method	Normal	Normal		Normal	Normal	Normal	Normal	Normal		

Table 4-1: Statistics and Basis values for LT Strength data

	Longitudinal Tension Modulus Statistics										
		Norm	alized			As-me	asured				
Env	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)			
Mean	24.51	24.67	25.54	25.59	24.58	24.73	25.58	25.31			
Stdev	0.3255	0.2639	0.5438	0.5087	0.5556	0.4450	0.3515	0.4436			
CV	1.328	1.069	2.129	1.988	2.260	1.800	1.374	1.753			
Mod CV	6.000	6.000	8.000	6.000	6.000	6.000	8.000	6.000			
Min	23.68	24.21	24.86	24.97	23.46	23.83	25.08	24.69			
Max	25.07	25.17	26.23	27.28	25.28	25.29	26.07	26.17			
No. Batches	3	3	2	3	3	3	2	3			
No. Spec.	18	18	7	18	18	18	7	18			

Table 4-2: Statistics for LT Modulus data

# 4.2 Transverse Tension (TT)

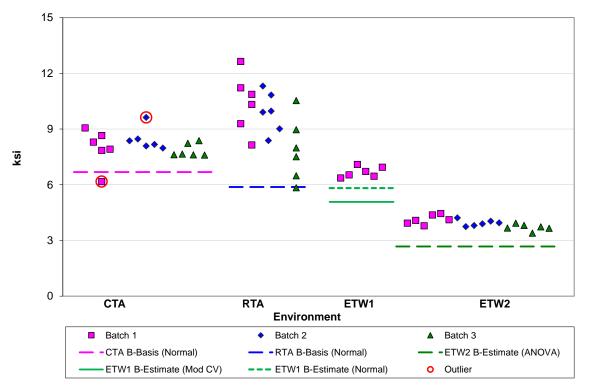
The TT data is not normalized for unidirectional tape, only as-measured values are provided. Data is available for two properties, strength and modulus. TT tests were performed at four different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for that condition.

The ETW2 dataset failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. It did not pass the ADK test after the modified CV transformation, so modified CV basis values are not provided for that dataset.

The CTA and RTA datasets had a CV higher than 8%, so modified CV basis values could not be provided.

There were two outliers, both in the CTA condition. The lowest value in batch one was an outlier for the CTA condition but not for the batch one. The largest value in batch two was an outlier for batch two but not for the CTA condition. Both outliers were retained for this analysis.

Statistics, basis values and estimates are given for strength data as-measured in Table 4-3 and for the modulus data as-measured in Table 4-4. The as-measured data, B-basis values and B-estimates are shown graphically in Figure 4-2.





Transverse	e Tension St	rength Basis	s Values and	Statistics					
As-measured									
Env	CTA (− 65°F)	RTA (70°F)	ETW1 (180°F) ETW2 (250°						
Mean	8.094	9.399	6.684	3.921					
Stdev	0.7133	1.784	0.2860	0.2624					
CV	8.813	18.98	4.279	6.691					
Mod CV	8.813	18.98	8.000	7.346					
Min	6.168	5.838	6.365	3.396					
Мах	9.622	12.64	7.090	4.451					
No.Batches	3	3	1	3					
No.Spec.	18	18	6	18					
	Basis Va	alues and Es	timates						
B-basis Value	6.685	5.877							
B-estimate			5.818	2.677					
A-estimate	5.687	3.381	5.202	1.790					
Method	Normal	Normal	Normal	ANOVA					
Мо	odified CV B	asis Values	and Estimate	es					
B-basis Value									
B-estimate	NA	NA	5.073	NA					
A-estimate		142	3.971	142					
Method			Normal						

Figure 4-2:	Batch	Plot for	TT Strend	gth as-measur	ed
i iguio 4 L.	Baton	1 101 101		gin us measur	50

Table 4-3: Statistics and Basis Values for TT Strength data as-measured

Т	Transverse Tension Modulus Statistics								
	As-measured								
Env	CTA (− 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)					
Mean	1.476	1.330	1.111	0.6996					
Stdev	0.07723	0.01902	0.03621	0.04292					
CV	5.232	1.431	3.261	6.136					
Mod CV	6.616	6.000	8.000	7.068					
Min	1.284	1.292	1.076	0.6489					
Max	1.623	1.357	1.146	0.7847					
No. Batches	3	3	1	3					
No.Spec.	18	18	6	18					

 Table 4-4: Statistics from TT Modulus data as-measured

# 4.3 Longitudinal Compression (LC)

The LC data is normalized, so both normalized and as-measured values are provided. Data is available for two properties, strength and modulus. LC tests were performed at six different environmental conditions. The ETA1, ETA2 and ETW1 conditions only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for those conditions. Strength values are not available directly from the LC test specimens. The strength values for 0° properties are computed via the formulas specified in section 2.3 from the UNC0 specimen values.

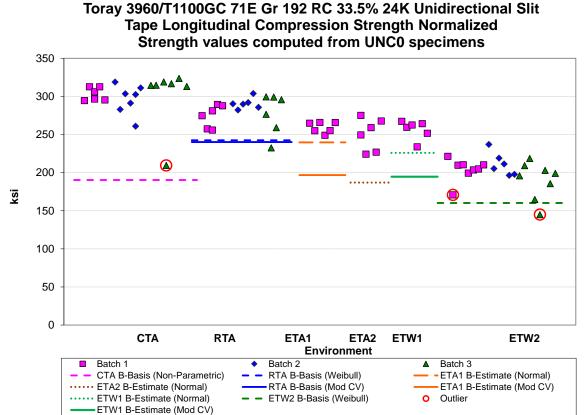
The RTA and ETW2 datasets, both normalized and as-measured, did not have an adequate fit to the normal distribution. The Weibull distribution was used to compute the basis values. After the transformation of data to fit the assumptions of the modified CV method, those datasets all passed the normality test so modified CV basis values are provided.

The CTA dataset both normalized and as-measured, failed all three distribution tests, requiring the non-parametric approach to compute design values.

The CTA, ETA2, and ETW2 datasets, both normalized and as-measured, had a CV higher than 8%, so modified CV basis values could not be provided for those datasets.

There were three outliers. The lowest value in batch three of the CTA condition was an outlier for both batch three and CTA condition. The lowest value in batch one of the ETW2 condition was an outlier for the batch one but not for the ETW2 condition. The lowest value in batch three of the ETW2 condition was an outlier for the ETW2 condition but not for the batch three. All three outliers were outliers for both the normalized and asmeasured datasets. All three outliers were retained for this analysis.

Statistics, basis values and estimates are given for normalized strength data in Table 4-5, the as-measured strength data in Table 4-6, for the normalized modulus data in Table 4-7, and for the as-measured modulus data in Table 4-8. The normalized data, B-basis values and B-estimates are shown graphically in Figure 4-3.



#### Figure 4-3 Batch plot for LC Strength normalized derived from UNC0

Longitu	Longitudinal Compression Strength Basis Values and Statistics normalized								
Env	CTA (- 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)			
Mean	300.0	280.7	259.2	250.4	256.5	200.8			
Stdev	25.98	18.63	7.18	21.10	12.32	20.12			
CV	8.659	6.637	2.768	8.427	4.803	10.02			
Mod CV	8.659	7.319	8.000	8.427	8.000	10.02			
Min	209.4	232.6	249.0	224.3	233.8	144.9			
Мах	323.6	303.8	265.9	275.2	267.3	237.1			
No. Batches	3	3	1	1	1	3			
No. Spec.	20	18	6	6	6	22			
		Basis V	alue and Es	timates					
B-basis Value	190.3	244.6				160.8			
B-Estimate			237.5	186.5	219.2				
A-Estimate	115.5	208.7	222.1	141.1	192.7	124.7			
Method	Non-Parm.	Weibull	Normal	Normal	Normal	Weibull			
		Modified C	/ Basis Valu	e Estimates					
B-basis Value		240.2							
B-Estimate	NA		196.8	NA	194.7	NA			
A-Estimate	142	211.5	154.0	114	152.4	114			
Method		Normal	Normal		Normal				

Table 4-5: Statistics and Basis Values for LC Strength derived from UNC0 normalized

Longitud	Longitudinal Compression Strength Basis Values and Statistics as-measured								
Env	CTA (− 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)			
Mean	299.3	280.8	260.4	252.3	257.8	200.8			
Stdev	25.67	20.29	6.820	21.57	10.50	20.65			
CV	8.575	7.227	2.619	8.547	4.071	10.28			
Mod CV	8.575	7.613	8.000	8.547	8.000	10.28			
Min	209.5	230.8	252.9	223.0	239.2	143.2			
Max	320.2	302.8	270.8	274.7	270.1	238.5			
No. Batches	3	3	1	1	1	3			
No. Spec.	20	18	6	6	6	22			
		Basis V	alue and Es	timates					
B-basis Value	190.3	242.4				160.1			
B-Estimate			239.7	187.0	226.0				
A-Estimate	117.3	204.6	225.0	140.6	203.4	123.5			
Method	Non-Parm.	Weibull	Normal	Normal	Normal	Weibull			
		Modified C	/ Basis Valu	e Estimates					
B-basis Value		238.6							
B-Estimate	NA		197.6	NA	195.7	NA			
A-Estimate		208.7	154.7		153.2	112			
Method		Normal	Normal		Normal				

Table 4-6: Statistics and Basis Values for LC Strength derived from UNC0 as-measured

	Longitudinal Compression Modulus Statistics normalized								
Env	CTA (− 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)			
Mean	21.63	21.62	21.78	21.51	21.46	21.52			
Stdev	0.5696	0.6001	0.3998	0.6097	0.7350	0.4989			
CV	2.634	2.776	1.835	2.834	3.424	2.318			
Mod CV	6.000	6.000	8.000	8.000	8.000	6.000			
Min	20.30	20.41	20.86	20.42	20.58	20.73			
Max	23.10	22.83	22.28	22.30	22.32	22.72			
No. Batches	3	3	2	2	1	3			
No.Spec.	36	36	12	12	6	18			

Table 4-7: Statistics from LC Modulus normalized data

	Longitudinal Compression Modulus Statistics as measured								
Env	CTA (− 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)			
Mean	21.72	21.71	22.15	21.90	21.87	21.64			
Stdev	0.4564	0.5426	0.4403	0.6296	0.6770	0.5986			
CV	2.101	2.499	1.987	2.874	3.096	2.766			
Mod CV	6.000	6.000	8.000	8.000	8.000	6.000			
Min	20.74	20.87	21.31	20.86	21.03	20.65			
Max	22.72	23.28	22.86	22.75	22.63	23.04			
No. Batches	3	3	2	2	1	3			
No. Spec.	36	36	12	12	6	18			

Table 4-8: Statistics from LC Modulus as-measured data

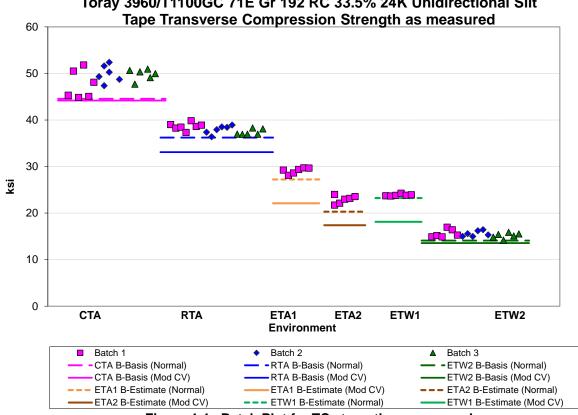
# 4.4 Transverse Compression (TC)

The TC data is not normalized for unidirectional tape, only as-measured values are provided. Data is available for two properties, strength and modulus. TC tests were performed at six different environmental conditions. The ETA1, ETA2, and ETW1 conditions only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for those conditions.

Pooling was appropriate for the CTA and RTA conditions for the modified CV basis values only. Prior to the modified CV transformation of data, they failed Levene's test and could not be pooled.

There were no statistical outliers.

Statistics, basis values and estimates are given for strength data in Table 4-9 and for the modulus data in Table 4-10. The as-measured data, B-estimates, and B-basis values are shown graphically in Figure 4-4.



# Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit

Figure 4-4: Batch Plot for TC strength as-measured

	Transverse	Compression	Strength Bas	is Values and	Statistics			
	As-measured							
Env	CTA (− 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)		
Mean	49.11	38.01	29.13	22.92	23.87	15.45		
Stdev	2.309	0.9188	0.6261	0.8626	0.2131	0.6898		
CV	4.702	2.417	2.149	3.764	0.8927	4.464		
Mod CV	6.351	6.000	8.000	8.000	8.000	6.232		
Min	44.84	36.40	28.13	21.71	23.67	14.21		
Мах	52.39	39.85	29.72	24.00	24.27	16.95		
No.Batches	3	3	1	1	1	3		
No. Spec.	18	19	6	6	6	18		
		Basis Va	lues and Esti	mates				
B-basis Value	44.55	36.22				14.09		
B-estimate			27.23	20.31	23.23			
A-estimate	41.32	34.95	25.89	18.45	22.77	13.13		
Method	Normal	Normal	Normal	Normal	Normal	Normal		
		Modified CV Ba	asis Values ar	nd Estimates				
B-basis Value	44.17	33.09				13.55		
B-estimate			22.11	17.40	18.12			
A-estimate	40.81	29.73	17.31	13.62	14.18	12.21		
Method	pooled	pooled	Normal	Normal	Normal	Normal		

Table 4-9: Statistics and Basis Values for TC Strength data

	Transverse Compression Modulus Statistics as-measured								
Env	CTA (− 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)			
Mean	1.495	1.386	1.279	1.201	1.198	0.9105			
Stdev	0.02958	0.02736	0.03340	0.03444	0.01689	0.04346			
CV	1.979	1.975	2.612	2.867	1.410	4.773			
Mod CV	6.000	6.000	8.000	8.000	8.000	6.386			
Min	1.447	1.314	1.227	1.160	1.176	0.8394			
Max	1.552	1.429	1.316	1.237	1.218	0.9823			
No. Batches	3	3	1	1	1	3			
No. Spec.	18	19	6	6	6	18			

Table 4-10: Statistics from TC Modulus data

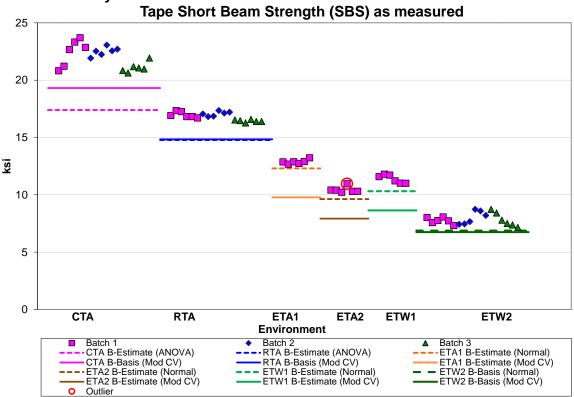
# 4.5 Short-Beam Strength (SBS)

The SBS data is not normalized, only as-measured values are provided. Data is available for only one property, strength. SBS tests were performed at six different environmental conditions. The ETA1, ETA2, and ETW1 conditions only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for those conditions.

The CTA and RTA datasets failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. Both datasets passed the ADK test after the modified CV transformation, so modified CV basis values are provided but pooling was not appropriate due to a failure of Levene's test.

There was one statistical outlier. The largest value in the ETA2 dataset was an outlier. With only one batch tested in this condition, it can only be assessed as an outlier for batch, not the condition. It was retained for this analysis.

Statistics and basis values are given for SBS data in Table 4-11. The as-measured data, B-basis values and B-estimates are shown graphically in Figure 4-5.



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Short Beam Strength (SBS) as measured

Figure 4-5: Batch plot for SBS as-measured

Shor	Short Beam Strength (SBS) Basis Values and Statistics As-measured								
Env	CTA (- 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)			
Mean	22.01	16.83	12.88	10.44	11.39	7.865			
Stdev	0.9683	0.3421	0.1917	0.2668	0.3546	0.4977			
CV	4.398	2.033	1.488	2.556	3.113	6.329			
Mod CV	6.199	6.000	8.000	8.000	8.000	7.164			
Min	20.63	16.28	12.68	10.22	11.01	7.156			
Max	23.70	17.35	13.23	10.96	11.80	8.738			
No. Batches	3	3	1	1	1	3			
No. Spec.	18	18	6	6	6	18			
		Basis Va	alues and Es	timates					
B-basis Value						6.882			
B-estimate	17.40	14.78	12.30	9.632	10.32				
A-estimate	14.10	13.32	11.89	9.057	9.552	6.186			
Method	ANOVA	ANOVA	Normal	Normal	Normal	Normal			
	Мс	dified CV B	asis Values	and Estimate	es				
B-basis Value	19.32	14.84				6.752			
B-estimate			9.779	7.924	8.645				
A-estimate	17.41	13.43	7.654	6.203	6.767	5.965			
Method	Normal	Normal	Normal	Normal	Normal	Normal			

Table 4-11: Statistics and Basis Values for SBS data

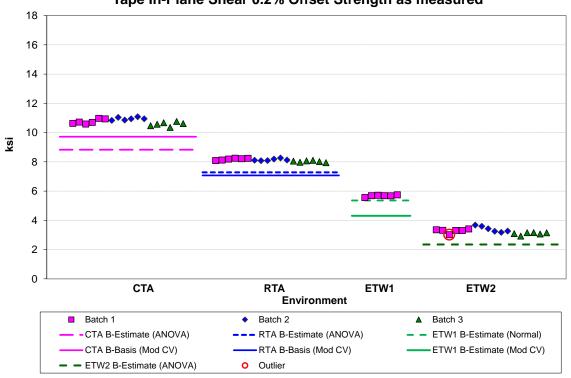
# 4.6 In-Plane Shear (IPS)

The IPS data is not normalized, only as-measured values are provided. Data is provided on three properties, 0.2% offset strength, strength at 5% strain and modulus. IPS tests were performed at four different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for those conditions.

The CTA, RTA and ETW2 datasets for both 0.2% offset strength and strength at 5% strain failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. The CTA and RTA datasets for both 0.2% offset strength and strength at 5% strain passed the ADK test after the modified CV transformation, so modified CV basis values are provided for those dataset. Pooling was appropriate for the CTA and RTA datasets for both 0.2% offset strength at 5% strain. The ETW2 datasets did not pass the ADK test after the modified CV transformation, so modified CV basis values are not provided for that condition.

There were two statistical outliers. The lowest value in batch one of the ETW2 dataset for 0.2% offset strength was an outlier for batch one but not for the ETW2 condition. The lowest value in batch three of the ETW2 dataset for strength at 5% strain was an outlier for batch three but not for the ETW2 condition. Both outliers were retained for this analysis.

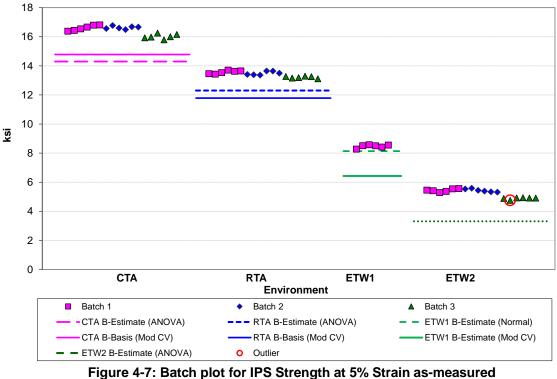
Statistics, estimates and basis values are given for the 0.2% offset strength data in Table 4-12, the strength at 5% strain data in Table 4-13 and modulus data in Table 4-14. The as-measured data, B-estimates and B-basis values are shown graphically for the 0.2% offset strength in Figure 4-6 and for strength at 5% strain in Figure 4-7.



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape In-Plane Shear 0.2% Offset Strength as measured

Figure 4-6: Batch plot for IPS for 0.2% Offset Strength as-measured

Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape In-Plane Shear Strength at 5% Strain as measured



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In-Plane Shear Strength Basis Values and Statistics As-				
measured 0.2% Offset Strength				
Env	CTA (− 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)
Mean	10.76	8.119	5.678	3.261
Stdev	0.2046	0.09326	0.06080	0.1923
CV	1.901	1.149	1.071	5.898
Mod CV	6.000	6.000	8.000	6.949
Min	10.35	7.943	5.564	2.924
Max	11.09	8.267	5.741	3.678
No.Batches	3	3	1	3
No.Spec.	18	18	6	18
	Basis V	alues and Es	timates	
B-estimate	9.634	7.629	5.494	2.349
A-estimate	8.829	7.279	5.363	1.700
Method	ANOVA	ANOVA	Normal	ANOVA
Modified Basis Values and Estimates				
B-basis Value	9.720	7.077		
B-estimate			4.309	NA
A-estimate	9.011	6.368	3.373	NA
Method	pooled	pooled	Normal	

Table 4-12: Statistics and Basis Values for IPS 0.2% Offset Strength data

In-Plane Shear Strength Basis Values and Statistics As-				
measured Strength at 5% Strain				
Env	CTA (− 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)
Mean	16.42	13.43	8.473	5.253
Stdev	0.3266	0.1843	0.1105	0.2810
CV	1.989	1.373	1.304	5.350
Mod CV	6.000	6.000	8.000	6.675
Min	15.79	13.11	8.276	4.755
Мах	16.81	13.70	8.574	5.584
No. Batches	3	3	1	3
No. Spec.	18	18	18 6 18	
	Basis V	alues and Es	timates	
B-estimate	14.30	12.31	8.138	3.311
A-estimate	12.79	11.51	7.900	1.925
Method	ANOVA	ANOVA	Normal	ANOVA
Modified Basis Values and Estimates				
B-basis Value	14.78	11.79		
B-estimate			6.431	NA
A-estimate	13.66	10.67	5.034	NA .
Method	pooled	pooled	Normal	

Table 4-13: Statistics and Basis Values for IPS Strength at 5% Strain data

In Plane Shear Modulus Statistics As-measured					
Env	CTA (− 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	
Mean	0.8492	0.7338	0.5418	0.3310	
Stdev	0.02115	0.01170	0.006182	0.02387	
CV	2.490	1.594	1.141	7.212	
Mod CV	6.000	6.000	8.000	7.606	
Min	0.8094	0.7146	0.5324	0.2936	
Max	0.8793	0.7537	0.5514	0.3784	
No. Batches	3	3	1	3	
No. Spec.	18	18	6	18	

Table 4-14: Statistics from IPS Modulus data

# 4.7 In-Plane Shear V-Notched (VNS)

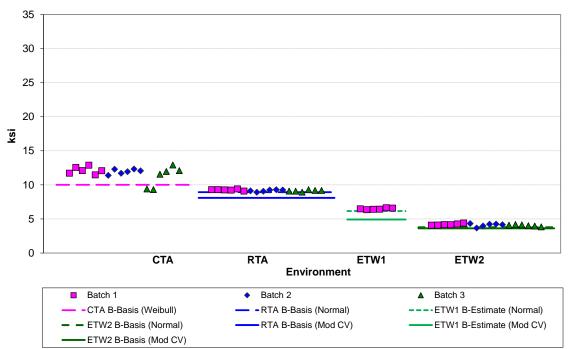
The VNS data is not normalized, only as-measured values are provided. Data is provided on four properties, 0.2% offset strength, strength at 5% strain, ultimate strength and modulus. VNS tests were performed at four different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for those conditions.

The CTA dataset for strength at 5% strain, the RTA dataset for ultimate strength and the ETW2 datasets for strength at 5% strain and ultimate strength failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. The CTA and ETW2 datasets for strength at 5% strain, the RTA dataset for ultimate strength passed the ADK test after the modified CV transformation, so modified CV basis values are provided for those dataset. Pooling was appropriate for the CTA and RTA datasets for strength at 5% strain and ultimate strength. The ETW2 dataset for ultimate strength did not pass the ADK test after the modified CV transformation, so modified CV basis values are not provided for that condition.

The CTA dataset for 0.2% offset strength did not pass the normality test, but the Weibull distribution had an adequate fit, so design values were computed using the Weibull distribution. The CTA dataset for 0.2% offset strength had a CV greater than 8%, so no modified CV basis values could be provided for that condition.

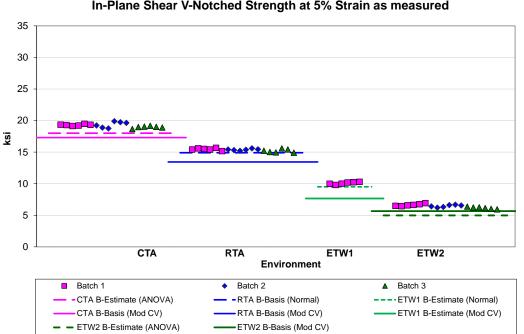
There were no statistical outliers.

Statistics, basis values and estimates are given for 0.2% offset strength in Table 4-15, the strength at 5% strain in Table 4-16, ultimate strength data in Table 4-17, and for the modulus data in Table 4-18. The as-measured data, the B-basis values and B-estimates are shown graphically for 0.2% offset strength in Figure 4-8, strength at 5% strain in Figure 4-9, and for ultimate strength in Figure 4-10.



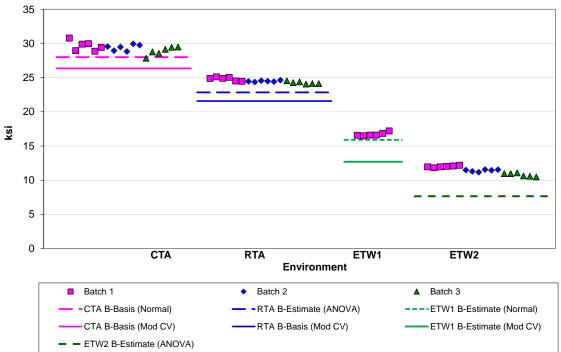
Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape In-Plane Shear V-Notched 0.2% Offset Strength as measured

Figure 4-8: Batch Plot for VNS 0.2% Offset Strength as-measured



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape In-Plane Shear V-Notched Strength at 5% Strain as measured

Figure 4-9: Batch Plot for VNS Strength at 5% Strain as-measured



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape In-Plane Shear V-Notched Ultimate Strength as measured

In Plane Shear V-Notched Basis Values and Statistics As-					
measured 0.2% Offset Strength					
Env	CTA (− 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	
Mean	11.77	9.185	6.490	4.113	
Stdev	0.9755	0.1300	0.1067	0.1734	
CV	8.287	1.415	1.644	4.216	
Mod CV	8.287	6.000	8.000	6.108	
Min	9.316	8.929	6.358	3.678	
Max	12.93	9.408	6.641	4.402	
No. Batches	3	3	1	3	
No. Spec.	18	18	6	18	
	Basis Va	lues and Es	timates	_	
B-basis Value	10.02	8.929		3.771	
B-estimate			6.166		
A-estimate	8.316	8.747	5.937	3.528	
Method	Weibull	Normal	Normal	Normal	
Modified CV Basis Values and Estimates					
B-basis Value		8.097		3.617	
B-estimate	NA		4.926		
A-estimate	INA	7.328	3.856	3.267	
Method		Normal	Normal	Normal	

Table 4-15: Statistics and Basis Values for VNS 0.2% Offset Strength data

In Plane Shear V-Notched Basis Values and Statistics As- measured Strength at 5% Strain					
Env CTA (~ 65°F) RTA (70°F) ETW1 (180°F) ETW2 (250°					
Mean	19.21	15.35	10.08	6.420	
Stdev	0.3338	0.2266	0.1901	0.2602	
CV	1.738	1.477	1.885	4.052	
Mod CV	6.000	6.000	8.000	6.026	
Min	18.66	14.90	9.795	5.942	
Max	19.90	15.68	10.30	6.924	
No. Batches	3	3	1	3	
No.Spec.	18	18	6	18	
	Basis Va	lues and Es	timates		
B-basis Value		14.90			
B-estimate	17.99		9.507	4.984	
A-estimate	17.13	14.58	9.098	3.960	
Method	ANOVA	Normal	Normal	ANOVA	
Modified CV Basis Values and Estimates					
B-basis Value	17.31	13.45		5.656	
B-estimate			7.653		
A-estimate	16.01	12.15	5.990	5.116	
Method	pooled	pooled	Normal	Normal	

Table 4-16: Statistics and Basis Values for VNS Strength at 5% Strain data

In Plane Shear V-Notched Basis Values and Statistics As-				
	measure	d Ultimate	Strength	
Env	CTA (− 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)
Mean	29.32	24.53	16.72	11.39
Stdev	0.6630	0.2990	0.2670	0.5422
CV	2.261	1.219	1.597	4.758
Modified CV	6.000	6.000	8.000	6.379
Min	27.85	24.08	16.48	10.47
Max	30.80	25.12	17.20	12.19
No. Batches	3	3	1	3
No.Spec.	18	18	6	18
	Basis Va	lues and Es	stimates	-
B-basis Value	28.01			
B-estimate		22.84	15.91	7.648
A-estimate	27.09	21.64	15.33	4.974
Method	Normal	ANOVA	Normal	ANOVA
Modified CV Basis Values and Estimates				
B-basis Value	26.37	21.57		
B-estimate			12.69	NA
A-estimate	24.36	19.56	9.931	INA
Method	pooled	pooled	Normal	

Table 4-17: Statistics and Basis Values for VNS Ultimate Strength data

#### February 12, 2025

In Plane Shear V-Notched Modulus Statistics As-measured					
Env	CTA (− 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	
Mean	0.8960	0.7615	0.5709	0.4036	
Stdev	0.09885	0.01533	0.01188	0.01701	
CV	11.03	2.013	2.081	4.214	
Mod CV	11.03	6.000	8.000	6.107	
Min	0.8096	0.7386	0.5559	0.3761	
Max	1.230	0.7938	0.5860	0.4372	
No. Batches	3	3	1	3	
No. Spec.	18	18	6	18	

Table 4-18:	Statistics	from VNS	Modulus data	
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#### 4.8 "25/50/25" Unnotched Tension 1 (UNT1)

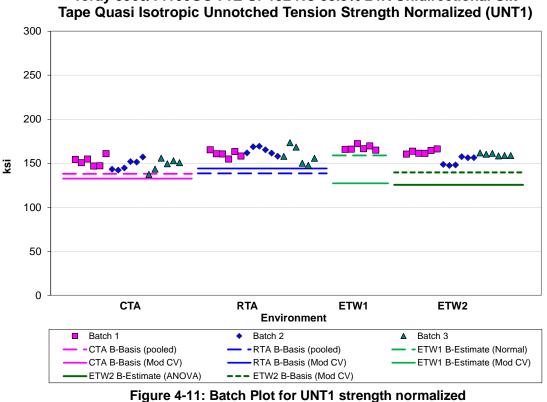
The UNT1 data is normalized, so both normalized and as-measured values are provided. Data is available for two properties, strength and modulus. UNT1 tests were performed at four different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for that condition.

The ETW2 datasets, both normalized and as-measured, failed the Anderson Darling ksample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. Both of the ETW2 datasets passed the ADK test after the modified CV transformation, so modified CV basis values are provided for those datasets.

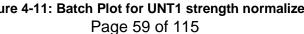
Pooling was appropriate for the CTA and RTA conditions for both the normalized and as-measured datasets.

There were no statistical outliers.

Statistics, basis values and estimates are given for UNT1 strength data in Table 4-19 and for the modulus data in Table 4-20. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-11.



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit



Unnotched Tension (UNT1) Strength Basis Values and Statistics								
		Norm	alized		As-measured			
Env	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)
Mean	149.7	161.2	167.6	158.5	149.5	160.9	168.0	158.4
Stdev	6.018	6.729	2.841	5.447	6.095	6.751	2.830	5.102
CV	4.019	4.175	1.695	3.438	4.076	4.196	1.684	3.221
Modified CV	6.010	6.087	8.000	6.000	6.038	6.098	8.000	6.000
Min	137.4	147.8	165.0	147.5	136.1	147.4	165.6	148.5
Max	161.0	173.4	172.3	166.3	161.4	171.6	172.5	166.3
No. Batches	3	3	1	3	3	3	1	3
No. Spec.	18	18	6	18	18	18	6	18
			Basis Va	alues and Es	timates			
B-basis Value	138.1	149.6			137.8	149.2		
B-estimate			159.0	125.6			159.4	127.1
A-estimate	130.2	141.6	152.9	102.1	129.8	141.2	153.3	104.7
Method	pooled	pooled	Normal	ANOVA	pooled	pooled	Normal	ANOVA
Modified CV Basis Values and Estimates								
B-basis Value	132.6	144.0		139.7	132.4	143.7		139.6
B-estimate			127.2				127.5	
A-estimate	120.9	132.4	99.56	126.4	120.7	132.0	99.82	126.4
Method	pooled	pooled	Normal	Normal	pooled	pooled	Normal	Normal

Table 4-19: Statistics and Basis Values for UNT1 Strength data

	Unnotched Tension (UNT1) Modulus Statistics							
		Norm	alized			As-me	asured	
Env	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)
Mean	9.265	9.122	9.007	8.626	9.253	9.106	9.031	8.625
Stdev	0.1136	0.1228	0.04639	0.1553	0.1226	0.1463	0.04643	0.1776
CV	1.226	1.347	0.5151	1.800	1.325	1.607	0.5141	2.060
Modified CV	6.000	6.000	8.000	6.000	6.000	6.000	8.000	6.000
Min	9.080	8.855	8.918	8.308	9.037	8.819	8.950	8.296
Max	9.469	9.276	9.045	8.965	9.426	9.303	9.078	8.963
No. Batches	3	3	1	3	3	3	1	3
No. Spec.	18	18	6	18	18	18	6	18

Table 4-20: Statistics from UNT1 Modulus data

## 4.9 "10/80/10" Unnotched Tension 2 (UNT2)

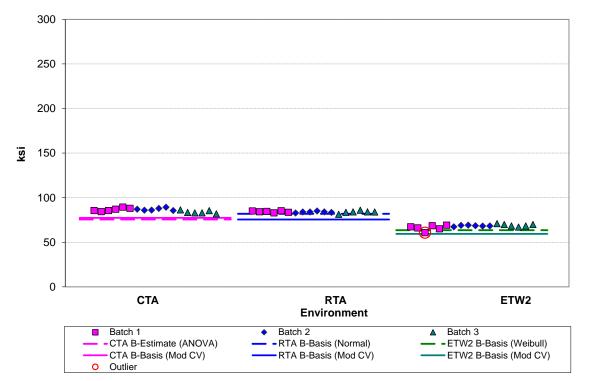
The UNT2 data is normalized, so both normalized and as-measured values are provided. Data is available for two properties, strength and modulus. UNT2 tests were performed at three different environmental conditions.

The CTA datasets, both normalized and as-measured, failed the Anderson Darling ksample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. Both of the CTA datasets passed the ADK test after the modified CV transformation, so modified CV basis values are provided for those datasets.

The ETW2 datasets, both normalized and as-measured, failed the normality test, but the Weibull distribution had an adequate fit, so design values were computed using the Weibull distribution. After the modified CV transformation of the data, these datasets passed the normality test so modified CV basis values are provided. Pooling was appropriate for all three conditions for modified CV basis values for both the normalized and as-measured datasets.

There was one statistical outlier. The lowest value in batch one of the ETW2 condition was an outlier for the ETW2 condition but not for the batch one. It was an outlier for both the normalized and as-measured datasets. It was retained for this analysis.

Statistics, basis values and estimates are given for UNT2 strength data in Table 4-21 and for the modulus data in Table 4-22. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-12.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape "Soft" Unnotched Tension Strength Normalized (UNT2)

Figure 4-12: Batch Plot for	UNT2 strength normalized
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Ur	Unnotched Tension (UNT2) Strength Basis Values and Statistics							
	Normalized				As-measured			
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (- 65°F)	RTA (70°F)	ETW2 (250°F)		
Mean	85.87	84.03	67.92	85.69	83.76	67.84		
Stdev	2.153	1.030	2.262	2.451	1.196	2.141		
CV	2.508	1.225	3.331	2.860	1.428	3.157		
Modified CV	6.000	6.000	6.000	6.000	6.000	6.000		
Min	81.84	81.41	60.80	81.36	80.60	60.84		
Max	89.50	85.95	70.98	89.79	85.41	70.26		
No. Batches	3	3	3	3	3	3		
No. Spec.	18	18	18	18	18	18		
		Basis Va	alues and Es	timates				
B-basis Value		82.00	63.57		81.40	64.12		
B-estimate	75.66			72.33				
A-estimate	68.38	80.56	58.88	62.80	79.72	60.03		
Method	ANOVA	Normal	Weibull	ANOVA	Normal	Weibull		
	Modified CV Basis Values and Estimates							
B-basis Value	77.40	75.56	59.45	77.24	75.31	59.39		
A-estimate	71.75	69.92	53.81	71.61	69.68	53.75		
Method	pooled	pooled	pooled	pooled	pooled	pooled		

Table 4-21: Statistics and Basis Values for UNT2 Strength data

#### NCP-RP-2023-002 Rev A

	Unnotched Tension (UNT2) Modulus Statistics								
		Normalized			As-measure	d			
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)			
Mean	5.909	5.669	4.464	5.897	5.651	4.459			
Stdev	0.1378	0.08138	0.06625	0.1625	0.08926	0.06361			
CV	2.333	1.435	1.484	2.756	1.580	1.426			
Modified CV	6.000	6.000	6.000	6.000	6.000	6.000			
Min	5.650	5.516	4.348	5.588	5.511	4.347			
Мах	6.235	5.816	4.602	6.255	5.813	4.555			
No. Batches	3	3	3	3	3	3			
No. Spec.	18	18	18	18	18	18			

# 4.10 "50/40/10" Unnotched Tension 3 (UNT3)

The UNT3 data is normalized, so both normalized and as-measured values are provided. Data is available for two properties, strength and modulus. UNT3 tests were performed at three different environmental conditions.

The as-measured ETW2 dataset failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. This dataset passed the ADK test after the modified CV transformation, so modified CV basis values are provided for that dataset.

The normalized RTA dataset failed the normality test, but the Weibull distribution had an adequate fit, so design values were computed using the Weibull distribution. After the modified CV transformation of the data, this dataset passed the normality test so modified CV basis values are provided.

The normalized CTA dataset failed all three distribution tests, requiring the nonparametric approach to compute design values. After the modified CV transformation of the data, this dataset did not pass the normality test so modified CV basis values are not provided.

After the modified CV transformation of the normalized ETW2 dataset, this dataset did not pass the normality test so modified CV basis values are not provided.

Pooling was appropriate for the as-measured CTA and RTA datasets.

There were two statistical outliers. The largest value in batch two of the CTA condition was an outlier for batch two but not for the CTA condition. The lowest value in batch two of the RTA condition was an outlier for both batch two and the RTA condition. Those outliers were for both the normalized and as-measured datasets. Both outliers were retained for this analysis.

Statistics and basis values are given for UNT3 strength data in Table 4-23 and for the modulus data in Table 4-24. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-13.



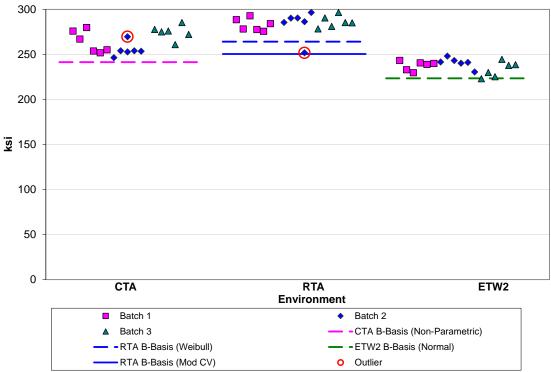


Figure	4-13:	Batch	Plot fo	or UNT3	strength	normalized
Inguic	<b>-</b> 10.	Duton	1 100 10		Sucigui	nonnanzoa

Unnotched Tension (UNT3) Strength Basis Values and Statistics								
Normalized				As-measured				
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)		
Mean	264.5	284.1	237.2	263.3	282.7	236.4		
Stdev	12.11	10.20	6.982	11.09	9.988	7.318		
CV	4.581	3.589	2.944	4.211	3.533	3.096		
Modified CV	6.290	6.000	6.000	6.106	6.000	6.000		
Min	246.4	251.8	223.1	247.4	252.2	221.7		
Max	285.3	296.5	248.1	282.0	296.8	248.1		
No. Batches	3	3	3	3	3	3		
No. Spec.	18	18	18	18	18	18		
		Basis Va	alues and Es	timates				
B-basis Value	241.4	264.1	223.4	244.1	263.5			
B-estimate						208.1		
A-estimate	197.8	242.8	213.6	231.0	250.4	187.9		
Method	Non-Parm.	Weibull	Normal	pooled	pooled	ANOVA		
	Modified CV Basis Values and Estimates							
B-basis Value		250.5		233.2	252.6	208.4		
A-estimate	NA	226.7	NA	212.8	232.1	188.6		
Method		Normal		pooled	pooled	Normal		

Table 4-23: Statistics and Basis Values for UNT3 Strength data

#### NCP-RP-2023-002 Rev A

	Unnotched Tension (UNT3) Modulus Statistics								
		Normalized			As-measure	d			
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)			
Mean	14.52	14.34	14.09	14.46	14.26	14.05			
Stdev	0.1544	0.1281	0.2426	0.1825	0.1429	0.2616			
CV	1.064	0.8935	1.721	1.262	1.002	1.862			
Modified CV	6.000	6.000	6.000	6.000	6.000	6.000			
Min	14.20	14.09	13.67	14.05	13.99	13.66			
Мах	14.82	14.57	14.51	14.74	14.45	14.43			
No. Batches	3	3	3	3	3	3			
No. Spec.	18	18	18	18	18	18			

Table 4-24: Statistics from UNT3 Modulus data

#### 4.11 "33/0/67" Unnotched Compression 0/90 (UNC0)

The UNC0 data is normalized, so both normalized and as-measured values are provided. Data is available for two properties, strength and modulus. UNC0 tests were performed at six different environmental conditions. The ETA1, ETA2 and ETW1 conditions only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for those conditions.

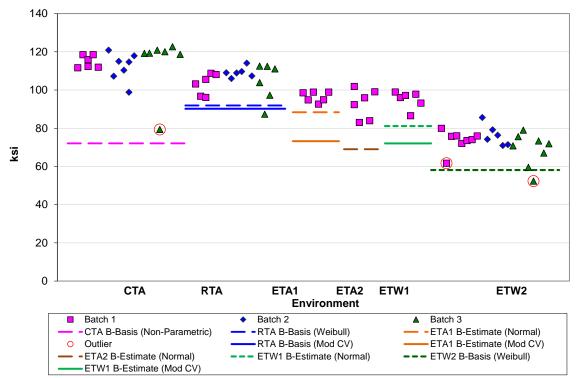
The RTA and ETW2 datasets, both normalized and as-measured, did not have an adequate fit to the normal distribution. The Weibull distribution was used to compute the basis values. After the transformation of data to fit the assumptions of the modified CV method, those datasets all passed the normality test so modified CV basis values are provided.

The CTA dataset, both normalized and as-measured, failed all three distribution tests, requiring the non-parametric approach to compute design values.

The CTA, ETA2 and ETW2 datasets, both normalized and as-measured, had a CV. higher than 8%, so modified CV basis values could not be provided for those datasets.

There were three outliers. The lowest value in batch three of the CTA condition was an outlier for both batch three and the CTA condition. The lowest value in batch one of the ETW2 condition was an outlier for the batch one but not for the ETW2 condition. The lowest value in batch three of the ETW2 condition was an outlier for the ETW2 condition but not for the batch three. All three outliers were outliers for both the normalized and asmeasured datasets. All three outliers were retained for this analysis.

Statistics and estimates of basis values are given for the normalized strength data in Table 4-25, the as-measured strength data in Table 4-26, for the normalized modulus data in Table 4-27 and for the as-measured modulus data in Table 4-28. The normalized data, B-basis values and B-estimates are shown graphically in Figure 4-14.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Unnotched Compression 0/90 Strength Normalized (UNC0)

Unnotcheo	Unnotched Compression 0/90 (UNC0) Strength Basis Values and Statistics Normalized						
Env	CTA (− 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)	
Mean	113.7	105.4	96.45	92.70	94.93	72.55	
Stdev	9.844	6.998	2.670	7.812	4.560	7.267	
CV	8.659	6.637	2.768	8.427	4.803	10.02	
Modified CV	8.659	7.319	8.000	8.427	8.000	10.02	
Min	79.36	87.36	92.65	83.03	86.54	52.35	
Max	122.6	114.1	98.92	101.9	98.92	85.64	
No. Batches	3	3	1	1	1	3	
No. Spec.	20	18	6	6	6	22	
		Basis V	alues and Es	timates			
B-basis Value	72.10	91.89				58.10	
B-estimate			88.36	69.04	81.12		
A-estimate	43.78	78.40	82.61	52.22	71.30	45.05	
Method	Non-Parm.	Weibull	Normal	Normal	Normal	Weibull	
		Modified CV	Basis Values a	and Estimate	S		
B-basis Value		90.21					
B-estimate	NA		73.20	NA	72.05	NA	
A-estimate	NA	79.43	57.30	NA	56.40	NA	
Method		Normal	Normal		Normal		

Table 4-25: Statistics and Basis Values for UNC0 Strength data Normalized

Unnotched Compression 0/90 (UNC0) Strength Basis Values and Statistics As-measured									
Env	CTA (− 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)			
Mean	113.4	105.4	96.70	93.24	95.24	72.52			
Stdev	9.721	7.617	2.533	7.969	3.878	7.458			
CV	8.575	7.227	2.619	8.547	4.071	10.28			
Modified CV	8.575	7.613	8.000	8.547	8.000	10.28			
Min	79.33	86.63	93.94	82.39	88.35	51.70			
Мах	121.3	113.7	100.6	101.5	99.77	86.12			
No. Batches	3	3	1	1	1	3			
No. Spec.	20	18	6	6	6	22			
		Basis V	alues and Es	timates	_				
B-basis Value	72.06	91.02				57.81			
B-estimate			89.03	69.10	83.50				
A-estimate	44.42	76.80	83.58	51.94	75.15	44.60			
Method	Non-Parm.	Weibull	Normal	Normal	Normal	Weibull			
	Modified CV Basis Values and Estimates								
B-basis Value		89.56							
B-estimate	NA		73.40	NA	72.29	NA			
A-estimate	IN/A	78.35	57.45	NA	56.58	INA			
Method		Normal	Normal		Normal				

Table 4-26: Statistics and Basis Values for UNC0 Strength data As-measured

ι	Unnotched Compression 0/90 (UNC0) Modulus Statistics Normalized							
Env	CTA (- 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)		
Mean	8.023	8.033	7.903	7.979	8.202	8.231		
Stdev	0.3060	0.1682	0.1185	0.1900	0.1044	0.2513		
CV	3.813	2.094	1.499	2.381	1.273	3.053		
Mod CV	6.000	6.000	8.000	8.000	8.000	6.000		
Min	7.464	7.780	7.704	7.752	8.087	7.778		
Мах	8.694	8.294	8.054	8.307	8.352	8.559		
No. Batches	3	3	1	1	1	3		
No. Spec.	19	18	6	6	6	18		

Table 4-27: Statistics from UNC0 Modulus data Normalized

U	Unnotched Compression 0/90 (UNC0) Modulus Statistics As-measured							
Env	CTA (− 65°F)	RTA (70°F)	ETA1 (180°F)	ETA2 (250°F)	ETW1 (180°F)	ETW2 (250°F)		
Mean	8.000	8.028	7.924	8.024	8.231	8.231		
Stdev	0.3484	0.1863	0.1430	0.1293	0.1310	0.2116		
CV	4.355	2.321	1.805	1.612	1.591	2.570		
Mod CV	6.178	6.000	8.000	8.000	8.000	6.000		
Min	7.462	7.759	7.762	7.855	7.994	7.917		
Max	8.976	8.343	8.091	8.243	8.361	8.548		
No. Batches	3	3	1	1	1	3		
No.Spec.	19	18	6	6	6	18		

Table 4-28: Statistics from UNC0 Modulus data As-measured

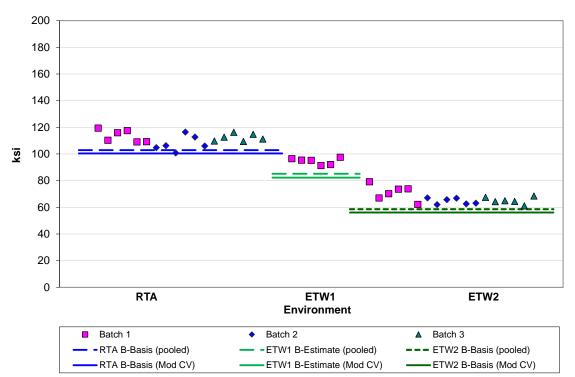
# 4.12 "25/50/25" Unnotched Compression 1 (UNC1)

The UNC1 data is normalized, so both normalized and as-measured values are provided. Data is available for two properties, strength and modulus. UNC1 tests were performed at three different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for that condition.

All three conditions met the requirements for pooling for both the normalized and asmeasured datasets

There were no statistical outliers.

Statistics, basis values and estimates are given for UNC1 strength data in Table 4-29 and for the modulus data in Table 4-30. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-15.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Quasi Isotropic Unnotched Compression Strength Normalized (UNC1)

Figure 4-15: Batch plot for UNC1 strength normalized

Unnotched Compression (UNC1) Strength Basis Values and Statistics								
		Normalized		As-measured				
Env	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)		
Mean	111.2	94.69	66.92	111.1	94.98	66.87		
Stdev	4.934	2.454	4.784	4.905	2.320	4.944		
CV	4.435	2.591	7.149	4.415	2.443	7.393		
Modified CV	6.218	8.000	7.574	6.207	8.000	7.696		
Min	100.8	91.32	61.16	101.5	91.64	60.69		
Max	119.4	97.52	79.19	118.9	97.74	79.35		
No. Batches	3	1	3	3	1	3		
No. Spec.	18	6	18	18	6	18		
		Basis Va	lues and Esti	mates				
B-basis Value	102.9		58.59	102.7		58.45		
B-estimate		85.14			85.33			
A-estimate	97.29	79.70	52.96	97.00	79.83	52.76		
Method	pooled	pooled	pooled	pooled	pooled	pooled		
	Modified CV Basis Values and Estimates							
<b>B-basis Value</b>	100.4		56.08	100.2		56.00		
B-estimate		82.26			82.51			
A-estimate	93.08	75.17	48.75	92.88	75.40	48.64		
Method	pooled	pooled	pooled	pooled	pooled	pooled		

Table 4-29: Statistics and Basis Values for UNC1 Strength data

Unnotched Compression (UNC1) Modulus Statistics						
	Normalized			As-measured		
Env	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)
Mean	8.088	7.839	7.810	8.078	7.864	7.804
Stdev	0.1448	0.08973	0.1664	0.1733	0.09751	0.1776
cv	1.791	1.145	2.130	2.145	1.240	2.276
Modified CV	6.000	8.000	6.000	6.000	8.000	6.000
Min	7.726	7.695	7.413	7.696	7.703	7.446
Max	8.293	7.969	8.048	8.302	7.998	8.074
No. Batches	3	1	3	3	1	3
No. Spec.	18	6	18	18	6	18

Table 4-30: Statistics from UNC1 Modulus data

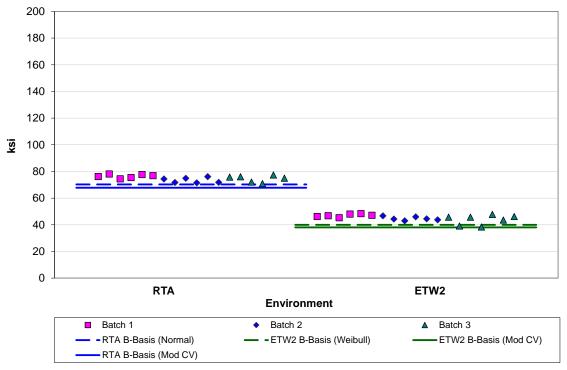
# 4.13 "10/80/10" Unnotched Compression 2 (UNC2)

The UNC2 data is normalized, so both normalized and as-measured values are provided. Data is available for two properties, strength and modulus. UNC2 tests were performed at two different environmental conditions.

The normalized ETW2 datasets, both normalized and as-measured, failed the normality test, but the Weibull distribution had an adequate fit, so design values were computed using the Weibull distribution. After the modified CV transformation of the data, this dataset passed the normality test so modified CV basis values are provided. Pooling the RTA and ETW2 datasets was appropriate for the modified CV basis value computations.

There were no statistical outliers.

Statistics and basis values are given for UNC2 strength data in Table 4-31 and for the modulus data in Table 4-32. The normalized data and the B-basis values are shown graphically in Figure 4-16.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape "Soft" Unnotched Compression Strength Normalized (UNC2)

Figure 4-16: Batch plot for UNC2 strength normalized

Unnotched C	Unnotched Compression (UNC2) Strength Basis Values and Statistics							
	Norm	alized	As-me	asured				
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)				
Mean	74.78	45.09	74.72	45.10				
Stdev	2.291	2.711	2.368	2.791				
CV	3.064	6.013	3.169	6.189				
Modified CV	6.000	7.006	6.000	7.094				
Min	70.86	38.33	70.72	38.22				
Max	78.12	48.42	78.56	48.66				
No. Batches	3	3	3	3				
No. Spec.	18	19	18	19				
	Basis Va	lues and Es	timates					
B-basis Value	70.26	39.96	70.04	39.72				
A-estimate	67.05	34.74	66.73	34.30				
Method	Normal	Weibull	Normal	Weibull				
Мо	dified CV B	asis Values a	and Estimate	es				
B-basis Value	67.77	38.11	67.67	38.09				
A-estimate	63.00	33.33	62.89	33.30				
Method	pooled	pooled	pooled	pooled				

Table 4-31: Statistics and Basis Values for UNC2 Strength data

Unnotc	Unnotched Compression (UNC2) Modulus Statistics						
	Norm	alized	As-me	asured			
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)			
Mean	5.046	4.365	5.041	4.367			
Stdev	0.09109	0.1250	0.08613	0.1292			
cv	1.805	2.862	1.709	2.958			
Modified CV	6.000	6.000	6.000	6.000			
Min	4.866	4.153	4.881	4.131			
Max	5.187	4.654	5.182	4.659			
No. Batches	3	3	3	3			
No. Spec.	18	18	18	18			

Table 4-32: Statistics from UNC2 Modulus data

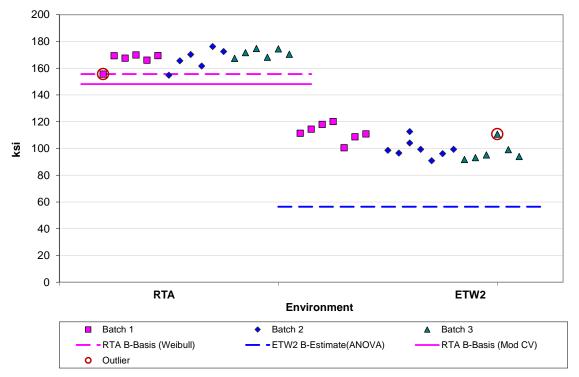
## 4.14 "50/40/10" Unnotched Compression 3 (UNC3)

The UNC3 data is normalized, so both normalized and as-measured values are provided. Data is available for two properties, strength and modulus. UNC3 tests were performed at two different environmental conditions.

The ETW2 datasets, both normalized and as-measured, failed the Anderson Darling ksample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. These datasets did not pass the ADK test after the modified CV transformation, so modified CV basis values are not provided for that dataset.

There were two statistical outliers. The lowest value in batch one of the RTA condition is an outlier for batch one but not for the RTA condition. The largest value in batch three of the ETW2 condition is an outlier for batch three but not for the ETW2 condition. Those outliers were for both the normalized and as-measured datasets. Both outliers were retained for this analysis.

Statistics, basis values and estimates are given for UNC3 strength data in Table 4-33 and for the modulus data in Table 4-34. The normalized data, B-estimates and the B-basis values are shown graphically in Figure 4-17.



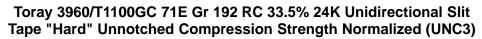


Figure 4-17: Batch plot for UNC3 strength normalized

Unnotched Compression (UNC3) Strength Basis Values and									
		Statistics							
	Normalized As-measured								
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)					
Mean	168.1	103.1	167.6	102.8					
Stdev	5.873	9.052	6.326	8.788					
CV	3.494	8.777	3.774	8.546					
Modified CV	6.000	8.777	6.000	8.546					
Min	154.7	90.82	154.0	90.97					
Мах	176.2	120.2	177.6	119.8					
No. Batches	3	3	3	3					
No. Spec.	18	21	18	21					
	Basis Va	alues and Es	timates						
B-basis Value	155.7		155.1						
B-estimate		56.45		57.99					
A-estimate	142.5	23.12	146.3	25.98					
Method	Weibull	ANOVA	Normal	ANOVA					
Мо	dified CV B	asis Values a	and Estimate	es					
B-basis Value	148.2		147.7						
A-estimate	134.1	NA	133.7	NA					
Method	Normal		Normal						

Table 4-33: Statistics and Basis Values for UNC3 Strength data

Unnotc	Unnotched Compression (UNC3) Modulus Statistics						
	Norm	alized	As-me	asured			
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)			
Mean	12.53	12.64	12.50	12.61			
Stdev	0.1093	0.4571	0.1513	0.4759			
cv	0.8722	3.616	1.211	3.773			
Modified CV	6.000	6.000	6.000	6.000			
Min	12.24	11.95	12.19	11.99			
Max	12.73	14.31	12.75	14.38			
No. Batches	3	3	3	3			
No. Spec.	18	21	18	21			

Table 4-34: Statistics from UNC3 Modulus data

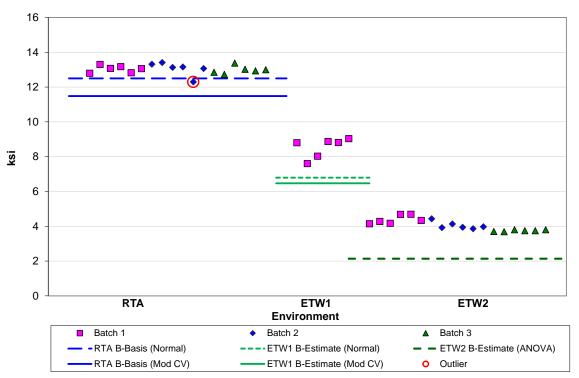
#### 4.15 "25/50/25" Laminate Short-Beam Strength (SBS1)

The SBS1 data is not normalized, only as-measured values are provided. Data is available for only one property, strength. SBS1 tests were performed at three different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for those conditions.

The ETW2 dataset failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. This dataset did not pass the ADK test after the modified CV transformation, so modified CV basis values are not provided for that dataset.

There was one outlier. The lowest value in batch two of the RTA condition was an outlier for both batch two and the RTA condition. It was retained for this analysis.

Statistics, estimates and basis values are given for SBS1 strength data in Table 4-35. The as-measured data, B-estimates and the B-basis values are shown graphically in Figure 4-18.



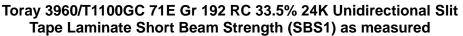


Figure 4-18: Batch plot for SBS1 strength as-measured

	Laminate Short Beam Strength (SBS1) Basis Values and Statistics As-measured							
Env	v RTA (70°F) ETW1 (180°F) ETW2 (250°F)							
Mean	13.03	8.527	4.059					
Stdev	0.2699	0.5727	0.3212					
CV	2.072	6.716	7.913					
Modified CV	6.000	8.000	7.957					
Min	12.30	7.604	3.687					
Max	13.41	9.036	4.690					
No. Batches	3	1	3					
No. Spec.	18	6	18					
E	Basis Values :	and Estimates	S					
B-basis Value	12.50							
B-estimate		6.792	2.135					
A-estimate	12.12	5.559	0.7625					
Method	Normal	Normal	ANOVA					
Modifie	d CV Basis V	alues and Es	timates					
B-basis Value	11.49							
B-estimate		6.472	NA					
A-estimate	10.39	5.066	INA					
Method	Normal	Normal						

Table 4-35: Statistics and Basis Values for SBS1 Strength data

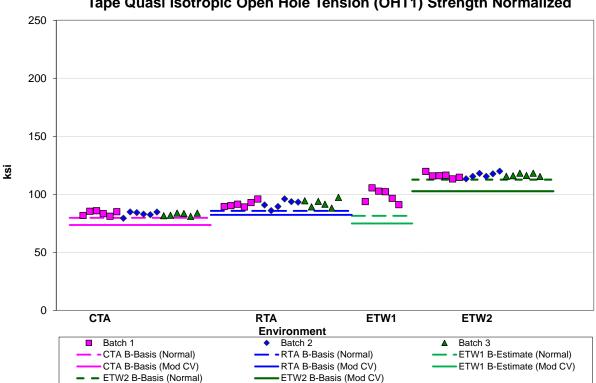
## 4.16 "25/50/25" Open-Hole Tension 1 (OHT1)

The OHT1 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. OHT1 tests were performed at four different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for that condition.

The CTA and RTA conditions could be pooled for the as-measured datasets but not for the normalized datasets due to a failure of Levene's test. The CTA and RTA conditions could be pooled for both normalized and as-measured datasets for the modified CV computations.

There were no statistical outliers.

Statistics, basis values and estimates are given for OHT1 strength data in Table 4-36. The normalized data, B-basis values and B-estimates are shown graphically in Figure 4-19.



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Quasi Isotropic Open Hole Tension (OHT1) Strength Normalized

Figure 4-19: Batch Plot for OHT1 strength normalized

	Open Hole Tension (OHT1) Strength Basis Values and Statistics									
			alized			-	easured			
Env	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)		
Mean	83.15	91.82	98.66	116.4	83.02	91.68	98.88	116.4		
Stdev	1.756	3.068	5.692	1.897	1.867	2.855	5.805	1.840		
CV	2.112	3.341	5.769	1.630	2.249	3.114	5.870	1.581		
Modified CV	6.000	6.000	8.000	6.000	6.000	6.000	8.000	6.000		
Min	79.39	85.99	91.13	113.2	79.70	86.34	91.35	113.8		
Мах	85.83	97.38	105.6	120.0	86.11	96.66	105.7	119.9		
No. Batches	3	3	1	3	3	3	1	3		
No. Spec.	18	18	6	18	18	18	6	18		
			Basis V	alues and Es	stimates					
B-basis Value	79.68	85.77		112.7	78.63	87.29		112.7		
B-estimate			81.42				81.30			
A-estimate	77.23	81.48	69.17	110.0	75.64	84.30	68.80	110.2		
Method	Normal	Normal	Normal	Normal	pooled	pooled	Normal	Normal		
		M	odified CV B	Basis Values	and Estimate	es				
B-basis Value	73.58	82.25		102.6	73.46	82.12		102.6		
B-estimate			74.89				75.05			
A-estimate	67.06	75.74	58.62	92.86	66.96	75.62	58.75	92.84		
Method	pooled	pooled	Normal	Normal	pooled	pooled	Normal	Normal		

Table 4-36: Statistics and Basis Values for OHT1 Strength data

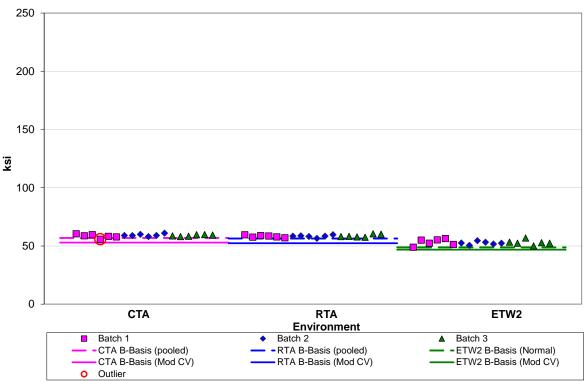
# 4.17 "10/80/10" Open-Hole Tension 2 (OHT2)

The OHT2 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. OHT2 tests were performed at three different environmental conditions.

The CTA and RTA conditions could be pooled for the normalized datasets but the ETW2 condition could not be included due to a failure of the normality test for the pooled dataset. All three conditions could be pooled for the normalized modified CV computations. All three conditions met the requirements for pooling for the as-measured datasets.

There was one statistical outliers. The lowest value in batch one of the normalized CTA dataset was an outlier for the CTA condition only. It was not an outlier for the batch one or the as-measured dataset. It was retained for this analysis.

Statistics, basis values and estimates are given for OHT2 strength data in Table 4-37. The normalized data and the B-basis values are shown graphically in Figure 4-20.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape "Soft" Open Hole Tension (OHT2) Strength Normalized

Figure 4-20: Batch Plot for OHT2 strength normalized

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C	Open Hole Tension (OHT2) Strength Basis Values and Statistics							
	Normalized				As-measure	d		
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)		
Mean	58.92	58.42	52.89	58.83	58.34	52.80		
Stdev	1.161	1.054	2.096	1.177	1.126	2.054		
CV	1.970	1.805	3.963	2.000	1.931	3.890		
Modified CV	6.000	6.000	6.000	6.000	6.000	6.000		
Min	55.82	56.52	48.96	56.13	56.51	49.18		
Max	60.97	60.46	56.83	60.89	60.55	56.55		
No. Batches	3	3	3	3	3	3		
No. Spec.	18	18	18	18	18	18		
		Basis Val	ues and Esti	mates				
B-basis Value	56.90	56.40	48.75	56.15	55.66	50.12		
A-estimate	55.53	55.02	45.82	54.36	53.87	48.34		
Method	pooled	pooled	Normal	pooled	pooled	pooled		
	Modified CV Basis Values and Estimates							
B-basis Value	52.89	52.38	46.85	52.80	52.31	46.78		
A-estimate	48.86	48.35	42.83	48.78	48.29	42.76		
Method	pooled	pooled	pooled	pooled	pooled	pooled		

Table 4-37: Statistics and Basis Values for OHT2 Strength data

# 4.18 "50/40/10" Open-Hole Tension 3 (OHT3)

The OHT3 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. OHT3 tests were performed at three different environmental conditions.

All three conditions met the requirements for pooling for both the normalized and asmeasured datasets.

There were no statistical outliers.

Statistics, basis values and estimates are given for OHT3 strength data in Table 4-38. The normalized data and B-basis values are shown graphically in Figure 4-21.

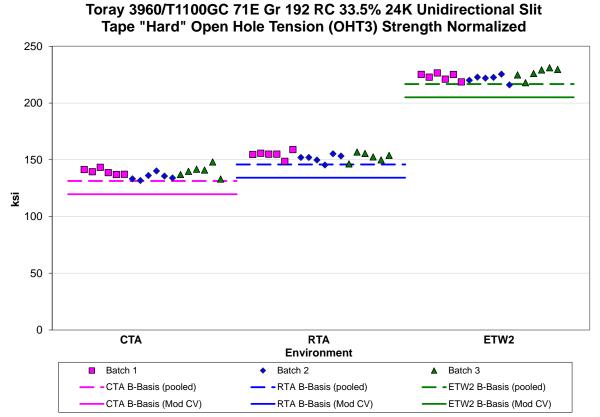


Figure 4-21: Batch Plot for OHT3 strength normalized

C	Open Hole Tension (OHT3) Strength Basis Values and Statistics							
		Normalized			As-measure	b		
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)		
Mean	138.3	152.8	223.7	137.2	151.7	222.1		
Stdev	4.107	3.617	4.118	3.813	3.819	3.245		
CV	2.971	2.367	1.841	2.779	2.517	1.461		
Modified CV	6.000	6.000	6.000	6.000	6.000	6.000		
Min	131.8	145.4	215.9	130.6	144.4	216.1		
Мах	148.1	159.0	231.1	145.3	159.4	227.5		
No. Batches	3	3	3	3	3	3		
No. Spec.	18	18	18	18	18	18		
		Basi	s Value Esti	mates				
B-basis Value	131.3	145.8	216.7	130.8	145.3	215.7		
A-estimate	126.6	141.2	212.0	126.5	141.0	211.4		
Method	pooled	pooled	pooled	pooled	pooled	pooled		
	Modified CV Basis Values and Estimates							
<b>B-basis Value</b>	119.6	134.2	205.0	118.7	133.2	203.6		
A-estimate	107.2	121.7	192.6	106.4	120.8	191.2		
Method	pooled	pooled	pooled	pooled	pooled	pooled		

Table 4-38: Statistics and Basis Values for OHT3 Strength data

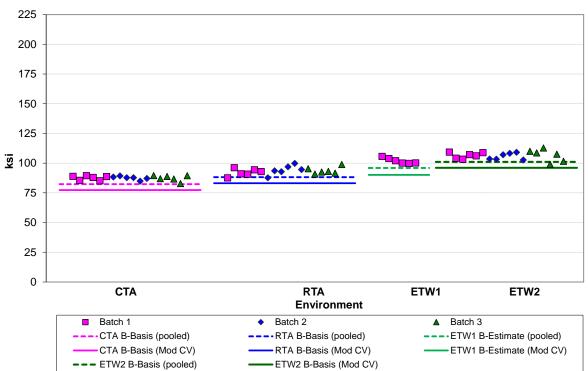
# 4.19 "25/50/25" Filled-Hole Tension 1 (FHT1)

The FHT1 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. FHT1 tests were performed at four different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for that condition.

All conditions met the requirements for pooling for both the normalized and asmeasured datasets.

There were no statistical outliers.

Statistics, estimates and basis values are given for FHT1 strength data in Table 4-39. The normalized data, B-estimates and the B-basis values are shown graphically in Figure 4-22.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Quasi Isotropic Filled Hole Tension (FHT1) Strength normalized

Figure 4-22: Batch plot for FHT1 strength normalized

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Filled-Hole Tension (FHT1) Strength Basis Values and Statistics									
	Normalized					As-me	asured		
Env	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	CTA (- 65°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	
Mean	87.50	93.35	101.9	106.3	87.53	93.29	102.1	106.2	
Stdev	1.885	3.312	2.402	3.508	1.955	3.171	2.507	3.372	
CV	2.155	3.548	2.357	3.302	2.233	3.399	2.455	3.175	
Modified CV	6.000	6.000	8.000	6.000	6.000	6.000	8.000	6.000	
Min	82.79	87.61	99.75	99.08	83.22	87.87	99.89	98.76	
Max	89.52	99.75	105.6	112.8	90.30	99.75	106.0	112.1	
No. Batches	3	3	1	3	3	3	1	3	
No. Spec.	18	18	6	18	18	18	6	18	
			Basis V	alues and Es	timates				
<b>B-basis Value</b>	82.32	88.16		101.1	82.48	88.24		101.1	
B-estimate			95.93				96.31		
A-estimate	78.87	84.72	92.58	97.62	79.12	84.88	93.05	97.78	
Method	pooled	pooled	pooled	pooled	pooled	pooled	pooled	pooled	
		N	odified CV E	Basis Values a	and Estimate	S		-	
<b>B-basis Value</b>	77.30	83.14		96.05	77.33	83.09		95.99	
B-estimate			90.14				90.37		
A-estimate	70.51	76.36	83.54	89.26	70.55	76.30	83.77	89.20	
Method	pooled	pooled	pooled	pooled	pooled	pooled	pooled	pooled	

Table 4-39: Statistics and Basis Values for FHT1 Strength data

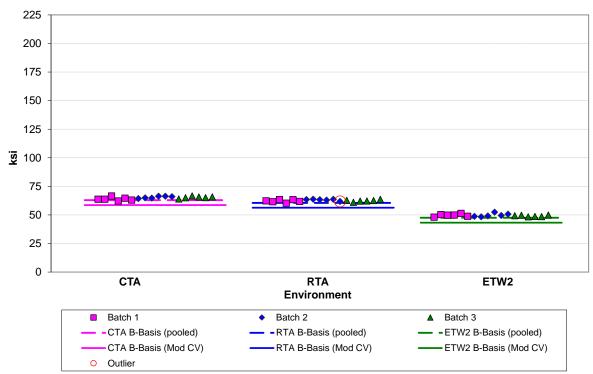
# 4.20 "10/80/10" Filled-Hole Tension 2 (FHT2)

The FHT2 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. FHT2 tests were performed at three different environmental conditions.

All three conditions met the requirements for pooling for both the normalized and asmeasured datasets.

There was one statistical outlier. The lowest value in batch two for the normalized RTA dataset was an outlier for batch two but not for the RTA condition and not for the asmeasured dataset. It was retained for this analysis.

Statistics and basis values are given for FHT2 strength data in Table 4-40. The normalized data and the B-basis values are shown graphically in Figure 4-23.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape "Soft" Filled Hole Tension (FHT2) Strength normalized

Figure 4-23: Batch plot for FHT2 strength normalized

	Filled-Hole T	ension (FHT2	) Strength Ba	sis Values a	nd Statistics	5
		Normalized			As-measure	d
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)
Mean	64.96	62.59	49.55	64.82	62.44	49.39
Stdev	1.281	1.008	1.129	1.288	1.085	1.217
CV	1.972	1.611	2.279	1.988	1.737	2.463
Modified CV	6.000	6.000	6.000	6.000	6.000	6.000
Min	62.25	60.25	48.13	62.36	60.29	47.81
Max	66.74	63.83	52.43	66.67	63.98	52.38
No. Batches	3	3	3	3	3	3
No. Spec.	18	18	18	18	18	18
		Basis Va	lues and Esti	mates		
B-basis Value	62.93	60.56	47.53	62.69	60.32	47.27
A-estimate	61.58	59.21	46.17	61.28	58.90	45.85
Method	pooled	pooled	pooled	pooled	pooled	pooled
	М	odified CV B	asis Values a	nd Estimates	5	
B-basis Value	58.65	56.28	43.24	58.52	56.14	43.10
A-estimate	54.44	52.07	39.03	54.32	51.94	38.90
Method	pooled	pooled	pooled	pooled	pooled	pooled

Table 4-40: Statistics and Basis Values for FHT2 Strength data

## 4.21 "50/40/10" Filled-Hole Tension 3 (FHT3)

The FHT3 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. FHT3 tests were performed at three different environmental conditions.

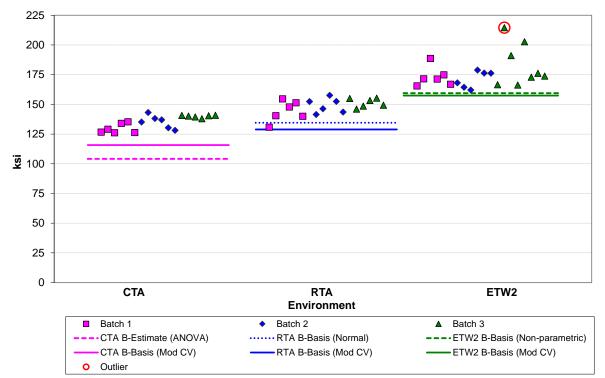
The normalized ETW2 dataset failed all three distribution tests, requiring the nonparametric approach to compute design values. After the modified CV transformation of the data, this dataset did pass the normality test, so modified CV basis values are provided.

The as-measured RTA and ETW2 datasets met all requirements for pooling.

The CTA datasets, both normalized and as-measured, failed the Anderson Darling ksample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. Both datasets passed the ADK test after the modified CV transformation, so modified CV basis values are provided for that dataset. Pooling was acceptable for computing the modified CV basis values.

There was one statistical outlier. The largest value in batch three of the ETW2 dataset was an outlier for the ETW2 condition, but not for the batch three. It was an outlier in both the normalized and as-measured datasets. It was retained for this analysis.

Statistics, estimates and basis values are given for FHT3 strength data in Table 4-41. The normalized data, B-estimates and B-basis values are shown graphically in Figure 4-24.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape "Hard" Filled Hole Tension (FHT3) Strength normalized

Figure 4-24: Batch plot for FHT3 strength normalized

	Filled-Hole Tension (FHT3) Strength Basis Values and Statistics						
		Normalized	· •	As-measured			
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	
Mean	134.9	148.1	176.4	134.5	147.4	175.9	
Stdev	5.752	6.879	13.41	5.846	7.109	12.98	
CV	4.263	4.644	7.600	4.348	4.823	7.380	
Modified CV	6.132	6.322	7.800	6.174	6.412	7.690	
Min	126.0	130.8	162.1	125.2	129.3	162.8	
Max	143.2	157.6	214.5	144.4	158.0	212.3	
No. Batches	3	3	3	3	3	3	
No. Spec.	18	18	20	18	18	20	
		Basis V	/alues and Est	imates			
<b>B-basis Value</b>		134.5	159.4		128.1	156.8	
B-estimate	104.1			103.4			
A-estimate	82.16	124.9	110.5	81.30	115.1	143.7	
Method	ANOVA	Normal	Non-Parametric	ANOVA	pooled	pooled	
		Modified CV	Basis Values a	nd Estimates	6		
B-basis Value	115.7	128.9	157.4	115.4	128.3	157.0	
A-estimate	102.9	116.1	144.6	102.7	115.6	144.3	
Method	pooled	pooled	pooled	pooled	pooled	pooled	
	Filled-Hole	Tension (FHT	3) Strength Ba	isis Values a	nd Statistics		
		Normalized	d		As-measured	k	
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	
Mean	134.9	148.1	176.4	134.5	147.4	175.9	
Stdev	5.752	6.879	13.41	5.846	7.109	12.98	
CV	4.263	4.644	7.600	4.348	4.823	7.380	
Modified CV	6.132	6.322	7.800	6.174	6.412	7.690	
Min	126.0	130.8	162.1	125.2	129.3	162.8	
Мах	143.2	157.6	214.5	144.4	158.0	212.3	
No. Batches	3	3	3	3	3	3	
No. Spec.	18	18	20	18	18	20	
	-	Basis V	alues and Est	imates			
B-basis Value	•	ļ	159.4			156.8	
B-estimate	104.1	134.5		103.4	128.1		
A-estimate	82.16	124.9	110.5	81.30	115.1	143.7	
Method	ANOVA	Normal	Non-Parametric	ANOVA	pooled	pooled	
Modified CV Basis Values and Estimates							
B-basis Value		128.9	157.4	115.4	128.3	157.0	
		1	1		128.3 115.6	157.0 144.3	

Table 4-41: Statistics and Basis Values for FHT3 Strength data

## 4.22 "25/50/25" Open-Hole Compression 1 (OHC1)

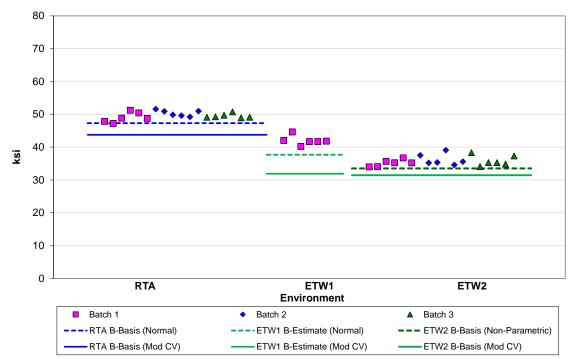
The OHC1 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. OHC1 tests were performed at three different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for that condition.

The as-measured ETW2 dataset failed the normality test, but the lognormal distribution had an adequate fit to compute design values. After the modified CV transformation of the data, the ETW2 as-measured dataset did pass the normality test, so modified CV basis values are provided.

The normalized ETW2 dataset failed all three distribution tests, requiring the nonparametric approach to compute design values. After the modified CV transformation of the data, the ETW2 normalized dataset did pass the normality test, so modified CV basis values are provided.

There was one statistical outlier. The largest value in the as-measured ETW1 dataset was an outlier. It was not an outlier in the normalized dataset. With only one batch tested in this condition, it can only be assessed as an outlier for batch, not the condition. It was retained for this analysis.

Statistics, estimates and basis values are given for OHC1 strength data in Table 4-42. The normalized data, B-estimates and the B-basis values are shown graphically in Figure 4-25.



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Quasi Isotropic Open Hole Compression (OHC1) Strength Normalized

	U	•		U		
Оре	en Hole Con	pression (OF	IC1) Strength	Basis Value	s and Statist	ics
		Normalized			As-measured	1
Env	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)
Mean	49.63	42.02	35.74	49.77	42.48	35.87
Stdev	1.173	1.431	1.471	1.061	1.530	1.448
CV	2.363	3.406	4.116	2.131	3.602	4.036
Modified CV	6.000	8.000	6.058	6.000	8.000	6.018
Min	47.24	40.22	33.97	47.93	40.88	33.86
Max	51.59	44.62	39.09	51.31	45.38	39.36
No. Batches	3	1	3	3	1	3
No. Spec.	18	6	18	18	6	18
		Basis V	alues and Es	timates		
B-basis Value	47.32		33.51	47.67		33.14
B-estimate		37.68			37.85	
A-estimate	45.68	34.60	27.54	46.19	34.55	31.35
Method	Normal	Normal	Non-Parm.	Normal	Normal	Lognormal
	Ν	lodified CV E	Basis Values a	and Estimate	es	
B-basis Value	43.75		31.46	43.87		31.61
B-estimate		31.89			32.24	
A-estimate	39.60	24.96	28.44	39.70	25.24	28.59
Method	Normal	Normal	Normal	Normal	Normal	Normal

Table 4-42: Statistics and Basis Values for OHC1 Strength data

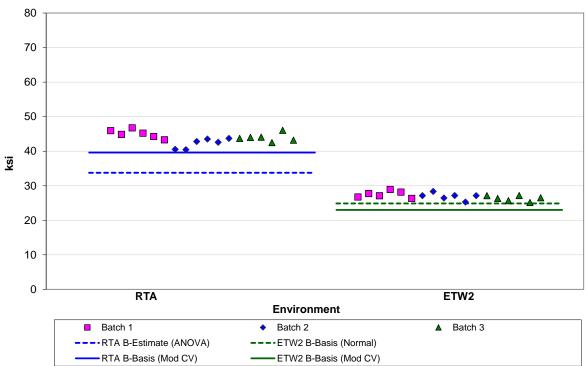
## 4.23 "10/80/10" Open-Hole Compression 2 (OHC2)

The OHC2 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. OHC2 tests were performed at two different environmental conditions.

The RTA datasets, both normalized and as-measured, failed the Anderson Darling ksample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. Both datasets passed the ADK test after the modified CV transformation, so modified CV basis values are provided for that dataset. Pooling was acceptable for computing the modified CV basis values.

There were no statistical outliers.

Statistics, estimates and basis values are given for OHC2 strength data in Table 4-43. The normalized data, B-estimates and the B-basis values are shown graphically in Figure 4-26.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape "Soft" Open Hole Compression Strength Normalized (OHC2)

Figure 4-26: Batch plot for OHC2 strength normalized

Open-Hole Compression (OHC2) Strength							
Basis Values and Statistics							
	Norm	Normalized As-measured					
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)			
Mean	43.60	26.99	43.50	26.93			
Stdev	1.815	1.069	1.846	1.132			
CV	4.164	3.962	4.243	4.202			
Modified CV	6.082	6.000	6.121	6.101			
Min	40.45	25.13	40.39	24.97			
Мах	46.76	28.94	46.52	29.06			
No. Batches	3	3	3	3			
No. Spec.	18	18	18	18			
	Basis Va	lues and Esti	mates				
B-basis Value		24.88		24.70			
B-estimate	33.77		33.14				
A-estimate	26.75	23.38	25.75	23.12			
Method	ANOVA	Normal	ANOVA	Normal			
М	Modified CV Basis Values and Estimates						
B-basis Value	39.59	22.99	39.47	22.90			
A-estimate	36.87	20.27	36.72	20.16			
Method	pooled	pooled	pooled	pooled			

Table 4-43: Statistics and Basis Values for OHC2 Strength data

## 4.24 "50/40/10" Open-Hole Compression 3 (OHC3)

The OHC3 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. OHC3 tests were performed at two different environmental conditions.

The RTA and ETW2 datasets, both normalized and as-measured, met all requirements for pooling. There were no statistical outliers.

Statistics, estimates and basis values are given for OHC3 strength data in Table 4-44. The normalized data and the B-basis values are shown graphically in Figure 4-27.

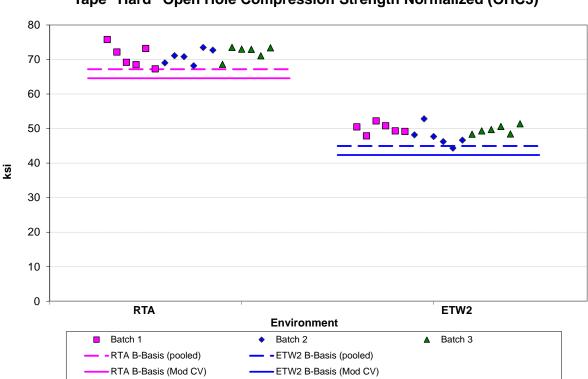




Figure 4-27: Batch plot for OHC3 strength normalized

Open-Hole Compression (OHC3) Strength Basis Values and Statistics							
	Norm	alized	As-me	asured			
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)			
Mean	71.33	49.09	71.04	48.89			
Stdev	2.388	2.153	2.351	2.024			
CV	3.348	4.386	3.309	4.139			
Modified CV	6.000	6.193	6.000	6.069			
Min	67.28	44.32	67.08	44.48			
Max	75.77	52.83	75.40	52.68			
No. Batches	3	3	3	3			
No. Spec.	18	18	18	18			
	Basis V	alues and Est	imates	-			
<b>B-basis Value</b>	67.19	44.95	67.04	44.90			
A-estimate	64.37	42.13	64.33	42.18			
Method	pooled	pooled	pooled	pooled			
Modified CV Basis Values and Estimates							
B-basis Value	64.57	42.33	64.35	42.20			
A-estimate	59.97	37.73	59.80	37.65			
Method	pooled	pooled	pooled	pooled			

Table 4-44: Statistics and Basis Values for OHC3 Strength data

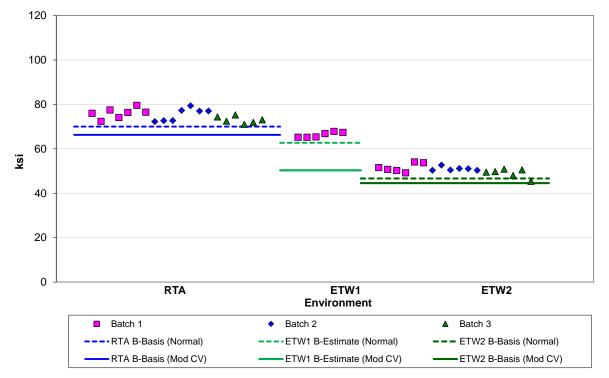
## 4.25 "25/50/25" Filled-Hole Compression 1 (FHC1)

The FHC1 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. FHC1 tests were performed at three different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for that condition.

The as-measured ETW2 dataset failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. This dataset passed the ADK test after the modified CV transformation, so modified CV basis values are provided for that dataset.

There was one statistical outlier. The lowest value in batch three of the as-measured ETW2 dataset was an outlier for the ETW2 condition but not for the batch three and not for the normalized dataset. It was retained for this analysis.

Statistics, estimates and basis values are given for FHC1 strength data in Table 4-45. The normalized data, B-estimates and the B-basis values are shown graphically in Figure 4-28.



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Quasi Isotropic Filled Hole Compression (FHC1) Strength Normalized

Figure 4-28: Batch plot for FHC1 strength normalized

Filled-Hole Compression (FHC1) Strength Basis Values and Statistics								
	Normalized				As-measured	I		
Env	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)		
Mean	74.94	66.31	50.52	75.03	66.92	50.65		
Stdev	2.578	1.201	1.967	2.789	0.7594	2.118		
CV	3.440	1.811	3.893	3.718	1.135	4.180		
Modified CV	6.000	8.000	6.000	6.000	8.000	6.090		
Min	71.04	65.19	45.36	70.71	66.27	44.94		
Max	79.57	67.82	54.05	79.59	68.08	54.15		
No. Batches	3	1	3	3	1	3		
No. Spec.	20	6	18	20	6	18		
		Basis Va	alues and Es	timates				
B-basis Value	69.98		46.63	69.66				
B-estimate		62.67			64.62	40.93		
A-estimate	66.45	60.08	43.88	65.84	62.98	33.99		
Method	Normal	Normal	Normal	Normal	Normal	ANOVA		
	Modified CV Basis Values and Estimates							
B-basis Value	66.28		44.53	66.36		44.56		
B-estimate		50.33			50.79			
A-estimate	60.13	39.39	40.30	60.20	39.76	40.26		
Method	Normal	Normal	Normal	Normal	Normal	Normal		

Table 4-45: Statistics and Basis Values for FHC1 Strength data

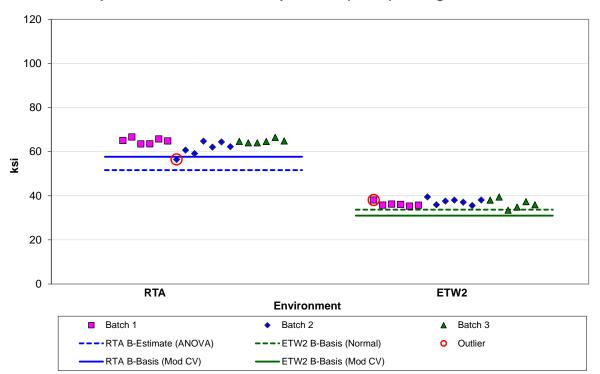
#### 4.26 "10/80/10" Filled-Hole Compression 2 (FHC2)

The FHC2 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. FHC2 tests were performed at two different environmental conditions.

The RTA datasets, both normalized and as-measured, failed the Anderson Darling ksample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. Both RTA datasets passed the ADK test after the modified CV transformation, so modified CV basis values are provided for that dataset. Pooling was acceptable for computing the modified CV basis values.

There were two statistical outliers. The lowest value in batch two of the RTA dataset was an outlier for the RTA condition but not for the batch two. It was an outlier in both the normalized and as-measured datasets. The largest value in batch one of the ETW2 condition was an outlier for batch one but not for the ETW2 condition. It was an outlier in both the normalized and as-measured datasets. Both outliers were retained for this analysis.

Statistics, estimates and basis values are given for FHC2 strength data in Table 4-46. The normalized data, B-estimates and the B-basis values are shown graphically in Figure 4-29.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape "Soft" Filled Hole Compression (FHC2) Strength Normalized

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Filled-Hole Compression (FHC2) Strength							
Basis Values and Statistics							
	Norm	alized	As-measured				
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)			
Mean	63.58	36.75	63.35	36.65			
Stdev	2.528	1.569	2.482	1.573			
CV	3.975	4.270	3.918	4.292			
Modified CV	6.000	6.135	6.000	6.146			
Min	56.49	33.48	56.07	33.07			
Max	66.66	39.49	66.47	39.55			
No. Batches	3	3	3	3			
No. Spec.	19	19	19	19			
	Basis V	alues and Est	imates				
B-basis Value		33.69		33.59			
B-estimate	51.66		52.50				
A-estimate	43.15	31.52	44.77	31.41			
Method	ANOVA	Normal	ANOVA	Normal			
Modified CV Basis Values and Estimates							
B-basis Value	57.93	31.09	57.71	31.02			
A-estimate	54.07	27.23	53.86	27.17			
Method	pooled	pooled	pooled	pooled			

#### Figure 4-29: Batch plot for FHC2 strength normalized

Table 4-46: Statistics and Basis Values for FHC2 Strength data

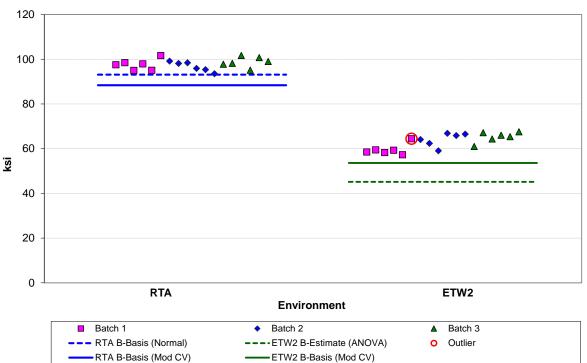
## 4.27 "50/40/10" Filled-Hole Compression 3 (FHC3)

The FHC3 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for only one property, strength. FHC3 tests were performed at two different environmental conditions.

The ETW2 datasets, both normalized and as-measured, failed the Anderson Darling ksample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. Both ETW2 datasets passed the ADK test after the modified CV transformation, so modified CV basis values are provided for that dataset. Pooling was acceptable for computing the modified CV basis values.

There was one statistical outlier. The largest value in batch one of the ETW2 condition was an outlier for batch one but not for the ETW2 condition. It was an outlier in both the normalized and as-measured datasets. It was retained for this analysis.

Statistics, estimates and basis values are given for FHC3 strength data in Table 4-47. The normalized data, B-estimates and the B-basis values are shown graphically in Figure 4-30.



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape "Hard" Filled Hole Compression (FHC3) Strength Normalized

Figure 4-30: Batch plot for FHC3 strength normalized

Filled-Hole Compression (FHC3) Strength							
Basis Values and Statistics							
	Norm	alized	As-mea	asured			
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)			
Mean	97.69	62.96	97.21	62.65			
Stdev	2.340	3.555	2.322	3.484			
CV	2.395	5.646	2.389	5.561			
Modified CV	6.000	6.823	6.000	6.781			
Min	93.50	57.25	93.39	56.97			
Мах	101.6	67.55	101.0	67.11			
No. Batches	3	3	3	3			
No. Spec.	18	18	18	18			
	Basis V	alues and Est	imates				
<b>B-basis Value</b>	93.07		92.62				
B-estimate		45.13		44.83			
A-estimate	89.80	32.41	89.37	32.13			
Method	Normal	ANOVA	Normal	ANOVA			
N	lodified CV B	asis Values a	nd Estimates	5			
B-basis Value	88.33	53.60	87.91	53.36			
A-estimate	81.96	47.23	81.59	47.03			
Method	pooled	pooled	pooled	pooled			

Table 4-47: Statistics and Basis Values for FHC3 Strength data

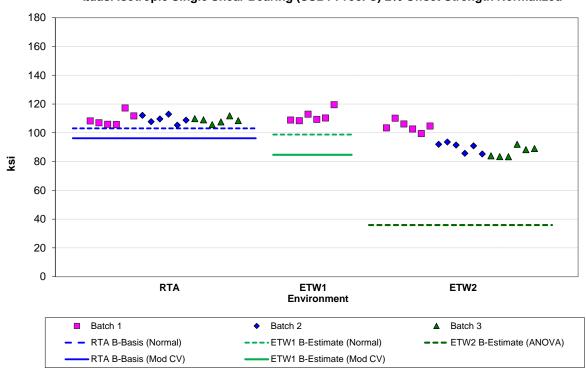
## 4.28 "25/50/25" Single-Shear Bearing 1 (SSB1, Proc. C)

The SSB1 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for three properties, 2% offset strength, ultimate and chord modulus. SSB1 tests were performed at three different environmental conditions. The ETW1 condition only conducted tests with one batch of material which is insufficient to meet CMH-17 guidelines, so only estimates of basis values are provided for that condition.

The ETW2 datasets for both 2% offset strength and ultimate strength, both the normalized and as-measured, failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. Only the normalized ETW2 ultimate strength dataset passed the ADK test after the modified CV transformation, so modified CV basis values are provided for that dataset only.

There was one statistical outlier. The largest value in batch three of the RTA condition for the ultimate strength property was an outlier for batch three only. It was not an outlier for the RTA condition or for the 2% offset strength property. It was an outlier in both the normalized and as-measured datasets. It was retained for this analysis.

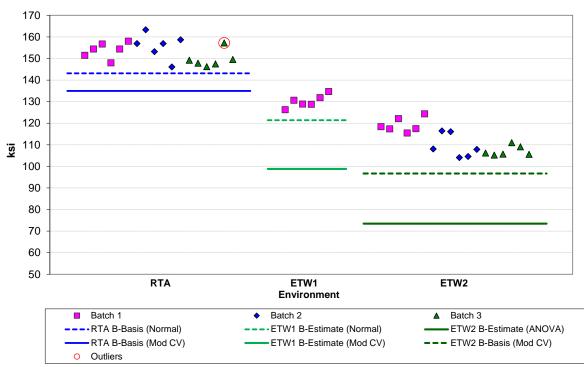
Statistics, estimates and basis values are given for the SSB1 2% offset strength data in Table 4-48, for ultimate strength data in Table 4-49, and for the chord modulus data in Table 4-50. The normalized data and the B-basis estimates and values are shown graphically for 2% offset strength in Figure 4-31 and for ultimate strength in Figure 4-32.

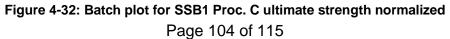


Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Quasi Isotropic Single Shear Bearing (SSB1 Proc. C) 2% Offset Strength Normalized

Figure 4-31: Batch plot for SSB1 Proc. C 2% offset strength normalized

Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Quasi Isotropic Single Shear Bearing (SSB1 Proc. C) Ultimate Strength Normalized





Single Shear Bearing (SSB1 Proc. C) 2% Offset Strength Basis Values and Statistics								
		Normalized		As-measured				
Env	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)		
Mean	109.2	111.6	93.67	108.8	111.6	93.31		
Stdev	3.094	4.211	8.625	3.249	4.325	8.845		
CV	2.834	3.774	9.208	2.986	3.873	9.479		
Modified CV	6.000	8.000	9.208	6.000	8.000	9.479		
Min	105.3	108.4	83.37	104.3	108.2	82.48		
Мах	117.3	119.5	110.2	117.4	119.8	109.9		
No. Batches	3	1	3	3	1	3		
No. Spec.	18	6	18	18	6	18		
		Basis Va	alues and Es	timates	_	-		
B-basis Value	103.1			102.4				
B-estimate		98.82	35.90		98.55	34.01		
A-estimate	98.74	89.75	NA	97.85	89.23	NA		
Method	Normal	Normal	ANOVA	Normal	Normal	ANOVA		
	Modified CV Basis Values and Estimates							
B-basis Value	96.24			95.93				
B-estimate		84.69	NA		84.74	NA		
A-estimate	87.10	66.29	INA	86.81	66.33	INA		
Method	Normal	Normal		Normal	Normal			

Table 4-48: Statistics for SSB1 Proc. C 2% Offset Strength data

Single Shear Bearing (SSB1 Proc. C) Ultimate Strength Basis Values and Statistics							
	Normalized			As-measured			
Env	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	
Mean	153.1	130.2	112.0	152.6	130.3	111.5	
Stdev	5.050	2.908	6.524	5.493	2.806	6.838	
CV	3.299	2.234	5.827	3.600	2.154	6.131	
Modified CV	6.000	8.000	6.914	6.000	8.000	7.066	
Min	146.1	126.3	104.1	144.4	126.7	103.9	
Мах	163.3	134.7	124.4	163.1	135.0	124.7	
No. Batches	3	1	3	3	1	3	
No.Spec.	18	6	18	18	6	18	
		Basis Va	alues and Es	timates			
<b>B-basis Value</b>	143.1			141.7			
B-estimate		121.4	73.44		121.8	71.04	
A-estimate	136.1	115.1	45.95	134.1	115.7	42.15	
Method	Normal	Normal	ANOVA	Normal	Normal	ANOVA	
	N	lodified CV E	Basis Values a	and Estimate	s		
B-basis Value	135.0		96.68	134.5			
B-estimate		98.81			98.87	NA	
A-estimate	122.1	77.34	85.87	121.7	77.39	NA	
Method	Normal	Normal	Normal	Normal	Normal		

Table 4-49: Statistics and Basis Values for SSB1 Proc. C Ultimate Strength data

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Single Shear Bearing (SSB1 Proc. C) Chord Modulus Statistics							
		Normalized			As-measured		
Env	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	RTA (70°F)	ETW1 (180°F)	ETW2 (250°F)	
Mean	1.878	2.060	1.721	1.872	2.061	1.715	
Stdev	0.1184	0.1293	0.2349	0.1167	0.1253	0.2378	
CV	6.307	6.278	13.65	6.236	6.080	13.87	
Modified CV	7.154	8.000	13.65	7.118	8.000	13.87	
Min	1.632	1.940	1.429	1.623	1.944	1.415	
Max	2.080	2.238	2.173	2.078	2.232	2.175	
No.Batches	3	1	3	3	1	3	
No. Spec.	18	6	18	18	6	18	

Table 4-50: Statistics and Basis Values for SSB1 Proc. C Chord Modulus data

## 4.29 "10/80/10" Single-Shear Bearing 2 (SSB2, Proc. C)

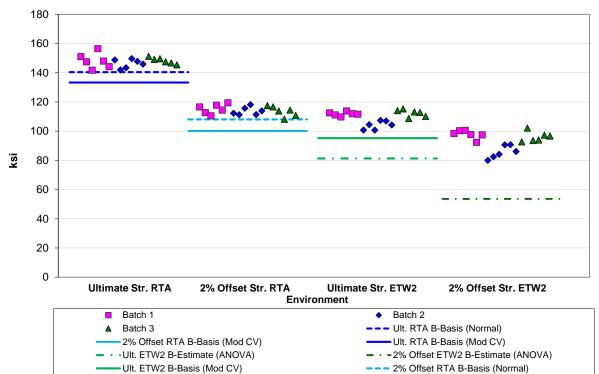
The SSB2 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for three properties, 2% offset strength, ultimate and chord modulus. SSB2 tests were performed at two different environmental conditions.

The ETW2 datasets for both 2% offset strength and ultimate strength, both normalized and as-measured, failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. The ultimate strength ETW2 datasets, both normalized and as-measured, passed the ADK test after the modified CV transformation but the 2% offset strength ETW2 datasets did not, so modified CV basis values are provided for only for the ultimate strength datasets.

Both the normalized and as-measured ultimate strength dataset met all requirements for pooling across the environments for the modified CV basis value computations.

There was one statistical outlier. The largest value in batch one of the as-measured RTA condition for the ultimate strength property was an outlier for the RTA condition, but not for the batch one and not for the normalized dataset. It was not an outlier for the 2% offset strength property. It was retained for this analysis.

Statistics, estimates and basis values are given for the SSB2 strength data in Table 4-51 and for the chord modulus data in Table 4-52. The normalized data, B-estimates, and the B-basis values are shown graphically in Figure 4-33.



Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape "Soft" Single Shear Bearing (SSB2 Proc. C) Strength Normalized

	Sing	e Shear Bear	ing (SSB2 Pr	oc. C) Streng	th Basis Valu	es and Stati	stics	·	
	2% Offset Strength					Ultimate Strength			
	Norm	alized	As-me	asured	Norma	alized	As-me	As-measured	
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)	
Mean	114.2	93.16	113.6	92.73	147.6	109.4	146.8	108.9	
Stdev	3.112	6.477	3.084	6.281	3.602	4.477	3.402	4.167	
CV	2.725	6.953	2.715	6.773	2.441	4.091	2.318	3.826	
Modified CV	6.000	7.476	6.000	7.387	6.000	6.045	6.000	6.000	
Min	108.2	80.04	107.0	80.04	141.7	100.7	141.3	100.7	
Max	119.5	102.2	119.1	101.1	156.5	115.3	156.1	114.0	
No. Batches	3	3	3	3	3	3	3	3	
No. Spec.	18	18	18	18	18	18	18	18	
			Basis Va	lues and Esti	mates				
B-basis Value	108.1		107.5		140.5		140.0		
B-estimate		53.61		54.95		81.27		83.37	
A-estimate	103.7	25.38	103.2	28.00	135.4	61.18	135.3	65.14	
Method	Normal	ANOVA	Normal	ANOVA	Normal	ANOVA	Normal	ANOVA	
Modified CV Basis Values and Estimates									
B-basis Value	100.7		100.1		133.3	95.19	132.6	94.79	
A-estimate	91.10	NA	90.6	NA	123.7	85.51	123.0	85.19	
Method	Normal		Normal		pooled	pooled	pooled	pooled	
		· · · · · · · · · · · · · · · · · · ·							

Table 4-51: Statistics and Basis Values for SSB2 Proc. C Strength data

Single Shear Bearing (SSB2 Proc. C) Chord Modulus Statistics							
	Norm	alized	As-me	asured			
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)			
Mean	1.318	1.260	1.310	1.254			
Stdev	0.02780	0.1260	0.02871	0.1227			
CV	2.110	10.01	2.191	9.790			
Modified CV	6.000	10.01	6.000	9.790			
Min	1.252	1.051	1.249	1.050			
Max	1.370	1.423	1.366	1.414			
No. Batches	3	3	3	3			
No. Spec.	18	18	18	18			

Table 4-52: Statistics for SSB2 Proc. C Chord Modulus data

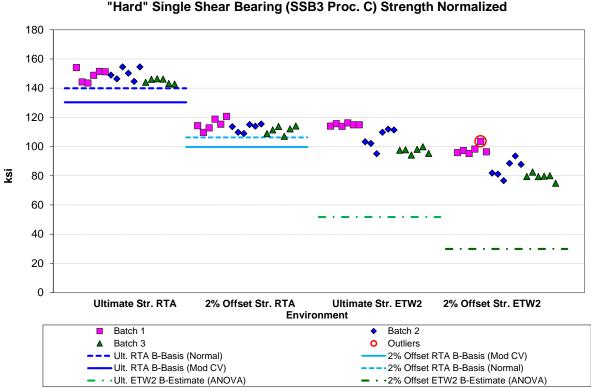
## 4.30 "50/40/10" Single-Shear Bearing 3 (SSB3, Proc. C)

The SSB3 data is normalized, so statistics for both normalized and as-measured values are provided. Data is available for three properties, 2% offset strength, ultimate and chord modulus. SSB3 tests were performed at two different environmental conditions.

The ETW2 datasets for both 2% offset strength and ultimate strength, both the normalized and as-measured, failed the Anderson Darling k-sample test (ADK test) for batch to batch variability, which means that CMH-17-1H guidelines required using the ANOVA analysis. With fewer than five batches, this is considered an estimate. None of these datasets passed the ADK test after the modified CV transformation, so modified CV basis values are not provided.

There was one statistical outlier. The largest value in batch one of the ETW2 condition for the 2% offset strength property was an outlier for batch one only. It was not an outlier for the ETW2 condition or for the ultimate strength property. It was an outlier in both the normalized and as-measured datasets. It was retained for this analysis.

Statistics, estimates and basis values are given for the SSB3 strength data in Table 4-53 and for the chord modulus data in Table 4-54. The normalized data, B-estimates and the B-basis values are shown graphically in Figure 4-34.



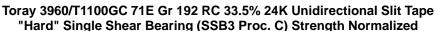


Figure 4-34: Batch plot for SSB3 Proc. C strength normalized

Single Shear Bearing (SSB3 Proc. C) Strength Basis Values and Statistics									
	2% Offset Strength					Ultimate	Strength		
	Normalized		As-measured		Normalized		As-measured		
Env	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)	RTA (70°F)	ETW2 (250°F)	
Mean	113.1	87.34	112.3	86.77	147.8	105.9	146.8	105.2	
Stdev	3.472	8.862	3.551	8.768	4.019	8.379	4.223	8.376	
CV	3.070	10.15	3.162	10.11	2.719	7.913	2.876	7.963	
Modified CV	6.000	10.15	6.000	10.11	6.000	7.957	6.000	7.982	
Min	107.0	74.92	104.8	73.92	142.8	94.16	140.9	93.30	
Max	120.7	103.6	119.7	102.3	154.5	116.2	154.6	115.3	
No. Batches	3	3	3	3	3	3	3	3	
No. Spec.	18	18	18	18	18	18	18	18	
			Basis V	alues and Es	timates				
B-basis Value	B-basis Value 106.2 105.3 139.9 138.5								
B-estimate		29.85		30.16		51.76		51.21	
A-estimate	101.4	NA	100.3	NA	134.3	13.13	132.6	12.68	
Method	Normal	ANOVA	Normal	ANOVA	Normal	ANOVA	Normal	ANOVA	
Modified CV Basis Values and Estimates									
B-basis Value	99.68		99.00		130.3		129.4		
A-estimate	90.21	NA	89.59	NA	117.9	NA	117.1	NA	
Method	Normal		Normal		Normal		Normal		

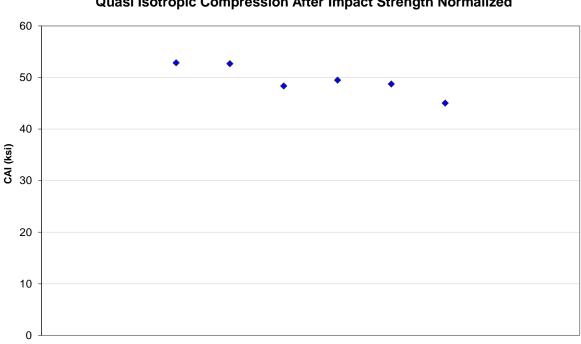
Table 4-53: Statistics and Basis Values for SSB3 Proc. C Strength data

Single Shear Bearing (SSB3 Proc. C) Chord Modulus Statistics							
	Norm	alized	As-measured				
Env	RTA (70°F) ETW2 (250°F) RTA (70°F)		ETW2 (250°F)				
Mean	1.768	1.682	1.756	1.671			
Stdev	0.05979	0.1821	0.06520	0.1783			
CV	3.382	10.83	3.714	10.67			
Modified CV	6.000	10.83	6.000	10.67			
Min	1.632	1.451	1.617	1.449			
Max	1.860	1.988	1.861	1.972			
No. Batches	3	3	3	3			
No. Spec.	18	18	18	18			

Table 4-54: Statistics for SSB3 Proc. C Chord Modulus data

## 4.31 "25/50/25" Compression After Impact 1 (CAI1)

The CAI1 data is normalized. Basis values are not computed for this property. Data from only one batch of material is available. However the summary statistics are presented in Table 4-55 and the data are displayed graphically in Figure 4-35. There were no statistical outliers.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Quasi Isotropic Compression After Impact Strength Normalized

RTA Environment, Batch 1

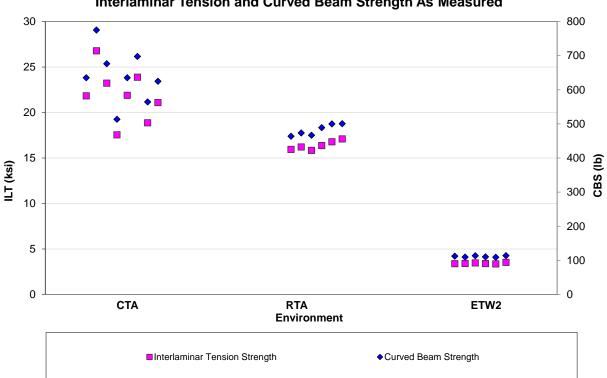
Compression After Impact Strength (ksi) Statistics							
Normalized As-measured							
Env	RTA (70°F)	RTA (70°F)					
Mean	49.52	50.24					
Stdev	2.937	2.973					
CV	5.931	5.917					
Modified CV	8.000	8.000					
Min	45.03	45.66					
Max	52.83	53.55					
No.Batches	1	1					
No.Spec.	6	6					

#### Figure 4-35: Plot for CAI1 strength normalized

Table 4-55: Statistics for CAI1 Strength data

# 4.32 "100/0/0" Interlaminar Tension and Curved Beam Strength (ILT and CBS)

The ILT and CBS data is not normalized. Basis values are not computed for these properties. Data from only one batch of material is available. However the summary statistics are presented in Table 4-56 and the data are displayed graphically in Figure 4-36. There were no statistical outliers.



#### Toray 3960/T1100GC 71E Gr 192 RC 33.5% 24K Unidirectional Slit Tape Interlaminar Tension and Curved Beam Strength As Measured

Interlaminar Tension (ILT) and Curved Beam Strength (CBS) Statistics As-Measured							
Property	Interla	minar Streng	gth (ksi)	Curved Beam Strength (lb)			
Env	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	CTA (− 65°F)	RTA (70°F)	ETW2 (250°F)	
Mean	21.89	16.37	3.423	640.3	482.2	111.4	
Stdev	2.886	0.4923	0.06192	80.04	16.51	2.03	
CV	13.18	3.007	1.809	12.50	3.424	1.819	
Mod CV	13.18	8.000	8.000	12.50	8.000	8.000	
Min	17.55	15.83	3.361	513.6	463.6	109.1	
Max	26.78	17.10	3.525	775.1	500.6	113.9	
No.Batches	1	1	1	1	1	1	
No. Spec.	8	6	6	8	6	6	

Table 4-56: Statistics for ILT and CBS data

#### 5. Outliers

Outliers were identified according to the standards documented in section 2.1.5, which are in accordance with the guidelines developed in section 8.3.3 of CMH-17-1H. An outlier may be an outlier in the normalized data, the as-measured data, or both. A specimen may be an outlier for the batch only (before pooling the three batches within a condition together) or for the condition (after pooling the three batches within a condition together) or both.

Approximately 5 out of 100 specimens will be identified as outliers due to the expected random variation of the data. This test is used only to identify specimens to be investigated for a cause of the extreme observation. Outliers that have an identifiable cause are removed from the dataset as they inject bias into the computation of statistics and basis values. Specimens that are outliers for the condition and in both the normalized and as-measured data are typically more extreme and more likely to have a specific cause and be removed from the dataset than other outliers. Specimens that are outliers only for the batch, but not the condition and specimens that are identified as outliers only for the normalized data or the as-measured data but not both, are typical of normal random variation.

All outliers identified were investigated to determine if a cause could be found. Outliers with causes were removed from the dataset and the remaining specimens were analyzed for this report. Information about specimens that were removed from the dataset along with the cause for removal is documented in the material property data report, NCAMP Test Report CAM-RP-2023-002 Rev N/C.

Outliers for which no causes could be identified are listed in Table 5-1. These outliers were included in the analysis for their respective test properties.

Test	Condition	Batch	Specimen Number	Normalized Strength	As-measured Strength	High/ Low	Batch Outlier	Condition Outlier	
UNC0	CTA (-65º F)	3	NTP3963Q1-TC-WEB-NIAR-T01-MST2-C-C1-1-UNC0-CTA-2	79.36	79.33	Low	Yes	Yes	
LC from UNC0	CIA (-05° F)	3	N IP3903Q1-1C-WEB-NIAK-101-MS12-C-C1-1-UNC0-C1A-2	209.4	209.5	LOW	res	res	
UNC0	ETW2 (250° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST2-A-C1-1-UNC0-ETW2-2	61.70	61.53	Low	Yes	No	
LC from UNC0	E1W2 (250° F)	1	N 1P3903Q1-1C-WEB-NIAR-101-MS12-A-C1-1-UNC0-E1W2-2	170.8	170.4	LOW	res	INO	
UNC0	ETW2 (250° F)	3	NTP3963Q1-TC-WEB-NIAR-T01-MST2-C-C2-1-UNC0-ETW2-2	52.35	51.70	Low	No	Yes	
LC from UNC0	ETw2 (250 T)	3	N IF 5905Q1-1C-WEB-NIAR-101-WS12-C-C2-1-UNC0-E1W2-2	144.9	143.2				
TT	CTA (-65º F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST1-A-C1-1-TT-CTA-1	NA	6.168	Low	No	Yes	
TT	CTA (-65º F)	2	NTP3963Q1-TC-WEB-NIAR-T01-MST1-B-C2-1-TT-CTA-3	NA	9.622	High	Yes	No	
LT	RTA (70° F)	2	NTP3963Q1-TC-WEB-NIAR-T01-MST1-B-C1-1-LT-RTA-1	580.4	576.7	High	Yes	No	
SBS1	ETA2 (250° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST1-A-C2-1-SBS-ETA2-1	NA	10.96	High	O	ne Batch	
IPS - 0.2% Strength Offset	ETW2 (250° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST3-A-C1-1-IPS-ETW2-3	NA	3.021	Low	Yes	No	
IPS - Strength at 5% Strain	ETW2 (250° F)	3	NTP3963Q1-TC-WEB-NIAR-T01-MST3-C-C1-1-IPS-ETW2-2	NA	4.755	Low	Yes	No	
UNT2	ETW2 (250° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST7-A-C1-1-UNT2-ETW2-3	60.80	60.84	Low	No	Yes	
UNT3	CTA (-65º F)	2	NTP3963Q1-TC-WEB-NIAR-T01-MST8-B-C2-1-UNT3-CTA-3	269.6	270.4	High	Yes	No	
UNT3	RTA (70° F)	2	NTP3963Q1-TC-WEB-NIAR-T01-MST8-B-C1-1-UNT3-RTA-2	251.8	252.2	Low	Yes	Yes	
UNC3	RTA (70° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST8-A-C1-1-UNC3-RTA-1	155.6	154.8	Low	Yes	No	
UNC3	ETW2 (250° F)	3	NTP3963Q1-TC-WEB-NIAR-T01-MST8-C-C2-1-UNC3-ETW2-1R	110.8	109.6	High	Yes	No	
OHT2	CTA (-65° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST7-A-C2-1-OHT2-CTA-1	55.82	Not at Outlier	Low	No	Yes	
OHC1	ETW1 (180°)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST6-A-C1-1-OHC1-ETW1-2	Not at Outlier	45.38	High	O	One Batch	
FHT2	RTA (70° F)	2	NTP3963Q1-TC-WEB-NIAR-T01-MST7-B-C2-1-FHT2-RTA-3	61.88	Not at Outlier	Low	Yes	No	
FHT3	ETW2 (250° F)	3	NTP3963Q1-TC-WEB-NIAR-T01-MST8-C-C1-1-FHT3-ETW2-2	214.5	212.3	High	No	Yes	
FHC1	ETW2 (250° F)	3	NTP3963Q1-TC-WEB-NIAR-T01-MST6-C-C2-1-FHC1-ETW2-3	Not at Outlier	44.94	Low	No	Yes	
FHC2	RTA (70° F)	2	NTP3963Q1-TC-WEB-NIAR-T01-MST7-B-C1-1-FHC2-RTA-1	56.49	56.07	Low	No	Yes	
FHC2	ETW2 (250° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST7-A-C1-1-FHC2-ETW2-1	38.07	37.95	High	Yes	No	
FHC3	ETW2 (250° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST8-A-C2-1-FHC3-ETW2-3	64.41	64.41	High	Yes	No	
SBS1	RTA (70° F)	2	NTP3963Q1-TC-WEB-NIAR-T01-MST6-B-C2-1-SBS1-RTA-2	NA	12.30	Low	Yes	Yes	
SSB1 - Ultimate Strength	RTA (70° F)	3	NTP3963Q1-TC-WEB-NIAR-T01-MST5-C-C2-1-SSB1-RTA-2	157.2	157.1	High	Yes	No	
SSB2 - Ultimate Strength	RTA (70° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST7-A-C2-1-SSB2-RTA-1	Not at Outlier	156.1	High	No	Yes	
SSB3 - 2% Offset Strength	ETW2 (250° F)	1	NTP3963Q1-TC-WEB-NIAR-T01-MST8-A-C2-1-SSB3-ETW2-2	103.6	102.3	High	No	Yes	

Table 5-1: List of Outliers

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